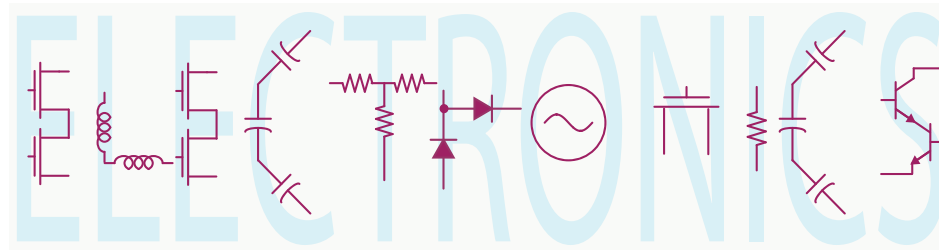


EE 42/100

Lecture 5: Analyzing a Complex Circuit: Nodal Analysis



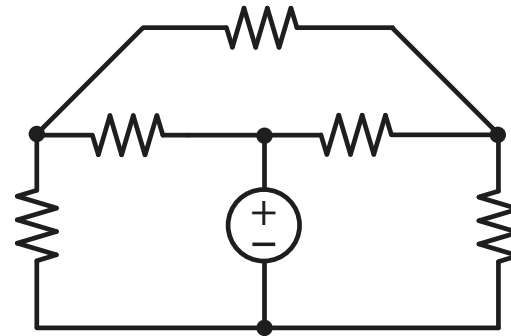
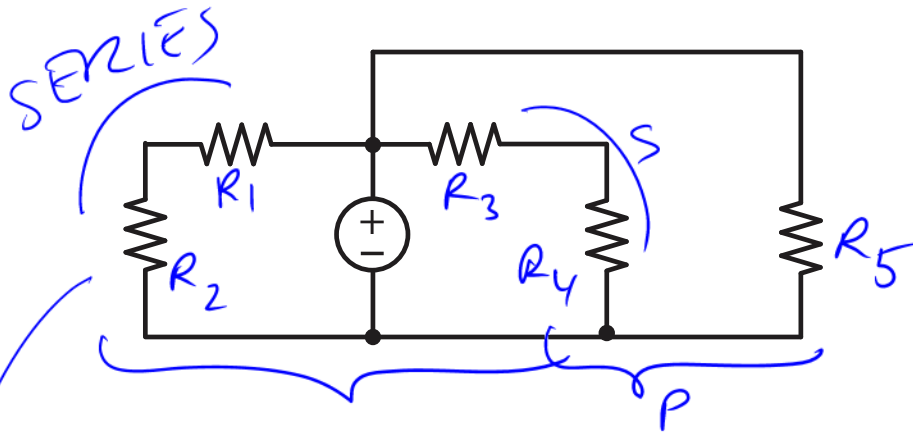
Rev B 1/30/2012 (8:56PM)

Prof. Ali M. Niknejad

University of California, Berkeley

Copyright © 2012 by Ali M. Niknejad

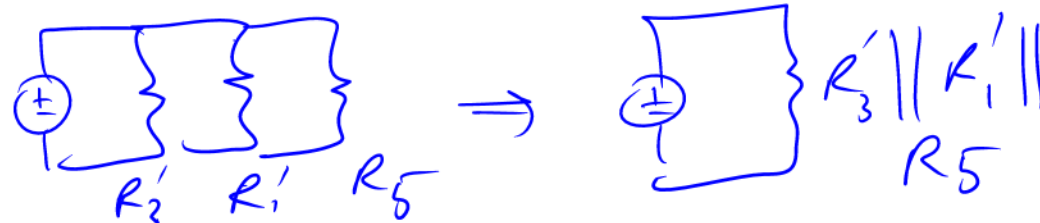
Analyzing a Complex Network



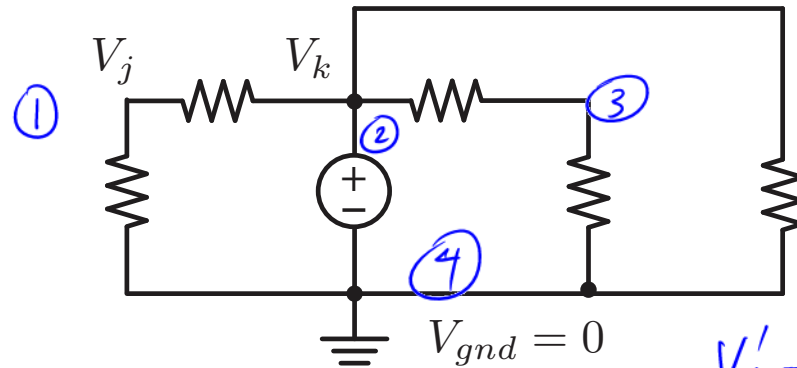
- Simple circuit can be solved using repeated applications of series-parallel formulas and current/voltage dividers (left schematic). Next lecture we'll learn a few more tricks to add to our toolbox.
- For now we'd like to develop a systematic methodology to solve for the currents and voltages (and hence power) in any arbitrary circuit (right schematic).
- Nodal Analysis: Repeated application of KCL to each node of the circuit. It can be used to solve for all of the voltages (and subsequently currents) in the circuit. This will be our prime analysis technique in this class.
- Mesh and Loop Analysis: Repeated application of KVL can be used to find the currents (and subsequently voltages) in a circuit. In this class we will not use mesh/loop analysis.

$$R_1' = R_1 + R_2$$

$$R_3' = R_3 + R_4$$



Identifying the Reference Node



$$V'_1 = V_{14} = V_1 - V_4$$

GND

$$V'_2 = V_{24} = V_2 - V_4$$

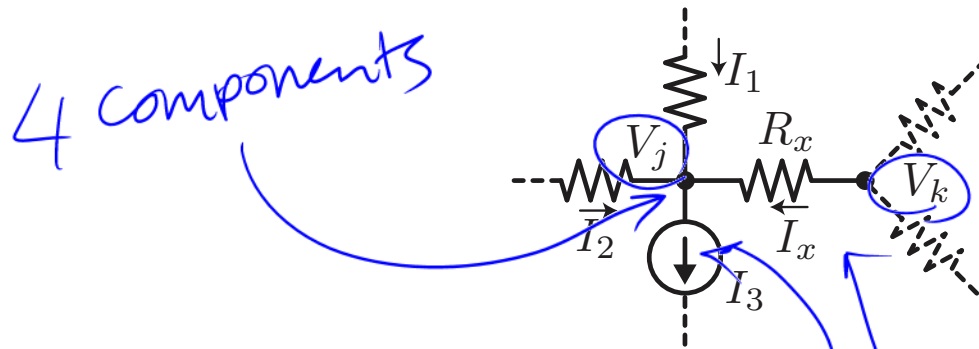
$$V'_1 - V'_2 = V_1 - V_4 - (V_2 - V_4) = V_1 - V_2$$

- Recall that voltage is defined as a quantity that measures the potential difference between two nodes in a circuit, V_{AB} .
- We can arbitrarily pick one node of the circuit and define all *node voltages* in reference to this node. Call this node *ground*, or node '0'. In other words, define V_k as the node voltage at node k which is the energy gained per unit charge as it moves from node *gnd* to node k , or in more cumbersome notation, $V_{k,gnd}$.
- If we subtract the two node voltages, we get

$$V_{j,gnd} - V_{k,gnd} = V_j - V_{gnd} - (V_k - V_{gnd}) = V_j - V_k = V_{j,k}$$

- In other words $V_{j,k} = V_{j,gnd} - V_{k,gnd}$, which makes sense since they are defined with respect to the same reference. Note that the reference potential is by definition at zero potential, $V_{gnd} = 0$.

Node Equations for Resistive Branches



- Since the potential at the ground node is known, only $n - 1$ unknown node voltages remain. Writing KCL at each other node results in an equation in the following form

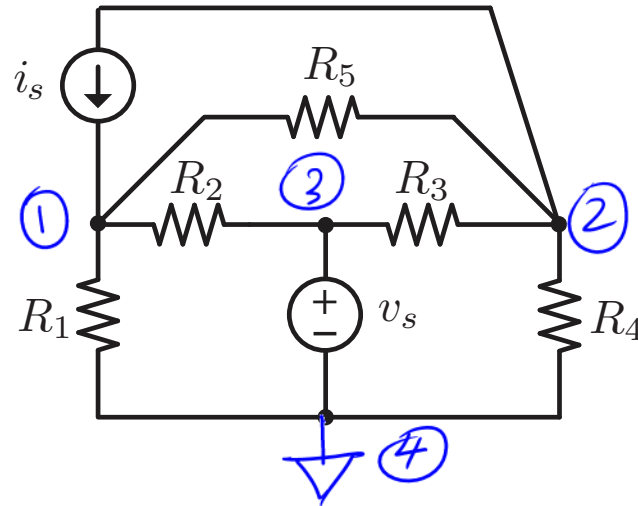
$$I_1 + I_2 - I_3 + I_x = 0$$

- In a resistive branch, the current can be written in terms of the node voltages. If current I_k flows from node a to node b , it's given by

$$I_x = \frac{V_k - V_j}{R_x} = G_x(V_k - V_j)$$

- If an independent current source is connected to the node, then the current is known.

KCL Example 1



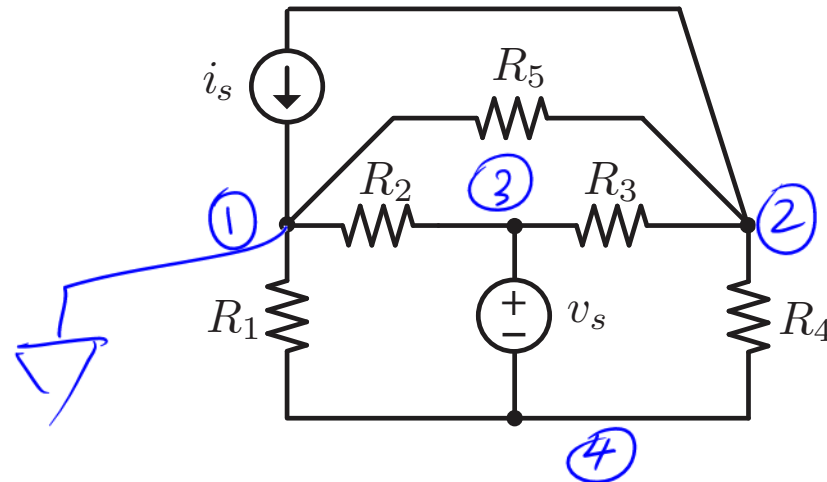
$$V_4 = 0V$$
$$V_3 = V_5$$

2 UNK

V_1 & V_2

- We are now in a position to solve many circuit problems. For example, in the above circuit we proceed as follows.
- First we choose the reference ground potential at the negative terminal of the voltage source. Why? Because then we eliminate one unknown node voltage from the circuit. The node connected to the positive terminal of the source is at a voltage of v_s .
- We have eliminated two nodes from the list of unknowns. Now there are only two nodes left in the circuit.

KCL Example 1



$$V_1 = 0$$

$$V_2 = ?$$

$$V_3 = ?$$

$$V_4 = ?$$

- We are now in a position to solve many circuit problems. For example, in the above circuit we proceed as follows.
- First we choose the reference ground potential at the negative terminal of the voltage source. Why? Because then we eliminate one unknown node voltage from the circuit. The node connected to the positive terminal of the source is at a voltage of v_s .
- We have eliminated two nodes from the list of unknowns. Now there are only two nodes left in the circuit.

$$\frac{V_1}{R_1} + \frac{V_1 - V_5}{R_2} + \frac{V_1 - V_2}{R_5} - \dot{V}_5 = 0$$

KCL (2):

$$\frac{V_2}{R_4} + \frac{V_2 - V_5}{R_3} + \frac{V_2 - V_1}{R_5} + \dot{V}_5 = 0$$

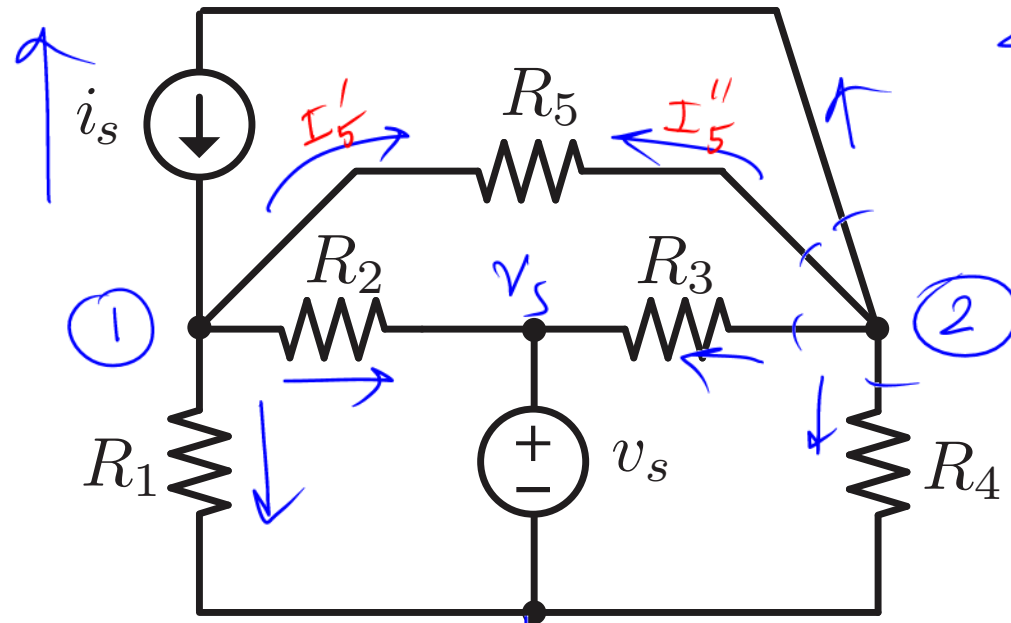
$$I_5'' = -I_5'$$

$$V_1 \left(\frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_5} \right) + V_2 \left(-\frac{1}{R_5} \right) = \dot{V}_5 + \frac{V_5}{R_2}$$

$$V_1 \left(-\frac{1}{R_5} \right) + V_2 \left(\frac{1}{R_4} + \frac{1}{R_3} + \frac{1}{R_5} \right) = -\dot{V}_5 + \frac{V_5}{R_3}$$

$$\begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} b_1 \\ b_2 \end{bmatrix}$$

Example 1 KCL Equations



2 UNK:
 $v_1 + v_2$

KCL ①:

$$\frac{v_1}{R_1} + \frac{v_1 - v_5}{R_2} + \frac{v_1 - v_2}{R_5} + (-i_s) = 0$$

KCL ②:

$$\frac{v_2}{R_4} + \frac{v_2 - v_5}{R_3} + \frac{v_2 - v_1}{R_5} + i_s = 0$$

$I_5'' = -I_5'$

KCL Example 1 (cont)

- For each node we write KCL equations. We setup two equations with two unknowns.
- It's good to write these equations in standard form. Put the unknowns on the left hand side and the known currents (due to the independent sources) on the right hand side. Then we have a matrix equation

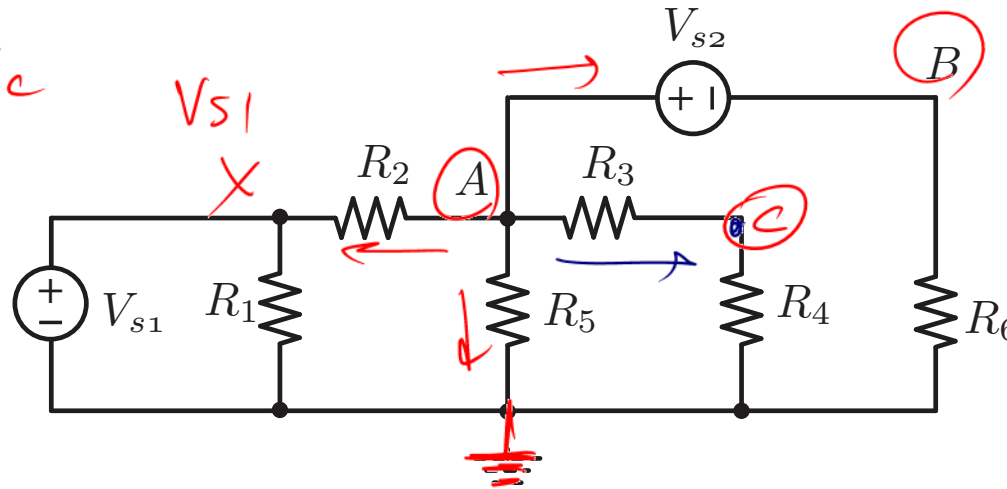
$$Av = b$$

which we solve by matrix inversion (Gaussian elimination, Cramer's rule, matlab, etc.)

$$v = A^{-1}b$$

Dealing with "Floating" Voltage Sources

PROBLEM:
 4 UNK (V_A, V_B, V_C, I_{S2})
 3
 I_{S2}
 ③ EQ BY KCL?



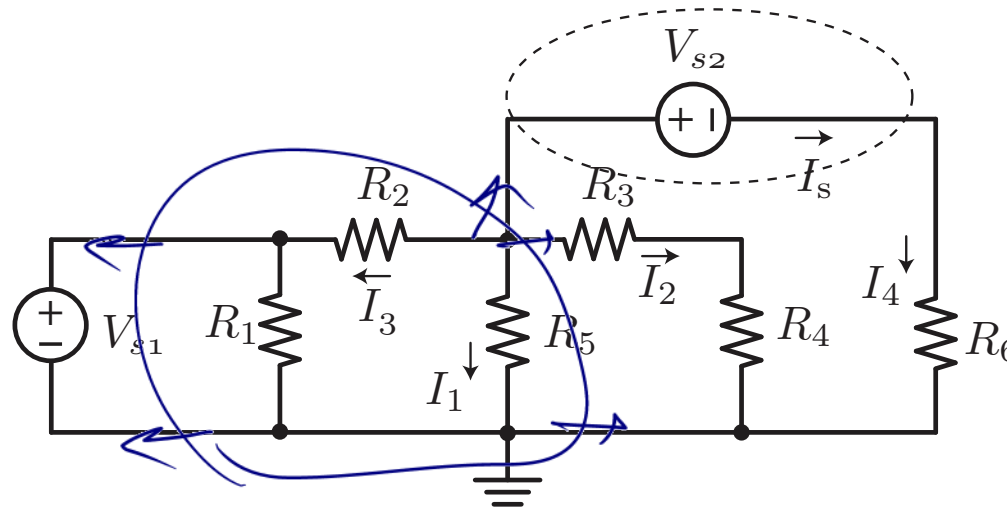
$V_A - V_B = V_{S2}$
 V_A & V_B ARE NOT IND.

- In the above example, two voltage sources appear so that we cannot label both negative terminals as ground. So we pick one.
- In this circuit, the number of unknowns is smaller because if we know the voltage at one node connected to the voltage source, the voltage at the other has a fixed relation, since $V_{AB} = V_s$.
- But in writing down KCL at one of the nodes, we encounter a problem. The current through the voltage source can take on any value, which means that other circuit elements determine the current through it.

KCL (A) : $\frac{V_A}{R_5} + \frac{V_A - V_{S1}}{R_2} + \frac{V_A - V_C}{R_3} + I_{S2} = 0$

UNK

KCL at a “Super Node”



- But note that if we write the KCL equations for both terminals of the voltage source, this unknown current appears twice.

$$\text{At the positive terminal: } I_1 + I_2 + I_3 + I_s = 0$$

$$\text{At the negative terminal: } I_4 - I_s = 0$$

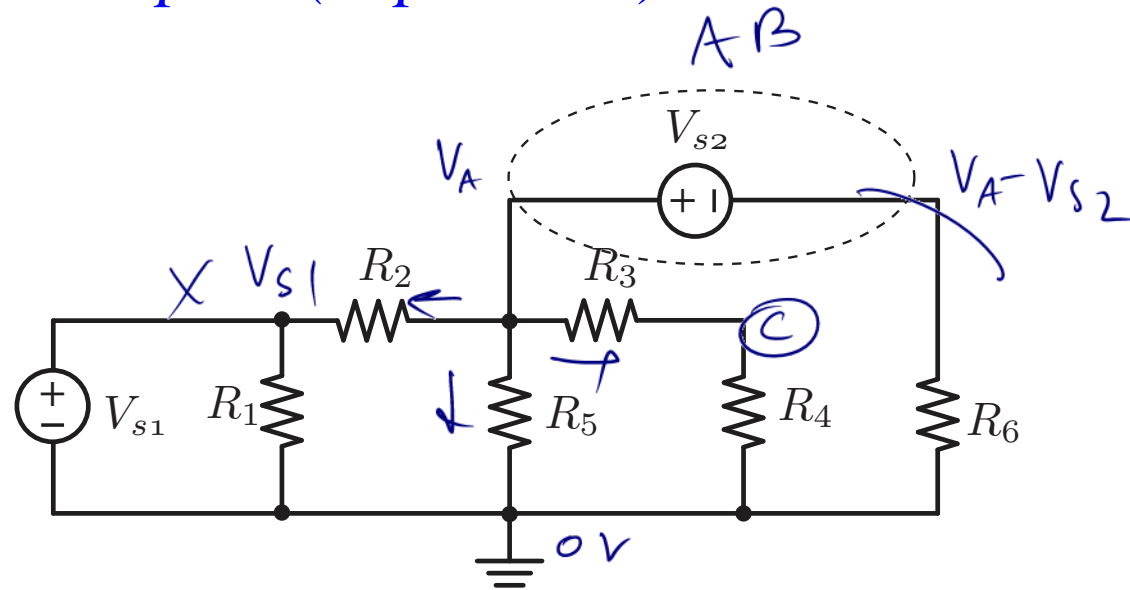
SUPER NODE

- If we add these two equations, I_s cancels out

$$I_1 + I_2 + I_3 + I_4 = 0$$

- This is an independent equation we can use. It's actually KCL for a “super node”, which is what we call nodes a and b together. We have just shown that current continuity applies to a node and also to a super node.

KCL Example 2 (Super Node)



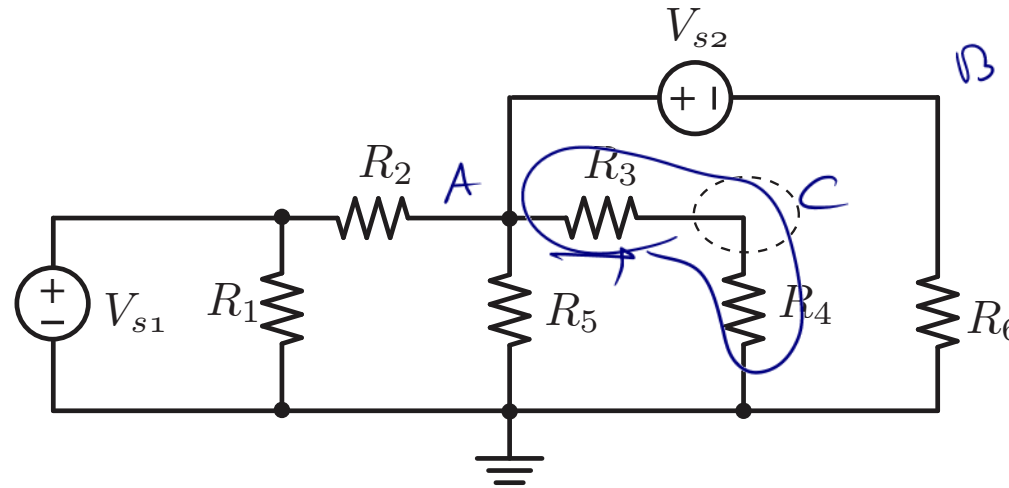
- Using the steps that we have learned, we first identify a ground node at a convenient location (negative terminal of a source). Then we identify two super nodes in the circuit. For each super node we write KCL, put the equation into standard form, and solve.

KCL @ \textcircled{AB}

$$\frac{V_A - V_{s1}}{R_2} + \frac{V_A}{R_5} + \frac{V_A - V_C}{R_3} + \frac{V_A - V_{s2}}{R_6} = 0$$

$\frac{V_A}{R_3 + R_4}$

Elimination Trivial Nodes



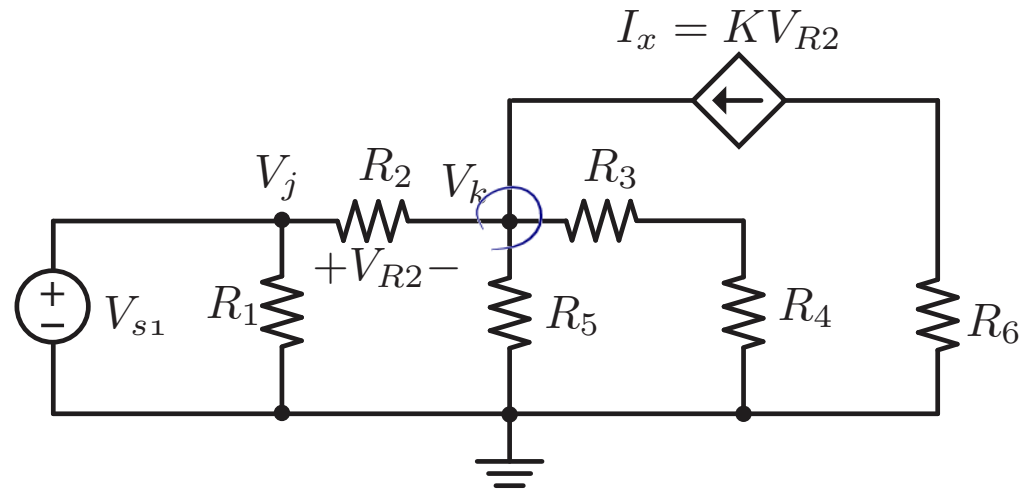
- Any node with less than three elements is in some sense trivial. That's because we can find the node voltage for such a node from the branch current. Thus, it's smart to avoid writing equations for these nodes and to deal with them later.
- In the above example the number of unknowns has been reduced from 2 to 1 by using this technique

$$\frac{V_{AC}}{R_3} = \frac{V_{A,0}}{R_3 + R_4}$$

$$V_C = \frac{R_4}{R_3 + R_4} V_A$$

$$V_B = V_A - V_{s2}$$

Dependent Sources

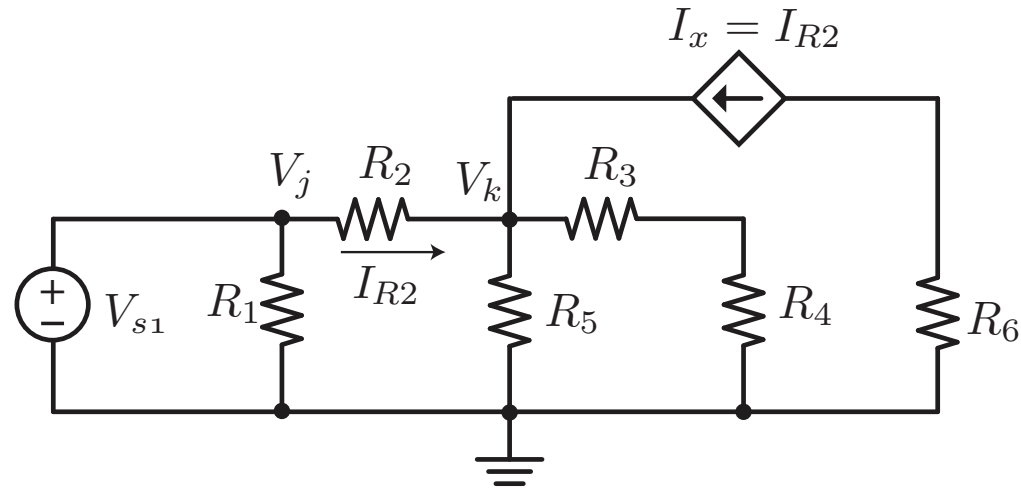


- Dependent sources require a bit more work but are generally dealt with in the same way. In the above circuit we initially treat the current through the dependent source as an unknown in writing KCL.
- There are now more unknowns than equations. For each additional unknown (dependent current), we can write an additional equation which relates the dependent current to the node voltages. For instance, for a VCCS, this is trivial

$$I_x = KV_{R2} = K(V_j - V_k)$$

$$\frac{V_k - V_j}{R_2} + \frac{V_k}{R_5} + \frac{V_k}{R_3 + R_4} - I_x = 0$$

Dependent Source (cont)

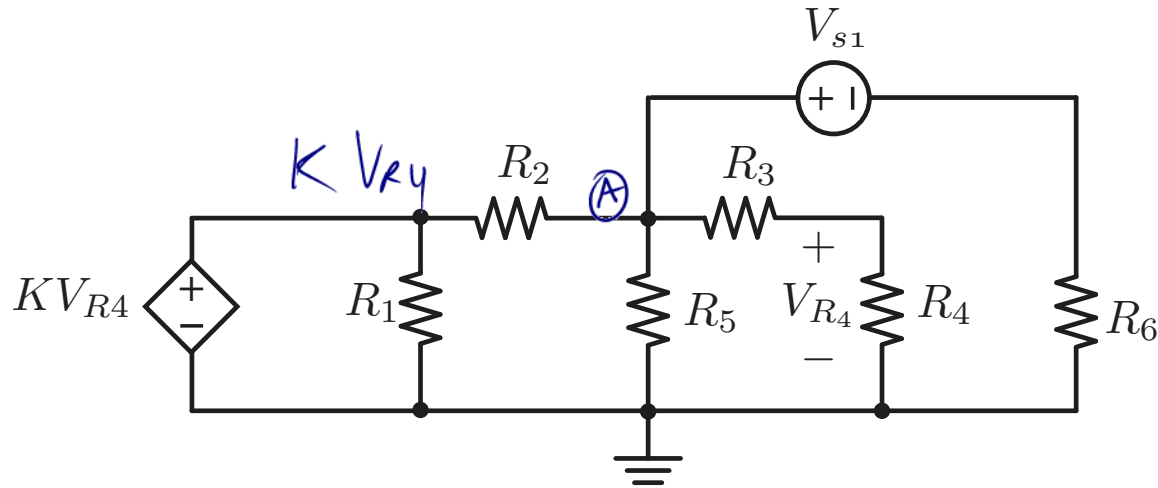


- For a CCCS, we simply need to calculate the current

$$I_x = JI_{R2} = J(V_j - V_k)/R_2$$

- Instead of making life more complicated by introducing new equations, we should actually just eliminate the unknown currents from our original set of equations. In other words, substitute the above equations for I_x and I_y , in our original $n - 1$ node equations.

Dependent Voltage Source

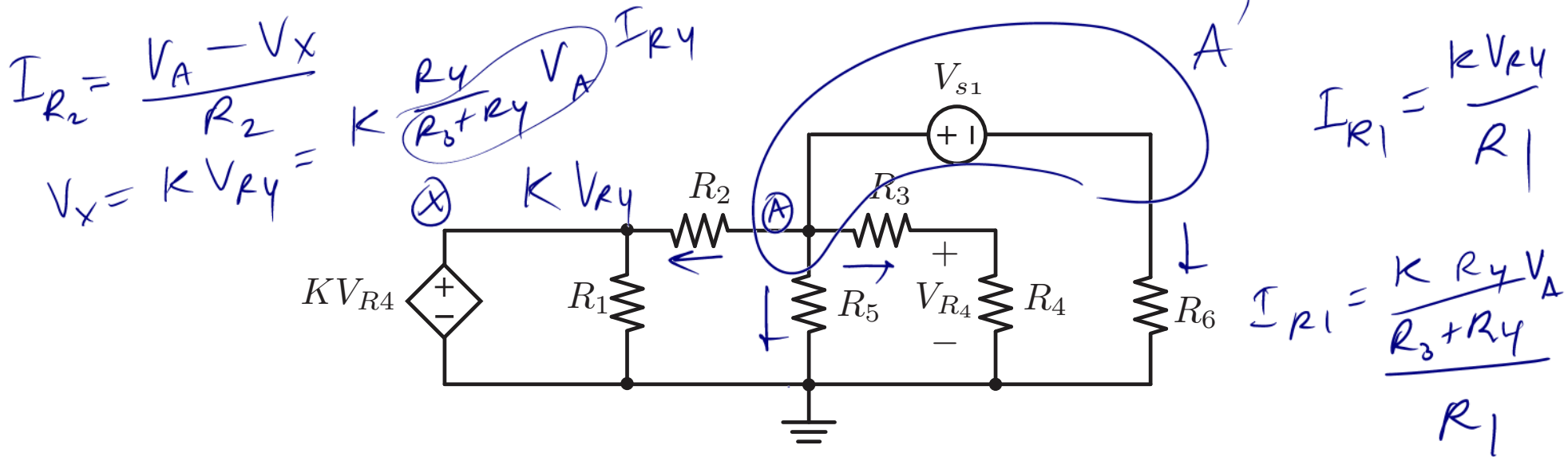


- Nodes with dependent voltage sources are handled in the same way. They can also form supernodes and a KCL equation can be written for the supernode, just like independent sources. The only difference is that the potential difference between the floating dependent voltage source is not known until all the equations are solved.

$$V_{R4} = I_4 \cdot R_4 = \frac{V_A}{R_3 + R_4} \times R_4 = \frac{R_4}{R_3 + R_4} V_A$$

$$KV_{R4} = \frac{K R_4}{R_3 + R_4} V_A$$

Dependent Voltage Source

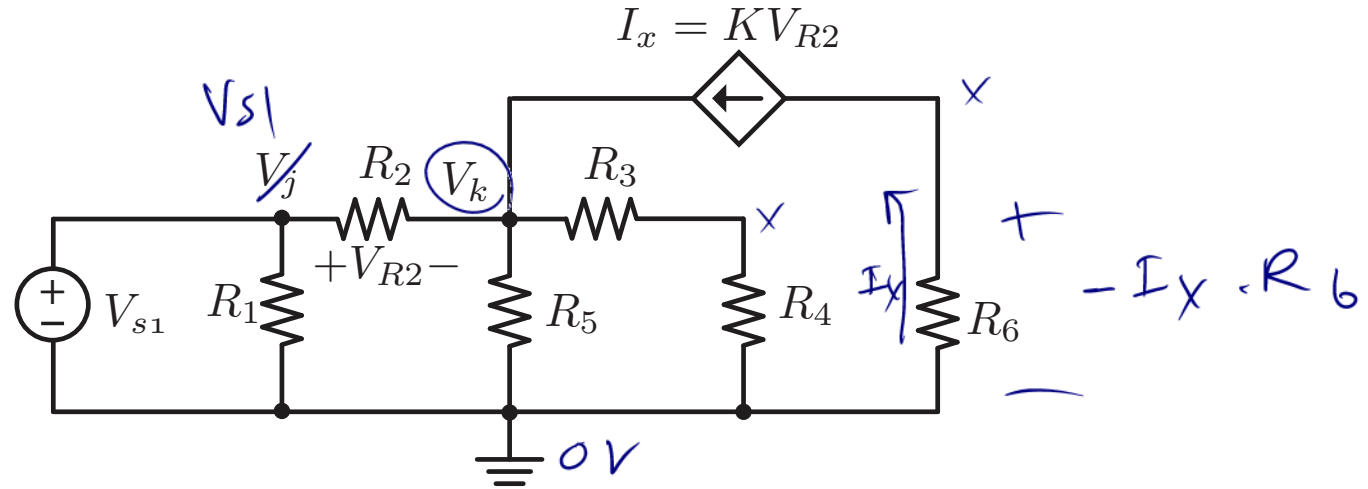


- Nodes with dependent voltage sources are handled in the same way. They can also form supernodes and a KCL equation can be written for the supernode, just like independent sources. The only difference is that the potential difference between the floating dependent voltage source is not known until all the equations are solved.

$$\text{KCL } A' : 0 = \underbrace{\left(V_A - \frac{K R_4}{R_3 + R_4} V_A \right)}_{V_X} \frac{1}{R_2} + \frac{V_A}{R_5} + \frac{V_A}{R_3 + R_4} + \frac{V_A - V_{S1}}{R_6}$$

$$K V_{R_4} = \frac{K R_4}{R_3 + R_4} V_A$$

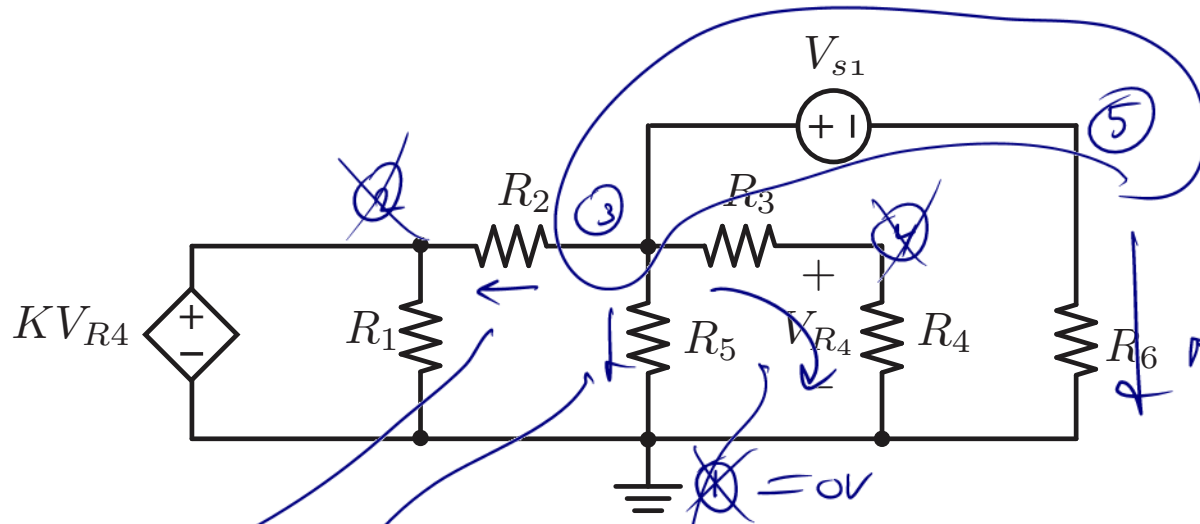
KCL Example 3 (Dependent I Source)



- In this example we start as always by defining the reference ground node, and then by writing node equations for all the remaining nodes.
- The only wrinkle is that the dependent current source, which introduces an extra unknown. To eliminate this extra unknown, we write additional equations expressing the unknown current in terms of the remaining node voltages.

$$\begin{aligned}
 \frac{V_k - V_{s1}}{R_2} + \frac{V_k}{R_5} + \frac{V_k}{R_3 + R_4} - I_x &= 0 && \text{2 unk} \\
 I_x = K V_{R2} = K (V_{s1} - V_k) &&& \text{1 unk} \\
 &&& \text{1 Eq}
 \end{aligned}$$

KCL Example 4: (Dependent V Source)



- This example involves a dependent voltage source. The solution procedure is nearly identical to the case without the dependent source, except that we write the auxiliary equation to eliminate the additional unknowns.

$$\frac{V_3 - kV_{R4}}{R_2} + \frac{V_3}{R_5} + \frac{V_3}{R_3 + R_4} + \frac{V_3 - V_{S1}}{R_6} = 0$$

$$V_{R4} = \frac{R_4}{R_3 + R_4} \cdot V_3$$