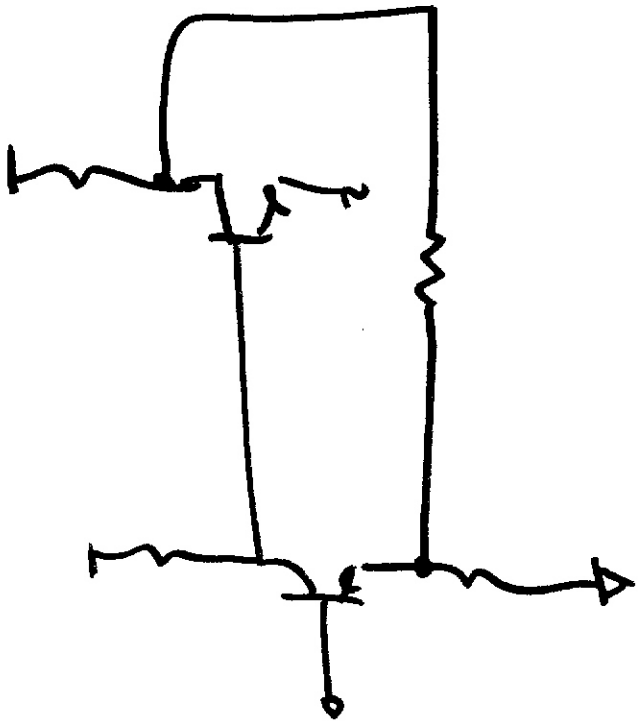
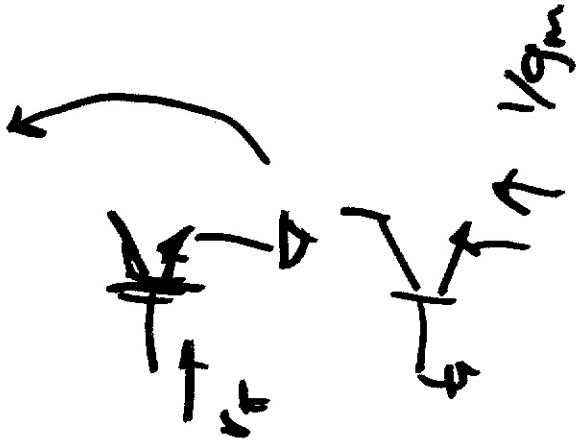
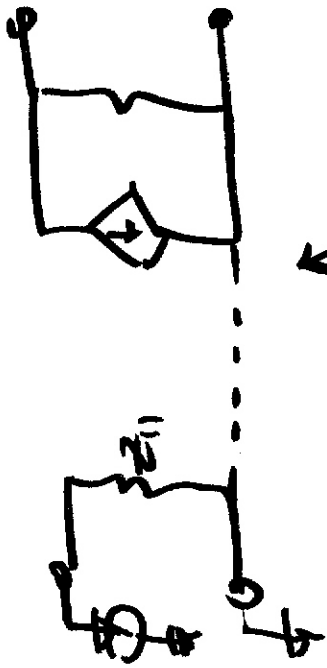


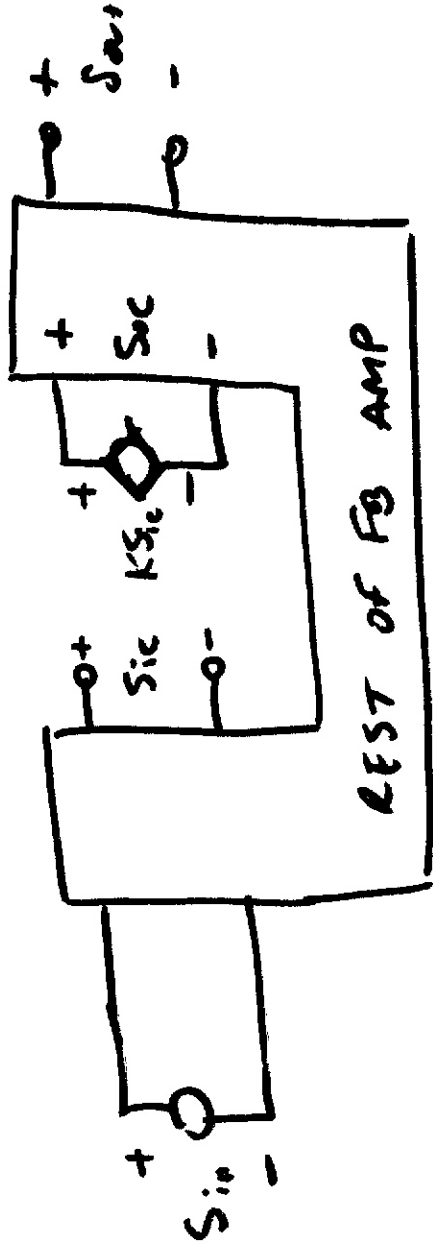
LECT 14



EX

11

RETURN RATIO ANALYSIS



$(k = g_m)$

(A) $S_{oc} = K S_{ic}$

(B) $S_{ic} = B_1 S_{in} - H S_{oc}$

(C) $S_{out} = d S_{in} + \beta_2 S_{oc}$

(D) $B_1 = \frac{S_{ic}}{S_{in}} \Big|_{S_{oc}=0} = \frac{S_{ic}}{S_{in}} \Big|_{k=0}$

GAIN
INPUT →
CONTROL
NODE
FOR $k=0$

$$(E) H = -\frac{S_{1c}}{S_{0c}} \Big|_{S_{1a}=0}$$

REVERSE GAIN

$$(F) d = \frac{S_{out}}{S_{in}} \Big|_{S_{0c}=0} = \frac{S_{out}}{S_{in}} \Big|_{k=0}$$

DIRECT FEEDBACK

$$(G) B_2 = \frac{S_{out}}{S_{0c}} \Big|_{S_{1a}=0}$$

PARTIAL GAIN
FROM GEN \rightarrow %
FOR INPUT
SHORT

(A) f(s)

$$S_{ic} + H \underbrace{S_{oc}}_{K S_{ic}} = B_1 S_{in}$$

$$S_{ic} (1 + KH) = B_1 S_{in}$$

$$\frac{S_{ic}}{S_{in}} = \left(\frac{B_1}{1 + KH} \right)$$

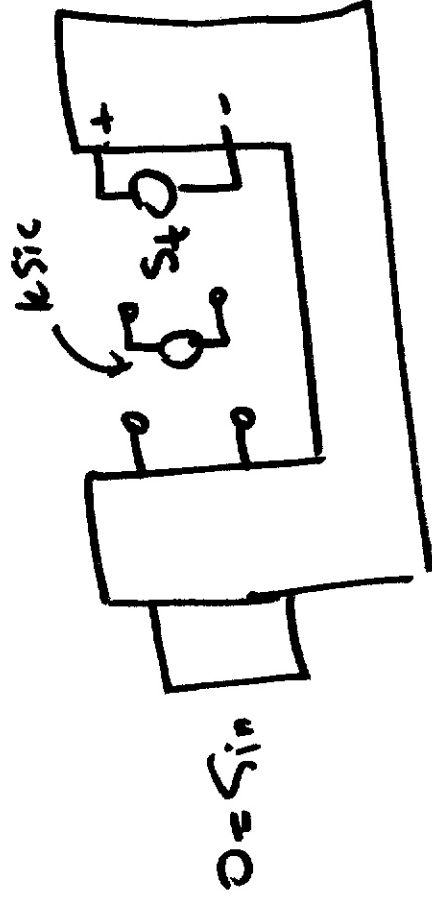
(C) $\frac{S_{out}}{S_{in}} = d \frac{S_{in}}{S_{in}} + B_2 \frac{S_{oc}}{S_{in}}$

$$= d + B_2 K \left(\frac{S_{ic}}{S_{in}} \right)$$

$A = d + \frac{B_1 K B_2}{1 + KH}$

CLOSED LOOP
GAIN

WHAT IS K_H ?



$K_H = R$ →
 LOOP GAIN
 OR
 RETURN RATIO

$$S_{ic} = \frac{B}{S_{in}} - H S_{oc}$$

$$= -H S_{oc}$$

$$S_r = -K_H S_{oc} = -K_H S_t$$

$$R = -\frac{S_r}{S_t} = \frac{K_H}{2}$$

$$A = d + \frac{B, K B_2}{1 + R}$$

$$g \approx B, K B_2$$

$$A = d + \frac{g}{1 + R} = \frac{d + dR + g}{1 + R}$$

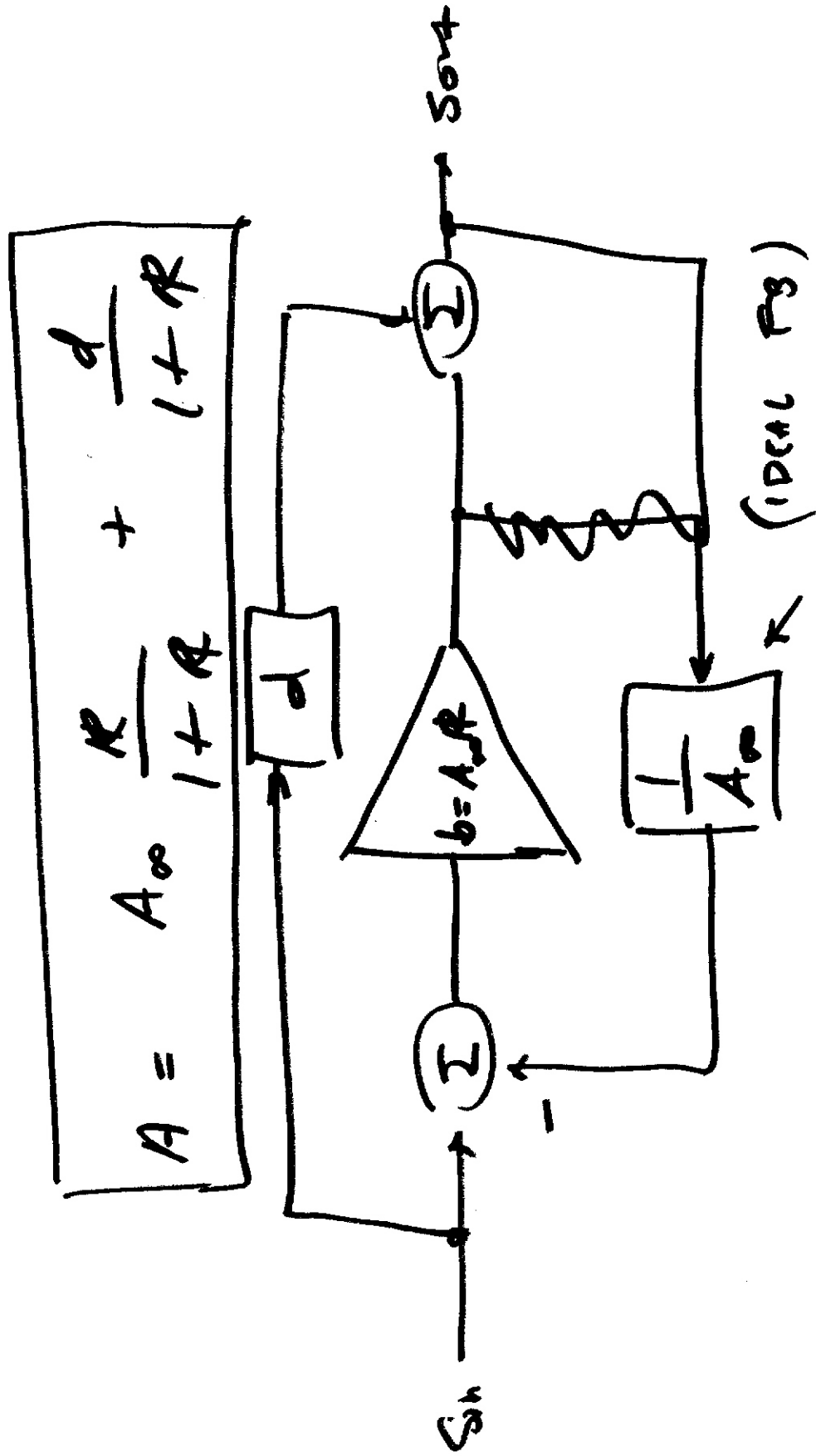
$$= \frac{R}{1 + R} \left(\frac{d + g}{R} \right)$$

$$= \frac{d(1 + R) + g}{1 + R}$$

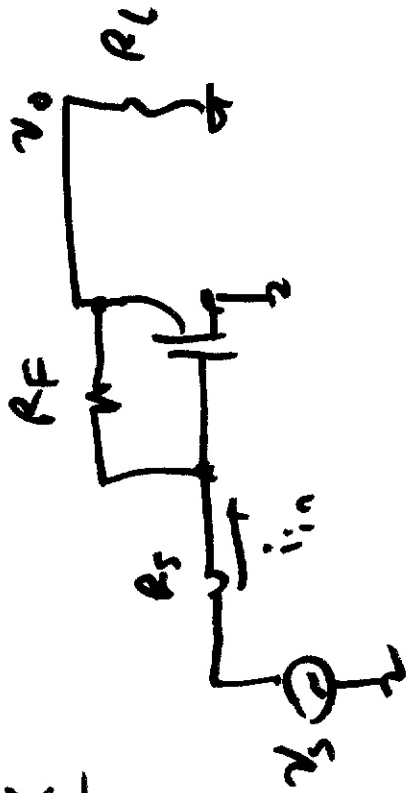
$$= \frac{R}{1 + R} \left(d + \frac{g}{R} \right) + \frac{d}{1 + R}$$

$A_{\infty} = \frac{g}{R} + d$
 CLOSED LOOP
 GAIN FOR VERY
 LARGE R

LET $R \rightarrow \infty$



EX



CALC A_{∞}
d
R

A_{∞} : GAIN AS $R \rightarrow \infty$ OR $h \rightarrow \infty$
 $g_m \rightarrow \infty$

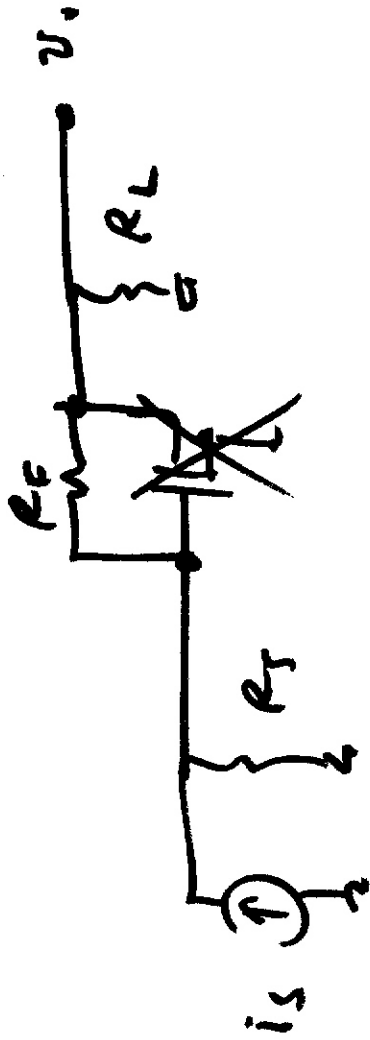
$$v_{gs} \rightarrow 0$$

$$\frac{v_s}{R_s} = i_{in}$$

$$v_o = -i_{in} \cdot R_F$$

$$\boxed{A_{\infty} = \frac{v_o}{i_{in}} = -R_F}$$

d : DIRECT FEEDBACK FOR $K = g_m = 0$



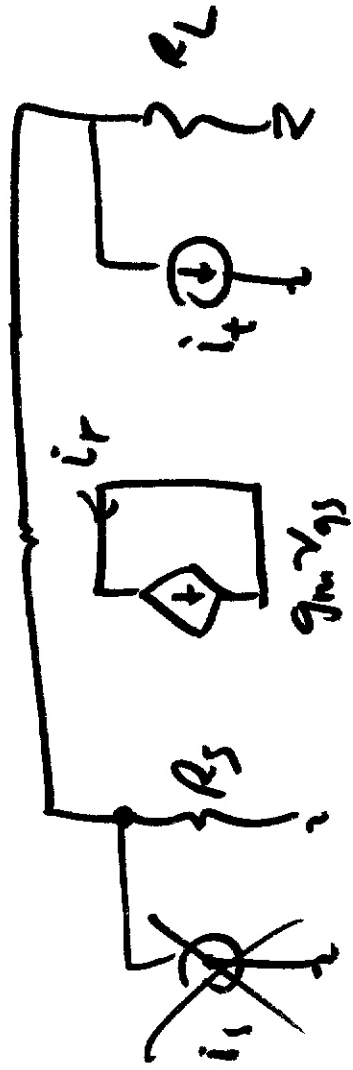
$$\frac{v_o}{i_s} = \frac{R_s}{R_s + R_F + R_L} \cdot R_L$$

$$d = \frac{R_s R_L}{R_s + R_F + R_L}$$

R RETURN RATIO

BREAK GENERATOR

INPUT = 0



$$V_{gs} = -i_L \cdot \frac{R_L}{R_L + R_F + R_S} \cdot R_S$$

$$i_L = g_m V_{gs} = - \frac{g_m R_L R_S}{R_L + R_F + R_S} i_L$$

$$R = \frac{-i_L}{i_L} = \frac{g_m R_L R_S}{R_L + R_F + R_S}$$

$$A = A_o \frac{R}{1+R} + \frac{d}{1+R}$$

$$= (-R_F) \frac{g_m R_L R_S}{(R_L + R_F + R_S) + g_m R_L R_S} +$$

$$\frac{R_S R_L}{R_S + R_F + R_L + g_m R_L R_S}$$

$$A = \frac{(1 - g_m R_F) R_S R_L}{R_F + R_L + (1 + g_m R_L) R_S}$$

$g_m R_E \rightarrow \infty$

$g_m R_L \rightarrow \infty$

$$A = \frac{-g_m R_E \beta_3 R_L}{g_m R_L \beta_3} = -R_E$$

$$= A_{\infty}$$

DIRECT $b = A_{\infty} \cdot R$

$$b = \left(\frac{g}{R} + d \right) R = g + dR$$

$$= B_1 k B_2 + d k H$$

$$= B_1 k B_2 + d k H$$

$$b = \left(B_1 + \frac{dH}{B_2} \right) k B_2 \left. \begin{array}{l} \frac{\sin \theta_1}{\sin \theta_2} \\ \frac{\sin \theta_1}{\sin \theta_2} \end{array} \right\} \begin{array}{l} \sin \theta_1 \\ \sin \theta_2 \end{array}$$

$$1F \quad S_{out} = 0$$

$$0 = S_{out} = d \sin + B_2 S_{oc}$$

$$B_2 S_{oc} = -d \sin$$

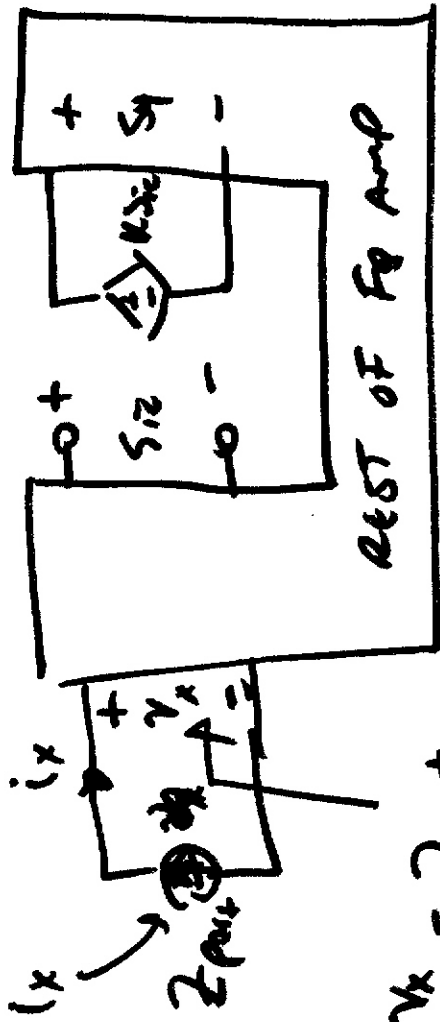
$$S_{ic} = B_1 \sin - H S_{oc}$$

$$= B_1 \sin - H \left(-\frac{d}{B_2} \right) \sin$$

②

$$\left| \frac{S_{ic}}{S_{in}} \right| = \left(B_1 + \frac{dH}{B_2} \right) S_{out=0}$$

CLOSED LOOP IMPEDANCES



$$Z_{F(1-k)} = Z_{F(1-k)}$$

$$V_x = a_1 i_x + a_2 S_Y$$

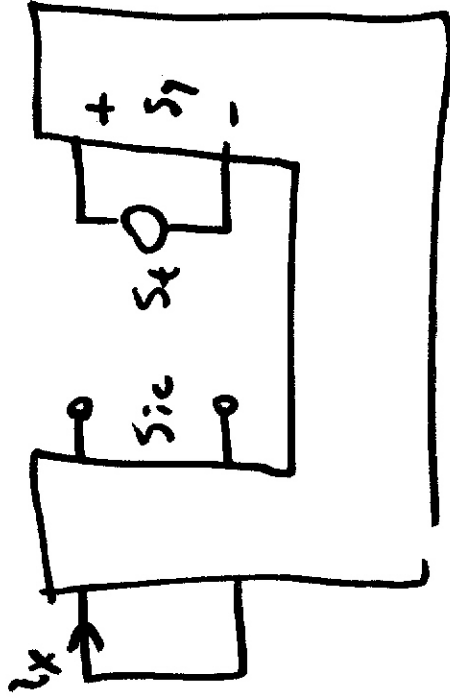
$$S_{ic} = a_3 i_x + a_4 S_Y$$

$$\text{SET } k=0 \Rightarrow S_Y=0$$

$$\frac{V_x}{i_x} = a_1 = Z_{F(1-k)} (k=0)$$

LEFT PORT X = SHORT CURRENT

$\rightarrow v_x = 0$



$s_t = s_y \quad i_x = -\frac{a_2}{a_1} s_t$

$s_{1c} = a_3 \left(-\frac{a_2}{a_1} s_t \right) + a_4 s_t$

~~$s_t = k s_{1c}$~~

$\frac{s_{1c}}{s_t} = a_4 - \frac{a_3 a_2}{a_1}$

$s_t = k s_{1c} = k \left(a_4 - \frac{a_3 a_2}{a_1} \right)$

$R_{S_{SHORT}} = -k \left(\right)$

$\frac{a_3 a_2}{a_1}$

$$R_{\text{start}} = -k \left(a_4 - \frac{a_3 a_2}{a_1} \right)$$

$$Z_x = \frac{v_x}{i_x} = a_1 + a_2 \frac{s_4}{i_x}$$

$$= a_1 + a_2 \frac{k s_{ic}}{i_x}$$

$$\frac{s_{ic}}{i_x} = a_3 + a_4 \cdot \frac{k s_{ic}}{i_x}$$

$$\left(\frac{s_{ic}}{i_x} \right) (1 - k a_4) = a_3$$

LET PORT X = OPEN CIRCUIT $i_x = 0$

$$\text{CALC } R \quad s_y = s_t$$

$$s_{ic} = a_y s_y$$

$$s_r = k s_{ic} = k a_y s_t$$

$$R_{\text{open}} = -k a_y$$

$$Z_x = a_1 + \frac{a_2 k a_3}{1 - k a_4}$$

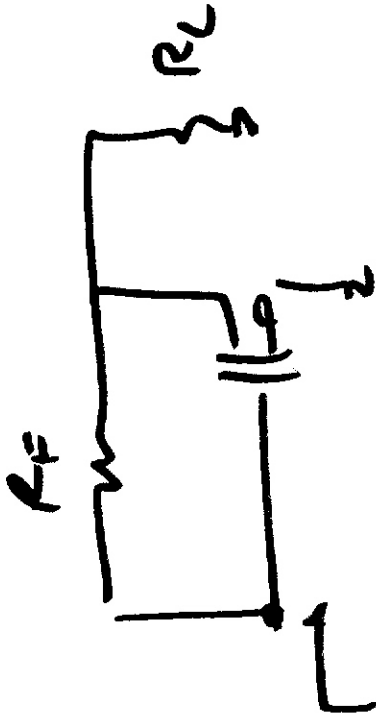
$$= \frac{a_1 - k a_1 a_4 + a_2 k a_3}{1 - k a_4}$$

$$= a_1 \left(\frac{1 - k \left(a_4 - \frac{a_2 a_3}{a_1} \right)}{1 - k a_4} \right)$$

$$Z_x = Z_{\text{port}}(k=0) \frac{(1 + R_{\text{short}})}{(1 + R_{\text{open}})}$$

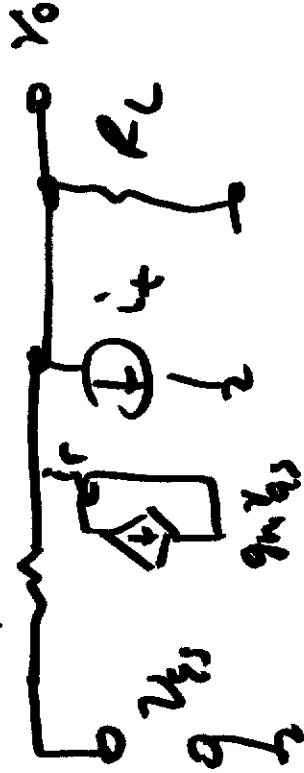
BLACKMAN'S IMPEDANCE FORMULA

EX



$$Z_{in} = ?$$

$$Z(R=0) = R_F + R_L$$



R_{open}

$$v_{gs} = v_o = -i_t \cdot R_L$$

$$i_t = g_m v_{gs} = -g_m R_L i_t$$

$$R_{open} = +g_m R_L$$

R_{short}

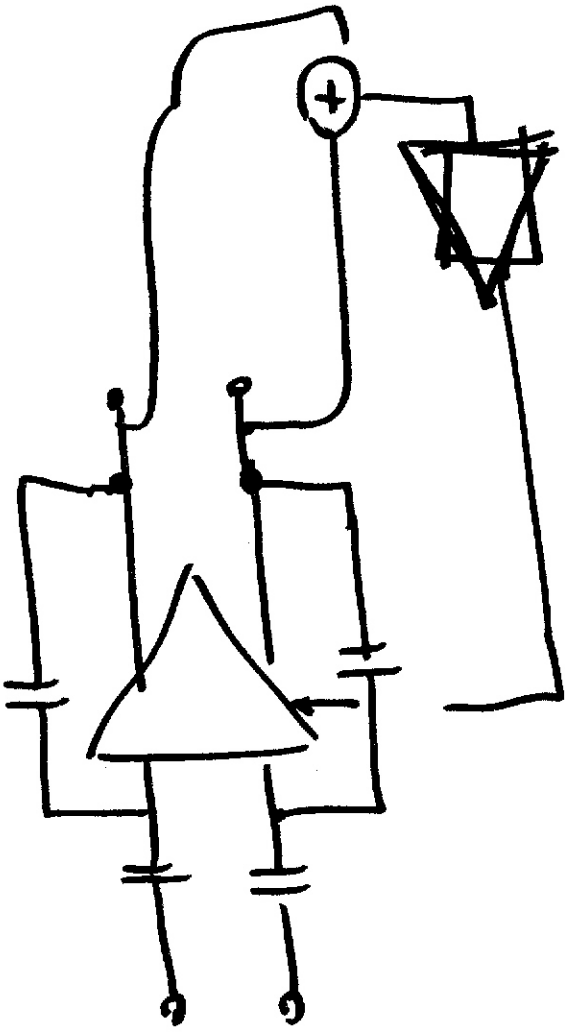


$$v_{gs} = 0 \quad i_r = 0$$

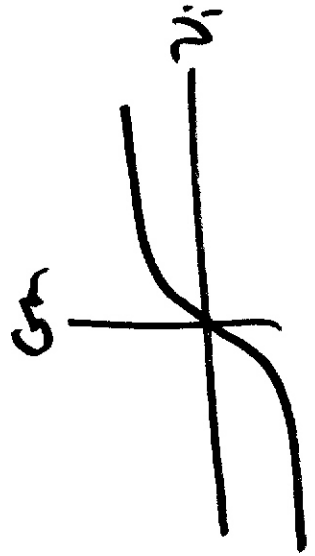
$$R_{short} = 0$$

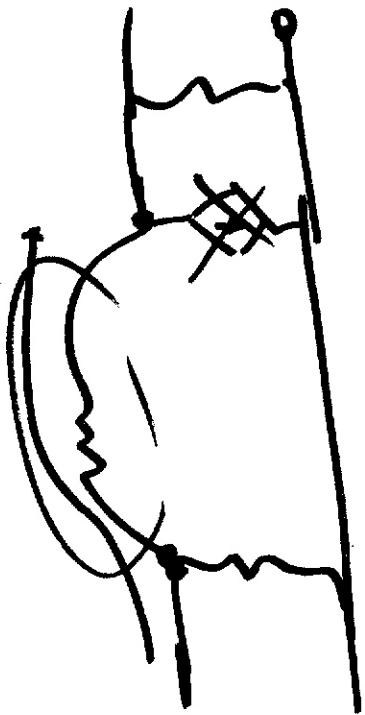
$$Z = Z(u=0) \frac{(1 + R_{short})}{(1 + R_{short}^{open})}$$

$$Z = \frac{(R_F + R_L)}{1 + j\omega R_L} \approx \left(\frac{1}{j\omega} \right) \left(\frac{R_F + R_L}{R_L} \right)$$



Common mode loop ξ
 DIFF mode loop DECOUPLED





$$y_{12} = 0 \Rightarrow \text{STOPS FB}$$

$$y_{21} = 0 \Rightarrow ?$$