

## Smith Chart<sup>†</sup> notes

1. A graphical method of solution for T-line calculations (and avoid calculations with complex numbers and exponentials)
2. A graphical method for passive network calculations
  - a) matching
  - b) impedance transformation
3. A graphical method for amplifier and oscillator design
  - a) bilinear transformation (circles mapping into circles)
  - b) preservation of matching theorem
  - c) signal flow analysis of circuits

<sup>†</sup>Philip H. Smith from Bell Labs. "Transmission-line calculator," *Electronics*, vol. 12, p.29, January 1939. and "An improved transmission line calculator," *Electronics*, vol. 17, p. 130, January 1944.

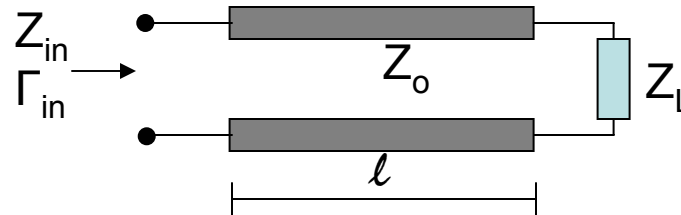
"Electronic Applications of the Smith Chart: in waveguide, circuit and component analysis," P.H. Smith, Krieger Publishing Co., 1983

## Preliminaries

a) 1-to-1 correspondence between  $Z$  and  $\Gamma$

$$Z = (1 + \Gamma) / (1 - \Gamma)$$

$$\Gamma = (Z - 1) / (Z + 1)$$



b) T.Line problems involve analysis of how  $\Gamma$  (or  $Z$ ) varies along the line with distance from load or generator

c) Amplifiers and oscillator designs follow the procedure:

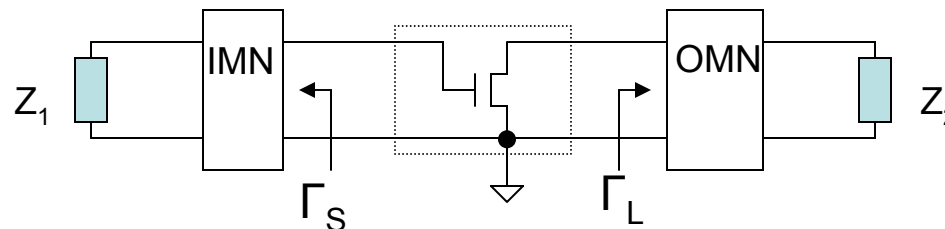
- get

(i) transistor data [S] (and Noise parameters)

(ii) required specifications for LNA or Oscillator

- Find  $\Gamma_S$  and  $\Gamma_L$  to attend specifications

- Realize  $\Gamma_S$  and  $\Gamma_L$  from known source and load impedances



## Bilinear Transformations

In a complex plane, a circle with center at  $(x_o, y_o)$  and radius  $R$  is described by

$$(x-x_o)^2 + (y-y_o)^2 - R^2 = 0$$

or

Now, let  $Z = x+jy$ ,  $Z_o = x_o+jy_o$ . The circle equation can be written as

$$|Z-Z_o|^2 - R^2 = 0 \quad \longleftarrow \quad \text{compact}$$

or

$$ZZ^* - ZZ_o^* - Z^*Z_o + (Z_oZ_o^* - R^2) = 0 \quad \longleftarrow \quad \text{more useful for inspection}$$

by inspection we will want to find  $Z_o$  and  $R$  in new expressions

Recall circle equation:

$$ZZ^* - ZZ_o^* - Z^*Z_o + (Z_oZ_o^* - R^2) = 0$$

4

Consider the bilinear transformation:

$$W = (AZ + B) / (CZ + D)$$

$A, B, C, D$  are complex constants.  $W$  and  $Z$  are complex variables.

- (i) This transformation will map circles in the  $Z$ -plane into circles in the  $W$ -plane.
- (i) Straight lines are limiting cases.

**Case 1)** Let  $|W|^2 = \rho^2$  or  $WW^* - \rho^2 = 0$ ; a circle centered at the origin.

Using the transformation, we get:

$$(AZ + B) / (CZ + D) (A^*Z^* + B^*) / (C^*Z^* + D^*) - \rho^2 = 0$$

Expanding:

$$ZZ^*(AA^* - \rho^2CC^*) - Z(\rho^2CD^* - AB^*) - Z^*(\rho^2C^*D - A^*B) + BB^* - \rho^2DD^* = 0$$

By comparison, this is a circle with center (coefficient of “ $-Z^*$ ”):

$$Z_o = (\rho^2C^*D - A^*B) / (AA^* - \rho^2CC^*) = (\rho^2C^*D - A^*B) / (|A|^2 - \rho^2|C|^2)$$

Radius is found from constant term that is “ $(Z_oZ_o^* - R^2)$ ”:

$$R^2 = Z_oZ_o^* - (|B|^2 - \rho^2|D|^2) / (|A|^2 - \rho^2|C|^2) \Rightarrow R = \rho(|AD - BC|) / (|A|^2 - \rho^2|C|^2)$$

**Case 2)** Let  $|W-W_o|^2 = \rho^2$ ; a circle centered at  $W_o$ .

Then:

$$W-W_o = (AZ+B)/(CZ+D) - W_o = [(A-CW_o)Z + (B-DW_o)] / (CZ+D)$$

We make  $A' = A - CW_o$ ;  $B' = B - DW_o$ , and reuse the equations of case 1.  
Thus making  $Z$  also describe a circle.

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Many amplifier design relations involves bilinear transformations.  
Example: input coefficient of reflection ( $\Gamma_{in}$ ) as a function of the load ( $\Gamma_L$ )

$$\Gamma_{in} = (\Delta \Gamma_L - S_{11}) / (S_{22} \Gamma_L - 1)$$

$$\Delta = S_{11} S_{22} - S_{12} S_{21}$$

## Smith chart “r” and “x” circles

Given a lossless T.line with characteristic impedance  $Z_o=R_o$ , terminated by an impedance  $Z_L$ , we write

$$\Gamma = \Gamma_r + j\Gamma_i = (Z_L - R_o)/(Z_L + R_o)$$

Which after normalization by  $R_o$ , leads to

$$\Gamma = \Gamma_r + j\Gamma_i = (z_L - 1)/(z_L + 1)$$

where  $z_L = Z_L/R_o$

Therefore:

$$z_L = r + jx = (1 + \Gamma)/(1 - \Gamma) = [(1 + \Gamma_r) + j\Gamma_i]/[(1 - \Gamma_r) - j\Gamma_i]$$

And, after multiplying numerator and denominator by complex conjugate of denominator, we reach

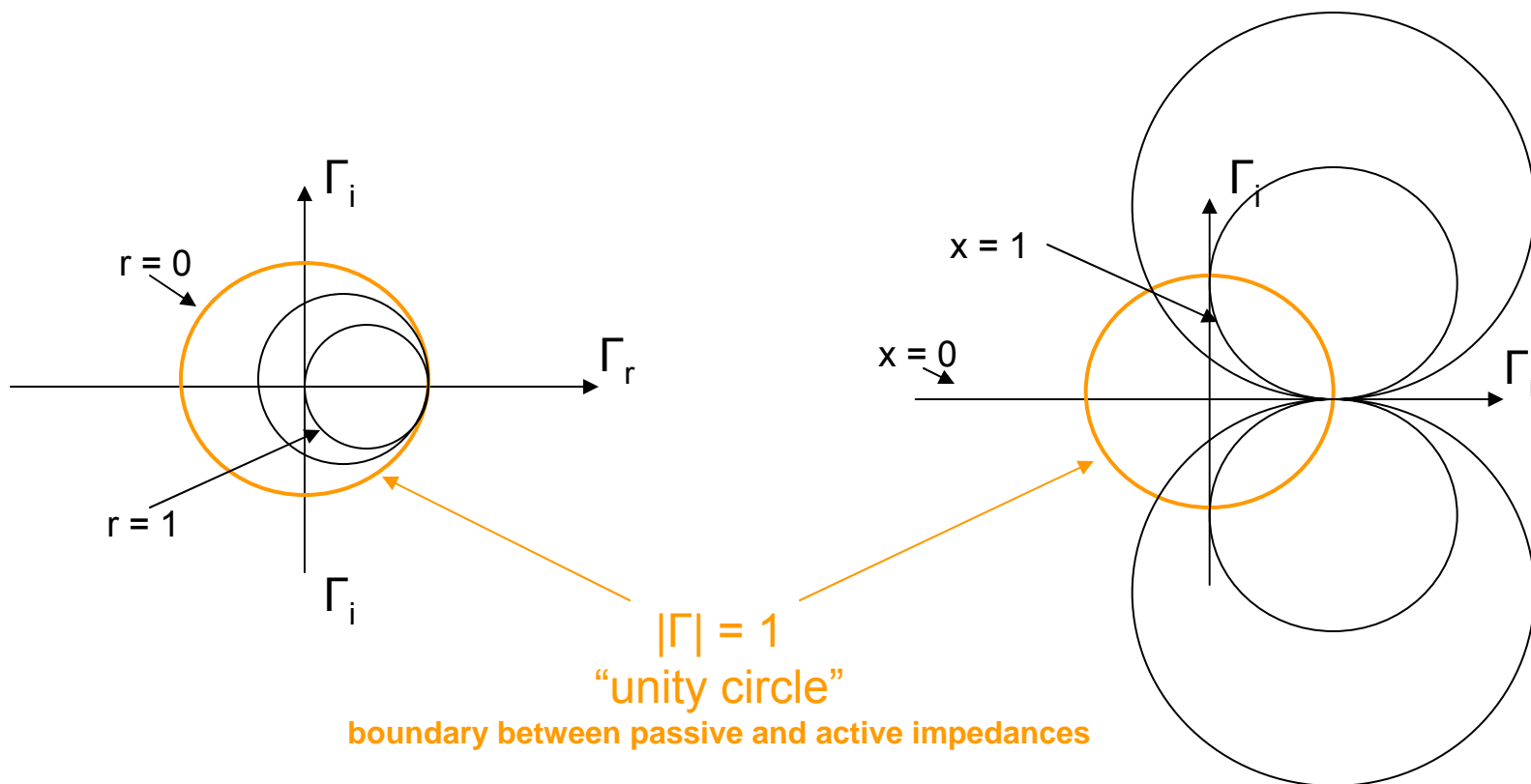
$$r = (1 - \Gamma_r^2 - \Gamma_i^2)/[(1 - \Gamma_r)^2 + \Gamma_i^2]$$

$$x = 2\Gamma_i/[(1 - \Gamma_r)^2 + \Gamma_i^2]$$

## Smith chart “r” and “x” circles ... cont.

Then, circles in the  $\Gamma$ -plane parameterized by “r” and “x” are:

$$[\Gamma_r - r/(r+1)]^2 + \Gamma_i^2 = [1/(1+r)]^2 \quad \text{and} \quad (\Gamma_r - 1)^2 + (\Gamma_i - 1/x)^2 = (1/x)^2$$

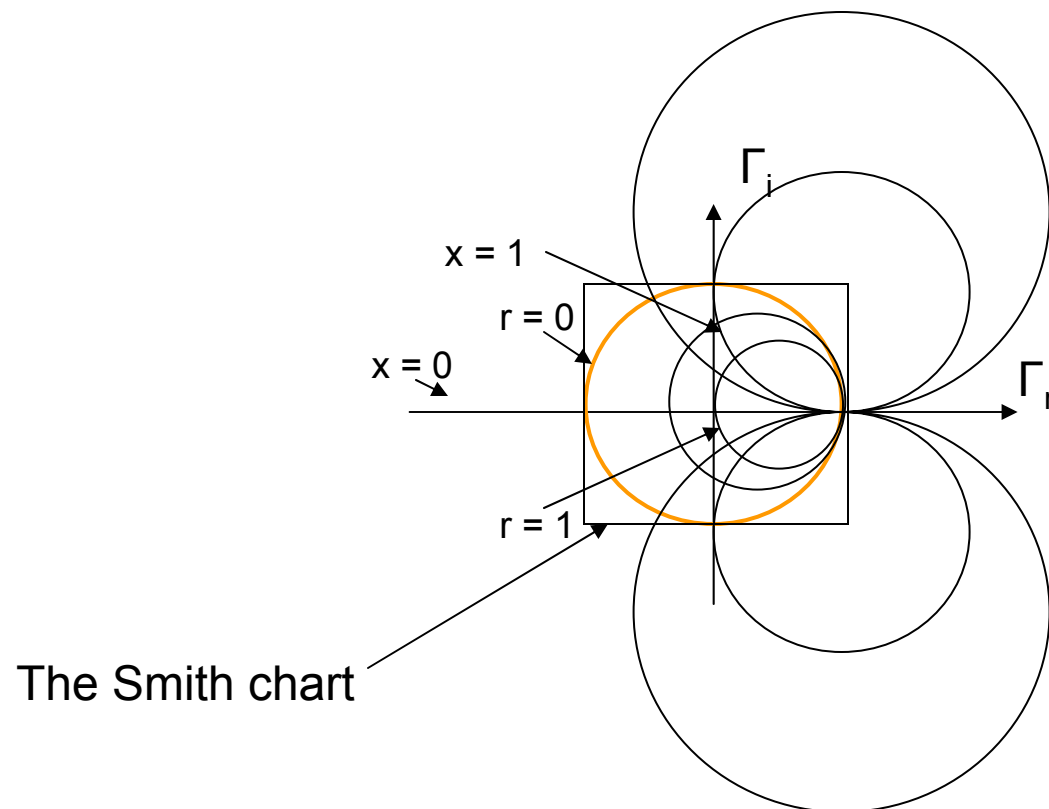


## Smith chart “r” and “x” circles ... cont.

8

The Smith chart for  $|\Gamma|$  less or equal to 1 (unity circle) represents all the passive impedances. Values of  $\Gamma$  higher than 1 require power gain and represent impedances that can only be produced by active devices.

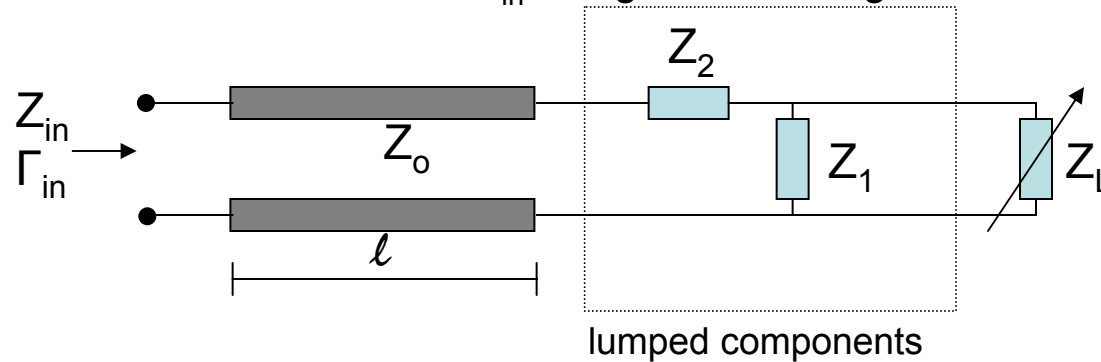
Overlaying  $\Gamma$  circles parameterized by “r” and “x” leads to the Smith chart below.





## Example of Smith chart methods: solving a problem

An engineer makes measurements for  $Z_{in}$  using the following network



The lumped-components box has fixed impedances  $Z_1$  and  $Z_2$ .

All these impedances are made of passive association of resistors, inductors and capacitors.

$Z_L$  is a variable impedance created by moving a short along a lossless T.line stub. A piece of lossless T.line of length,  $l$ , transforms the impedance from the lumped component box to the  $Z_{in}$  impedance to be measured.

4 measurements were made for  $Z_{in}$  for 4 different values of  $Z_L$ , and they resulted:

$$Z_{in}(1) = 0.290 + j0.420$$

$$Z_{in}(2) = 0.026 + j0.174$$

$$Z_{in}(3) = 0.130 + j0.690$$

$$Z_{in}(4) = 0.362 - j0.045$$

When the engineer showed the 4 results to his manager, his manager replied one of the measurements was wrong. How can he tell and which is the wrong one?