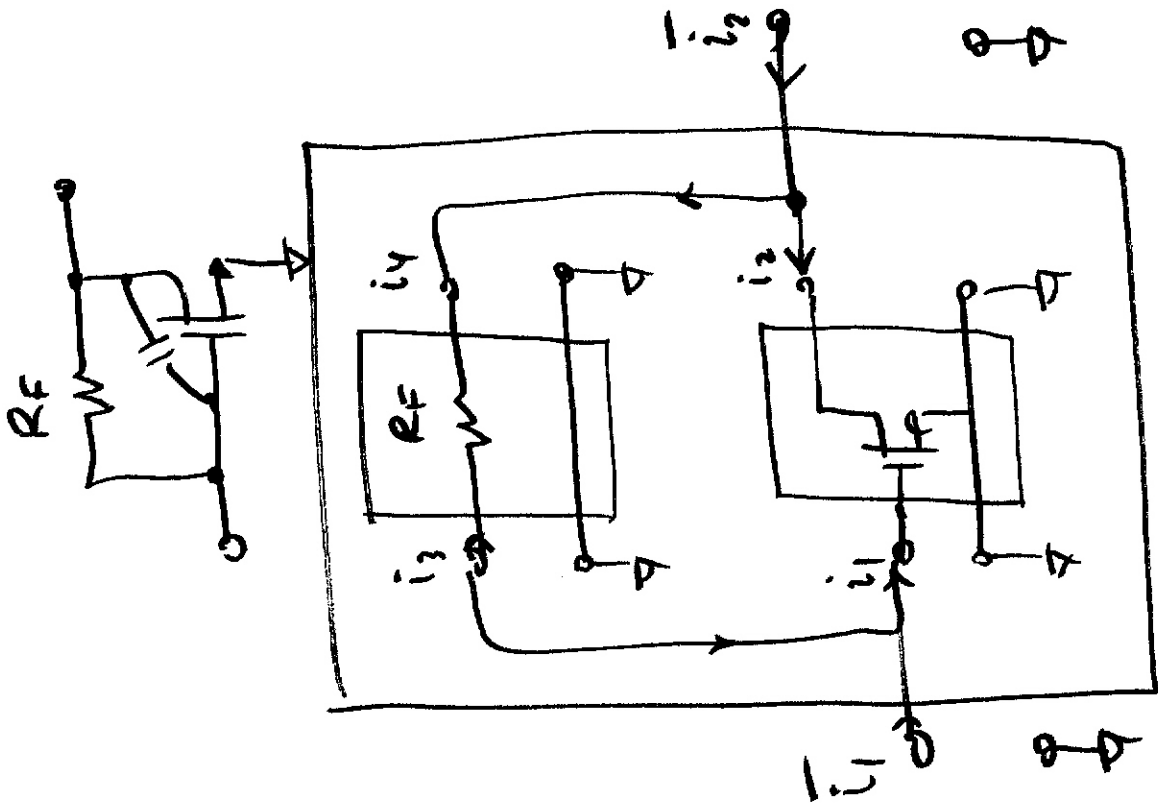


FEEDBACK



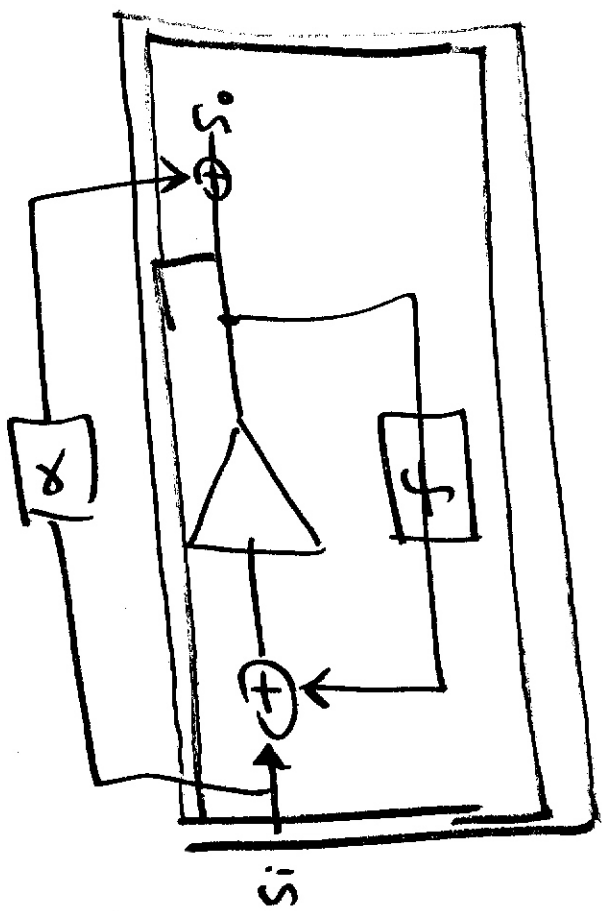
$$\bar{i}_2 = i_2 + i_4$$

$$\bar{i}_1 = i_1 + i_3$$

$$\begin{pmatrix} i_1 \\ i_2 \end{pmatrix} = Y^a \begin{pmatrix} v_1 \\ v_2 \end{pmatrix}$$

$$\begin{pmatrix} i_3 \\ i_4 \end{pmatrix} = Y^{fb} \begin{pmatrix} v_1 \\ v_2 \end{pmatrix}$$

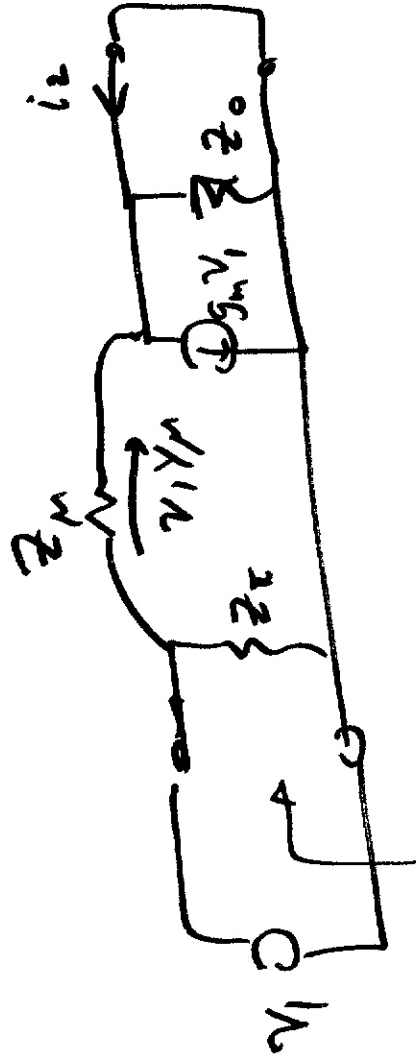
$$\begin{pmatrix} \bar{i}_1 \\ \bar{i}_2 \end{pmatrix} = (Y^a + Y^{fb}) \begin{pmatrix} v_1 \\ v_2 \end{pmatrix}$$



Y-Param AMP

$$i_1 = Y_{11} v_1 + Y_{12} v_2$$

$$i_2 = Y_{21} v_1 + Y_{22} v_2$$



$$Y_{11} = \frac{i_1}{v_1} \Big|_{v_2=0} = g_m - Y_r$$

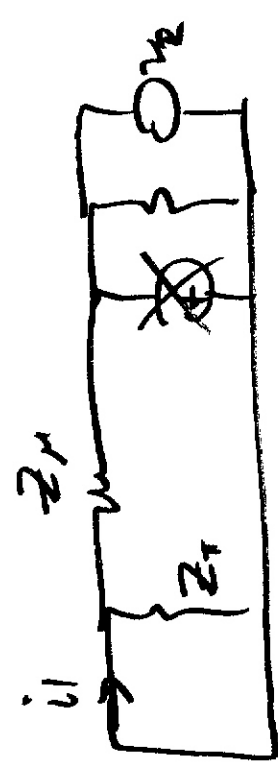
$$Y_{21} = \frac{i_2}{v_1} \Big|_{v_2=0}$$

$$Y_{12} = \frac{i_1}{v_2} \Big|_{v_1=0} = -Y_r$$

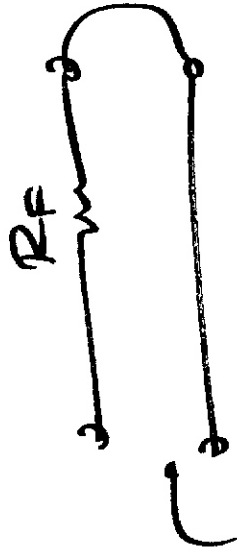
$$Y_{11} = \frac{i_1}{v_1} \Big|_{v_2=0}$$

$$Y_{11} = Y_{\pi} + Y_{\mu}$$

$$Y_{22} = Y_0 + Y_{\mu}$$



FB NETWORK



$$Y_{11} = Y_{22} = Y_{RF} = GF$$

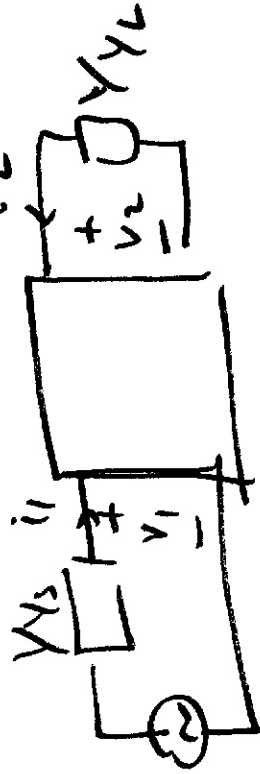
$$Y_{12} = Y_{21} = -GF$$

$$Y = Y^a + Y^{fb} =$$

$$Y^a + \begin{pmatrix} GF & -GF \\ -GF & GF \end{pmatrix} =$$

$$\begin{bmatrix} j\omega(C_{gs} + C_{gd}) + GF & -j\omega C_{gd} - GF \\ g_m - j\omega C_{gd} - GF & G_o + j\omega(C_{d6} + C_{gd}) + GF \end{bmatrix}$$

$$i_2 = -Y_L \cdot v_2$$



$$i_2 = Y_{21} v_1 + Y_{22} v_2 = -Y_L v_2$$

$$v_2 (Y_{22} + Y_L) = -Y_{21} v_1$$

$$A_{v,i} = \frac{V_2}{V_1} = - \frac{Y_{21}}{Y_{22} + Y_L}$$

$$A_V = \frac{V_2}{V_S} = \frac{V_2}{V_1} \cdot \frac{V_1}{V_S} = A_{v,i} \cdot \underbrace{\frac{Y_S}{Y_S + Y_{in}}}_{\text{VOLTAGE DIVIDER}}$$

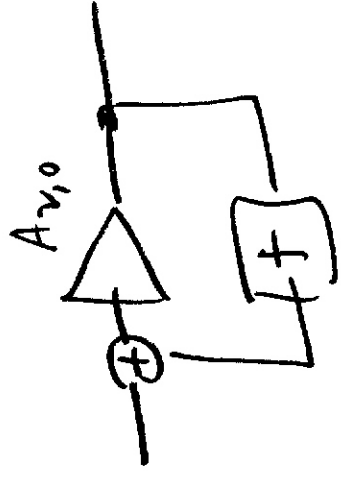
$$Y_{in} = Y_{11} - \frac{Y_{12} Y_{21}}{(Y_L + Y_{22})}$$

$$A_V = \frac{-Y_{21}}{Y_{22} + Y_L} \cdot \frac{Y_S (\cancel{Y_L + Y_{22}})}{Y_S (Y_L + Y_{22}) + Y_{11} (Y_L + Y_{22}) - Y_{12} Y_{21}}$$

$$A_V = \frac{-Y_{21} Y_S}{(Y_S + Y_{11})(Y_L + Y_{22}) - Y_{12} Y_{21}}$$

$$A_{v,0} = A_v \Big|_{Y_{12}=0} = \frac{-Y_{21} Y_S}{(Y_S + Y_{11})(Y_L + Y_{22})}$$

$$A_v = \frac{\frac{-Y_{21} Y_S}{(Y_S + Y_{11})(Y_L + Y_{22})}}{1 - \frac{Y_{12} Y_{21}}{(Y_S + Y_{11})(Y_L + Y_{22})}}$$



$$\frac{S_o}{S_i} = \frac{A_{v,0}}{1 - A_{v,0} f}$$

$$A_v = \frac{A_{v,0}}{1 - T}$$

$$T = A_{v,0} \cdot f = \frac{Y_{12} Y_{21}}{(Y_S + Y_{11})(Y_L + Y_{22})} = \frac{-Y_{21} Y_S}{(Y_S + Y_{11})(Y_L + Y_{22})} \cdot f$$

$$f = -\frac{Y_{12}}{Y_S}$$

$$A_{vo} = \frac{-Y_{21} Y_S}{(Y_S + Y_{in})(Y_L + Y_{out})} = \frac{-(g_m - j\omega C_{gd} - G_F) G_S}{(G_S + j\omega(C_{gs} + C_{gd}) + G_F) \times (G_L + j\omega(C_{ab} + C_{pd}) + G_F)}$$

$$T = A_{vo} \cdot f = -A_{vo} \cdot \frac{-(j\omega C_{gd} + G_F)}{G_S}$$

$$T(\omega \gg 0) = \frac{+g_m G_S}{(G_S + G_F)(G_L + G_F)} \cdot \frac{G_F}{G_S}$$

$$T = \frac{g_m R_F}{(G_S + G_F)(G_L + G_F)} = \frac{g_m R_F}{\left(1 + \frac{R_F}{R_S}\right)\left(1 + \frac{R_F}{R_L}\right)}$$

EX: $g_m = 10 \text{ mS}$ $R_F = 10 \text{ k}\Omega$

$$\frac{R_F}{R_S} = \frac{R_F}{R_L} = 1$$

$$T = \frac{100}{4} = 25$$

$$T = \frac{g_m R_F}{\left(1 + \frac{R_F}{R_L}\right)}$$

T =

AS $R_S \rightarrow \infty$

CURRENT AMPLIFIER
(TO VOLTAGE)

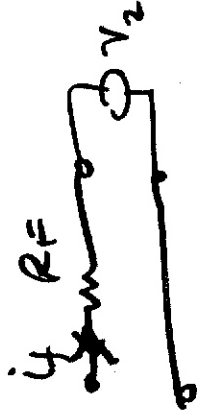
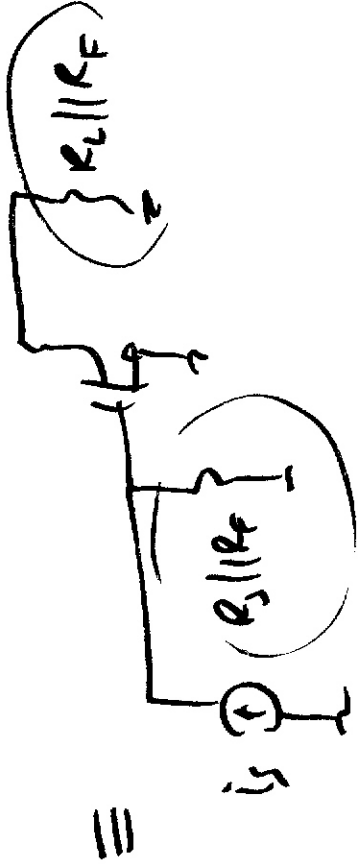
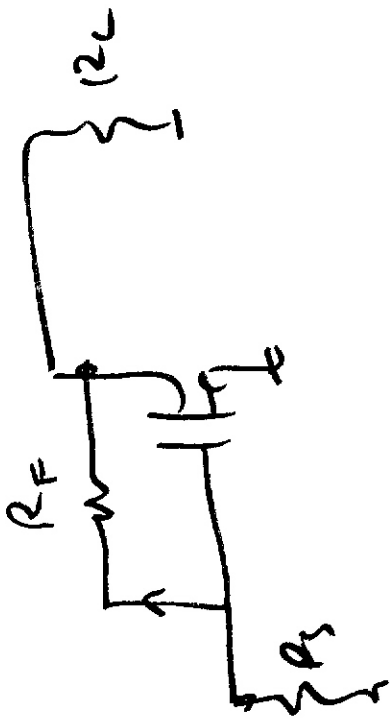
GOOD

$$\Rightarrow \frac{g_m R_F}{\left(1 + \frac{R_F}{R_S + R_0}\right)}$$

T =

AS $R_S \rightarrow 0$

LOADED FB CIRC



$$f = -1/R_F$$

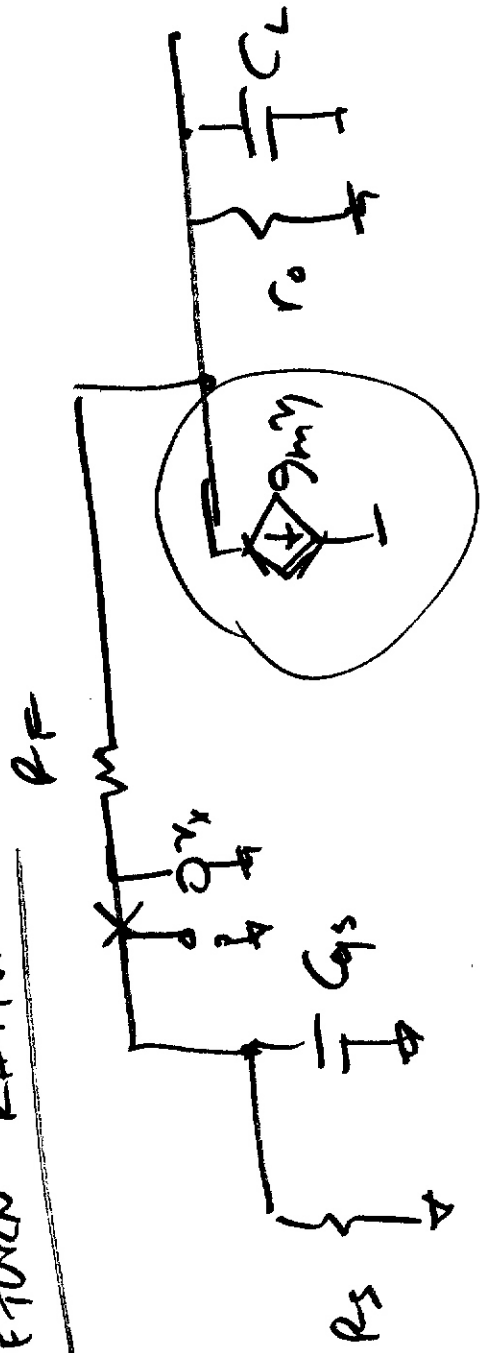
$$A_0 = -g_m \cdot (R_s || R_F) \cdot (R_L || R_F)$$

$$T = A_0 f = \frac{g_m \cdot R_F}{\left(\frac{1}{R_s} + \frac{1}{R_F}\right) \left(\frac{1}{R_L} + \frac{1}{R_F}\right)}$$

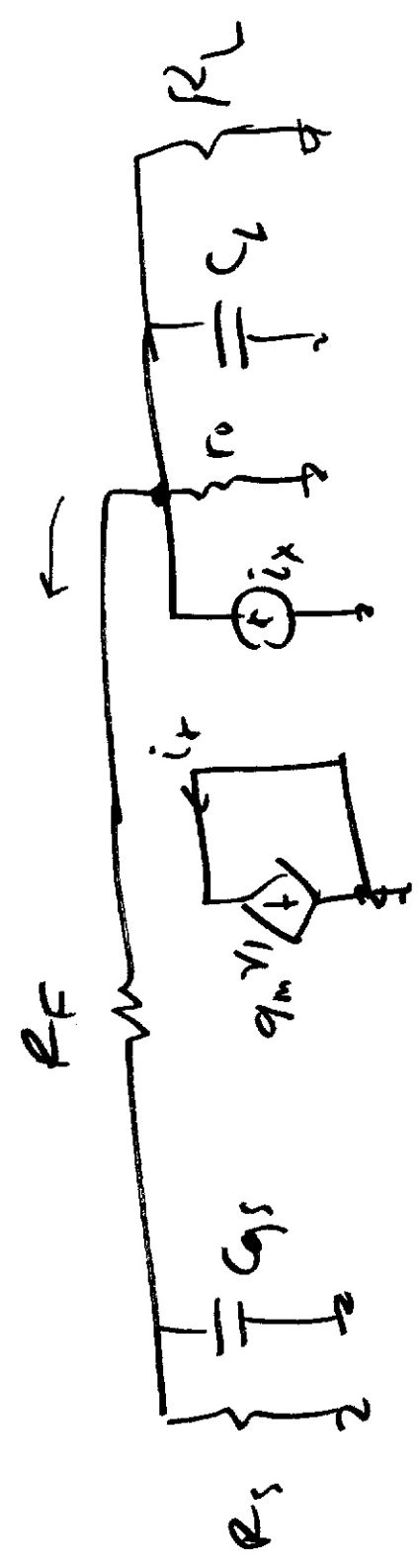
$$= \frac{g_m R_F}{\left(1 + \frac{R_F}{R_s}\right) \left(1 + \frac{R_F}{R_L}\right)}$$

$$= \frac{g_m R_F}{\left(1 + \frac{R_F}{R_s}\right) \left(1 + \frac{R_F}{R_L}\right)}$$

RETURN RATIO



IDEAL CURRENT SOURCE



$$R = \frac{i_x}{i_x}$$

$$i_x \frac{(G_0 + j\omega C_L)}{G_0 + j\omega C_L} \oplus$$

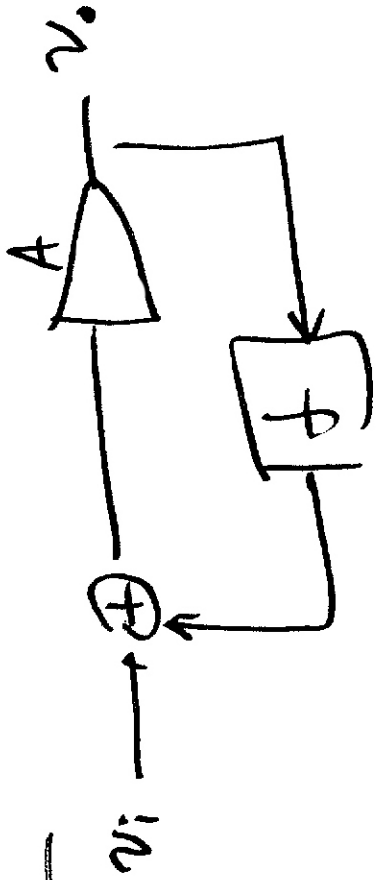
$$i_x \frac{R_L}{R_L + R_F + R_S} \cdot R_S \cdot g_m = i_r$$

$$T = \frac{i_r}{i_x} = \frac{g_m R_L R_S}{R_L + R_F + R_S}$$

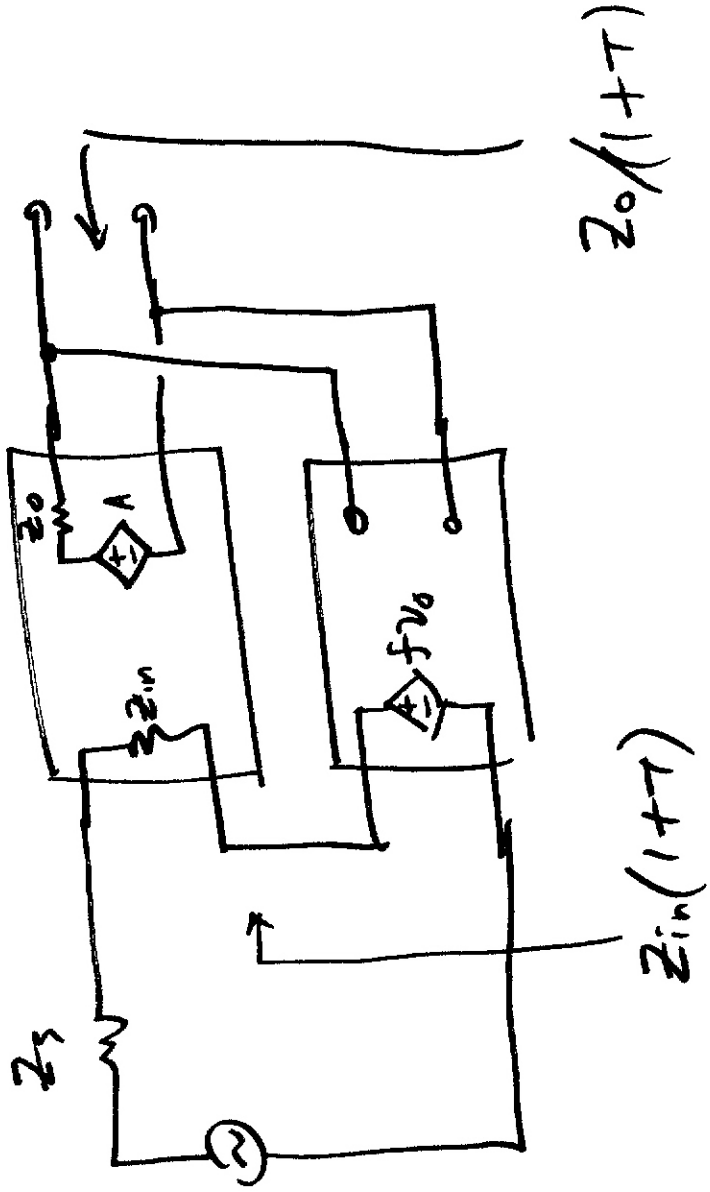
$$= \frac{g_m \cdot R_F}{\left(\frac{R_F}{R_S} + \frac{R_F}{R_L} + \frac{R_F^2}{R_L R_S}\right)}$$

$$= \frac{g_m R_F}{\left(1 + \frac{R_F}{R_S}\right)\left(1 + \frac{R_F}{R_L}\right) \underbrace{(-1)}_{\leftarrow}}$$

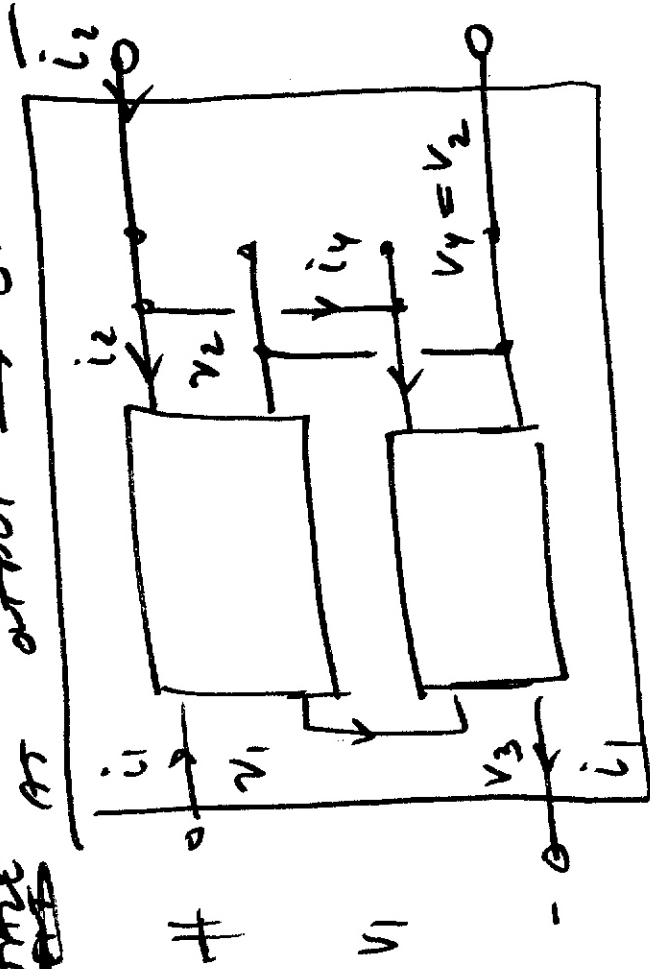
"LOADED" FB



VOLTAGE AMP \Rightarrow SERIES - SHUNT FB



VOLTAGE AT INPUT \Rightarrow SERIES
~~VOLTAGE~~ VOLTAGE AT OUTPUT \Rightarrow SHUNT



$$i_1 = i_3 = i_1 \quad \bar{v}_2 = v_2 = v_4$$

$$\bar{v}_1 = v_1 + v_3 \quad \bar{i}_2 = i_2 + i_4$$

$$\begin{pmatrix} v_1 \\ i_2 \end{pmatrix} = A \cdot \begin{pmatrix} i_1 \\ v_2 \end{pmatrix}$$

$$v_1 = h_{11} i_1 + h_{12} v_2$$

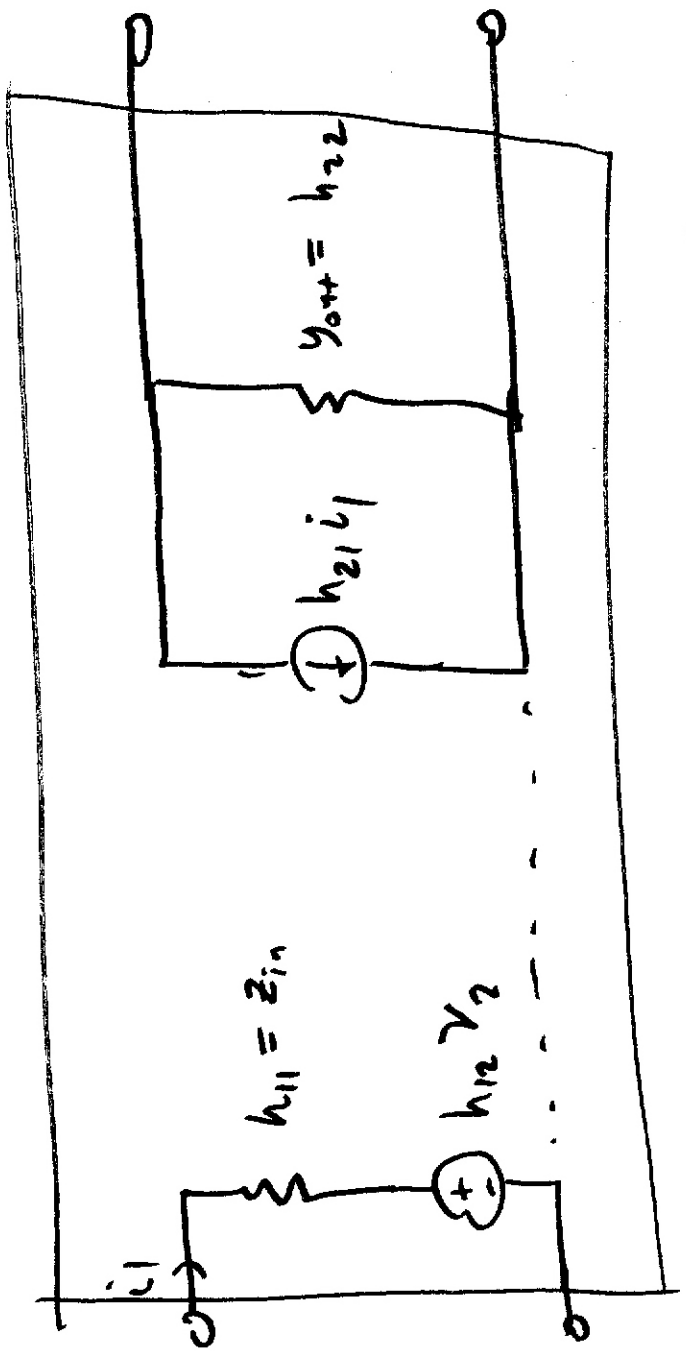
$$i_2 = h_{21} i_1 + h_{22} v_2$$

$$h_{11} = \frac{v_1}{i_1} \Big|_{v_2=0} \quad \text{SHORT CIRCUIT INPUT IMPEDANCE}$$

$$h_{21} = \frac{i_2}{i_1} \Big|_{v_2=0} \quad \text{SHORT CIRCUIT CURRENT GAIN}$$

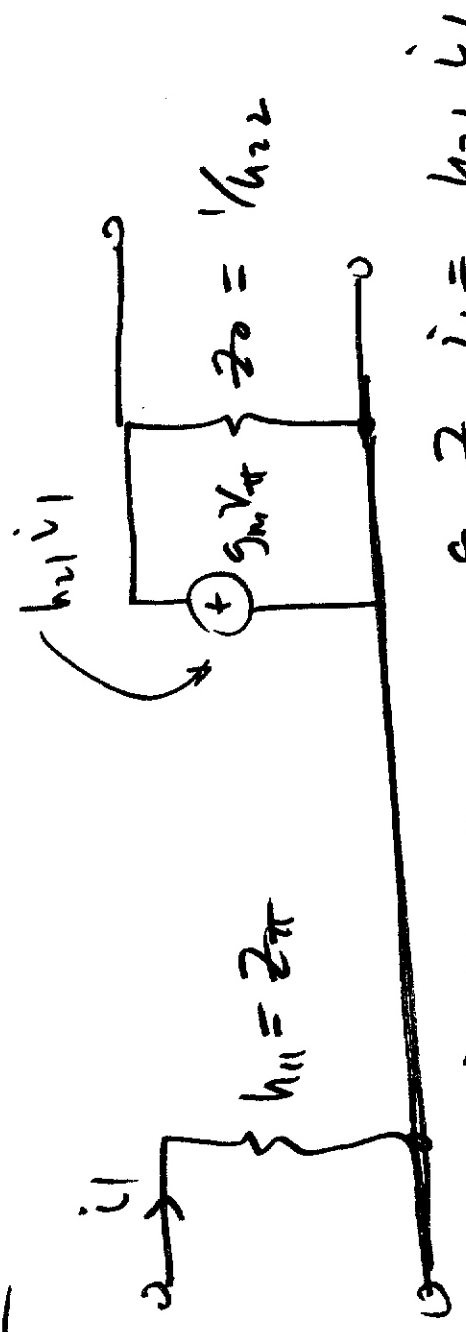
$$h_{12} = \frac{v_1}{v_2} \Big|_{i_1=0} \quad \text{REVERSE VOLTAGE GAIN OPEN CIRCUIT}$$

$$h_{22} = \frac{i_2}{v_2} \Big|_{i_1=0} \quad \text{OPEN CIRCUIT OUTPUT ADMITTANCE}$$



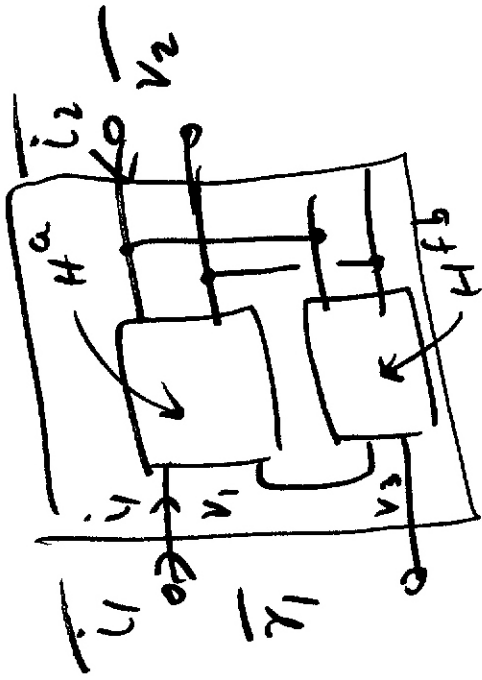
UNILATERAL AMP

TRANSISTOR $h_{12} \approx 0$



$$g_m \gamma_{\pi} = i_1 \cdot Z_{\pi} \cdot \gamma_m = g_m Z_{\pi} \quad i_1 = h_{21} i_1$$

$$h_{21} = g_m Z_{\pi} = \beta$$

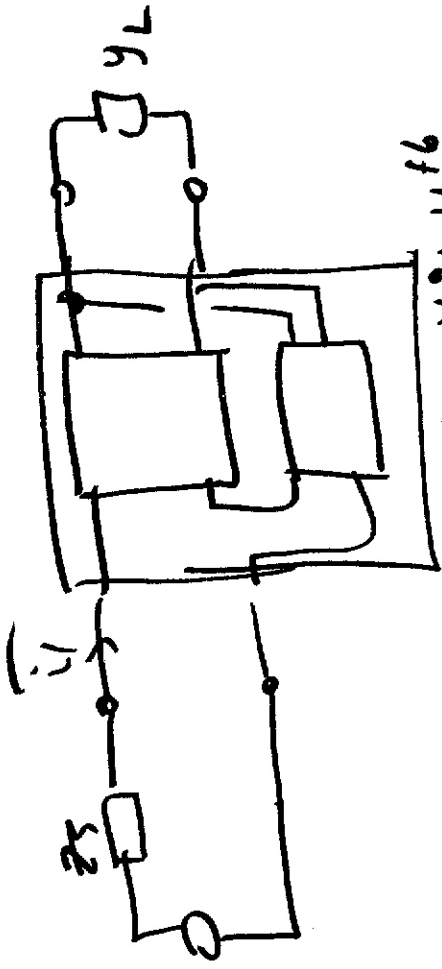


$$\begin{pmatrix} v_1 \\ i_1 \end{pmatrix} = H^{amp} \cdot \begin{pmatrix} i_1 \\ v_2 \end{pmatrix}$$

$$\begin{pmatrix} v_3 \\ i_4 \end{pmatrix} = H^{fb} \cdot \begin{pmatrix} i_3 = i_1 \\ v_4 = v_2 \end{pmatrix}$$

$$\begin{pmatrix} v_1 + v_3 \\ i_2 + i_4 \end{pmatrix} = (H^{amp} + H^{fb}) \begin{pmatrix} i_1 \\ v_2 \end{pmatrix}$$

$$\begin{pmatrix} v_1 \\ i_2 \end{pmatrix} = H \begin{pmatrix} i_1 \\ v_2 \end{pmatrix}$$



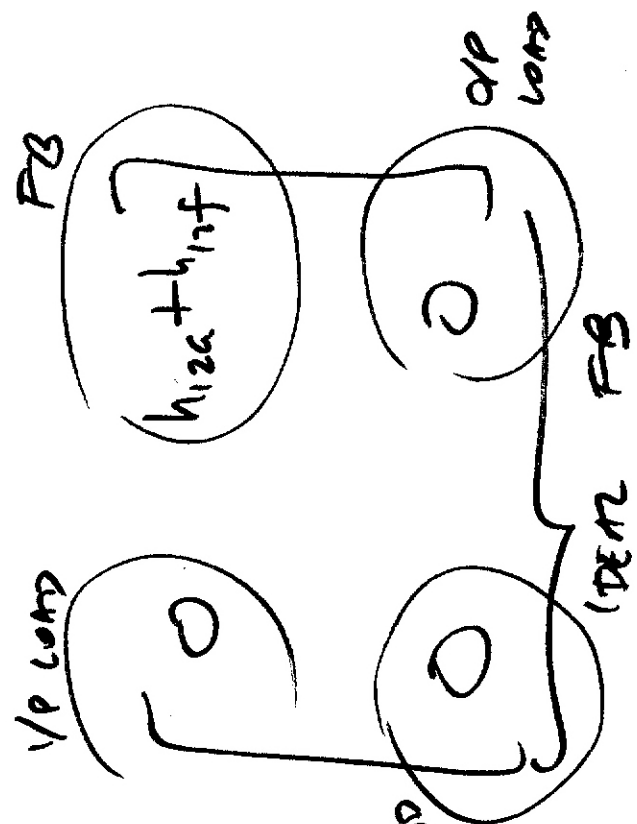
$$H = H_{21} + H_{11} Y_L$$

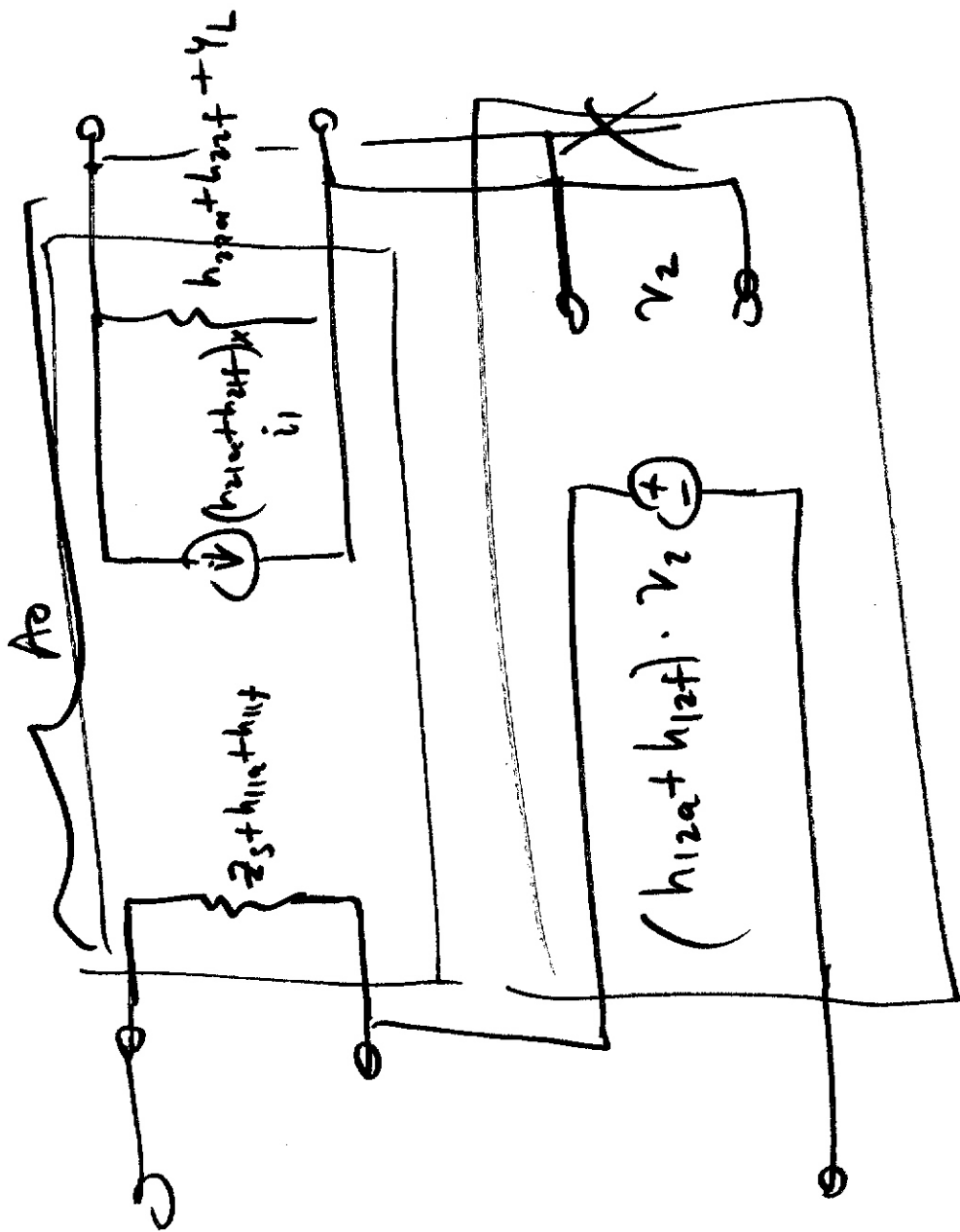
$$V_2 = (Z_s + h_{11a} + h_{11f}) \bar{I}_1 + (h_{12a} + h_{12f}) \bar{V}_2$$

$$0 = (h_{21a} + h_{21f}) \bar{I}_1 + (Y_L + h_{22a} + h_{22f}) \bar{V}_2$$

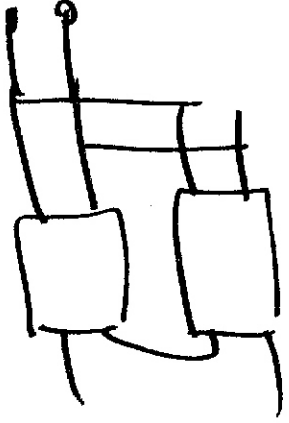
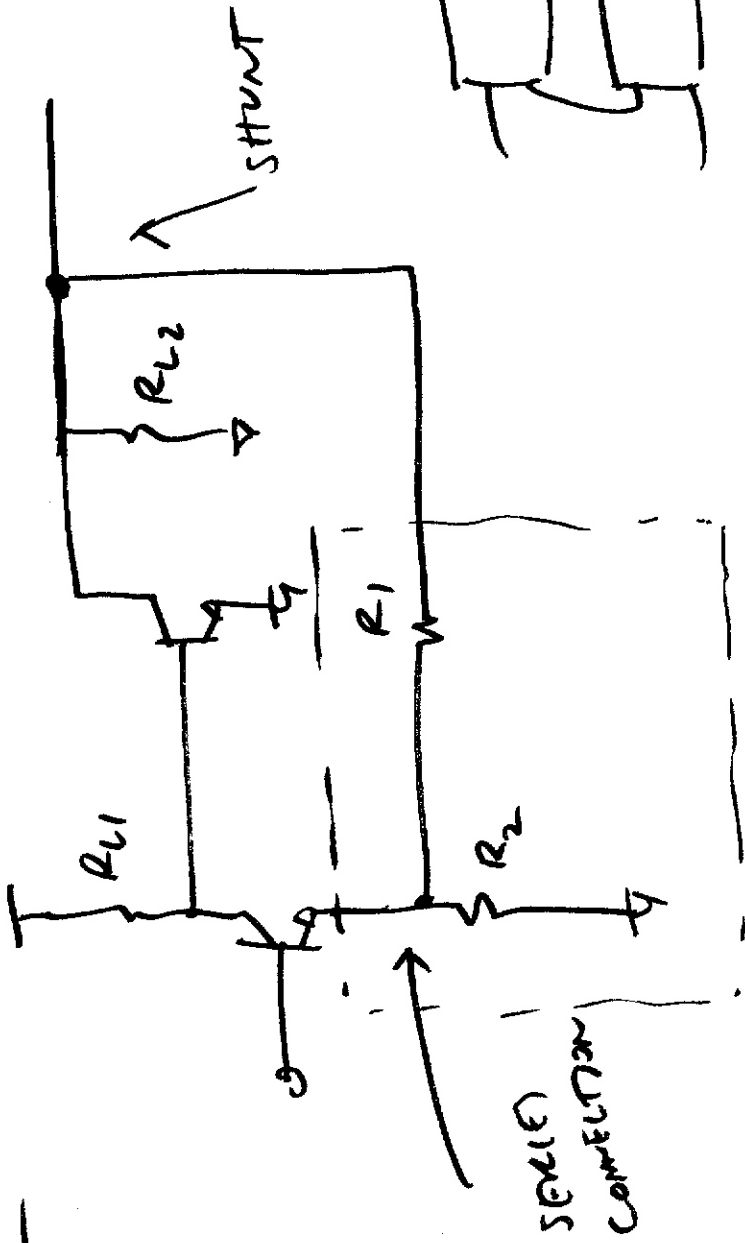
$$H = \begin{bmatrix} Z_s + h_{11a} + h_{11f} & 0 \\ h_{21a} + h_{21f} & Y_L + h_{22a} + h_{22f} \end{bmatrix} + \text{FB}$$

IDEAL UNILATERAL AMP





EX



VOLTAGE - DIVIDER
SERIES - SHUNT
✓ OPEN
→ START

$$h_{11fb} = R_1 \parallel R_2$$

$$h_{22fb} = (R_1 + R_2)^{-1}$$

