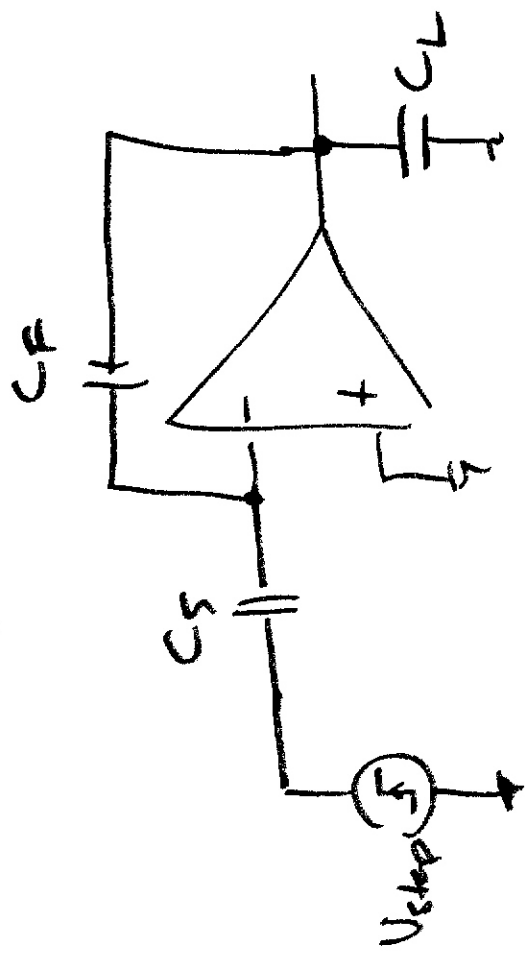


LECT 16 SETTLING TIME (CONT) PART II

POLE & ZERO

$$V_{o, \text{step}}(t) = -V_{\text{step}} \cdot C \left\{ 1 - \underbrace{\left(1 + \frac{f}{2}\right) e^{-t/\tau}}_{\text{DYNAMIC ERROR TERM}} \right\}$$



$$P = - \frac{f G_m}{C_{\text{eff}}}$$

$$Z = + \frac{G_m}{C_f}$$

$$\frac{P}{2} = 1 + \epsilon \quad V_{o, \text{step}}(t) = -V_{\text{step}} \cdot C \left\{ 1 - \epsilon e^{-t/\tau} \right\}$$

TWO CASES : I. $\left| \frac{F}{Z} \right| \ll 1$
 \rightarrow EFFECTIVE ZERO NOT THERE

II. $\left| \frac{F}{Z} \right| \sim 1 \rightarrow$ CANNOT NEGLECT ZERO

AMP SETTING

OPEN LOOP : $A(s) = \frac{A_0}{(1 + s/\omega_{p1})}$

$|A(j\omega_{ua})| = 1 \approx \frac{A_0}{s/\omega_{p1}} \Big|_{s=j\omega_{ua}}$

$\omega_{ua} \approx A_0 \cdot \omega_{p1}$

MIDBAND GAIN :

$A(s) = \frac{A_0 \omega_{p1}}{s} = \frac{\omega_{ua}}{s}$

CLOSED LOOP

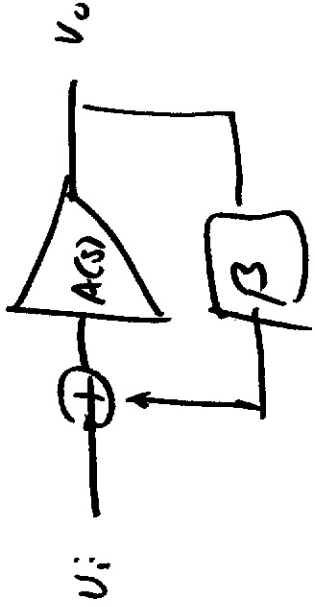
$$A_{cl} = \frac{A(s)}{1 + \beta A(s)}$$

MIDBAND

$$A_{cl} = \frac{\omega_{ua}/s}{1 + \beta \frac{\omega_{ua}}{s}} = \frac{1}{\beta} \frac{1}{1 + s/\beta\omega_{ua}}$$

$$\omega_{-3dB} = \beta \omega_{ua}$$

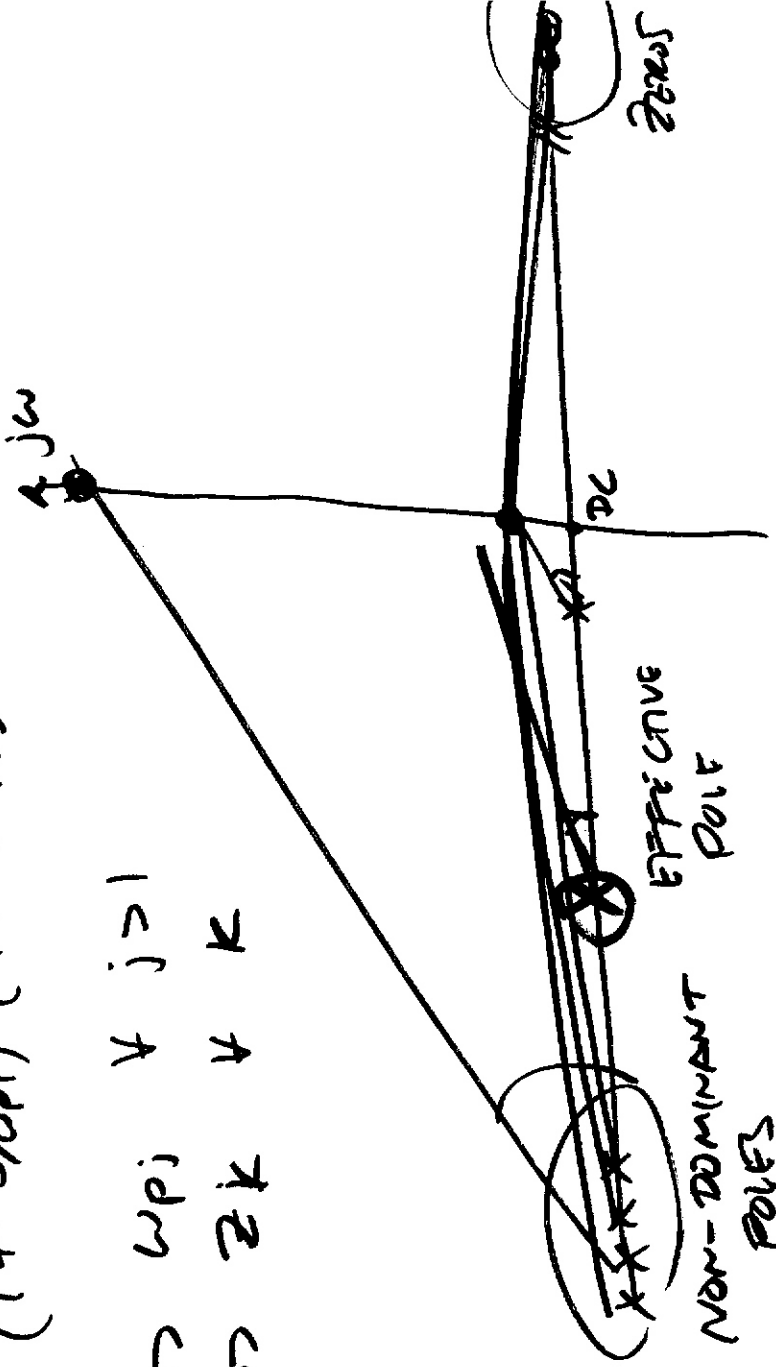
BASIC GAIN/SW
TRADEOFF



MULTI-POLE/ZERO SYSTEM

$$A(s) = \frac{A_0 (1 + s/z_1) \dots (1 + s/z_m)}{(1 + s/\omega_{p1}) (1 + s/\omega_{p2}) \dots (1 + s/\omega_{pn})}$$

$\omega_{p1} \gg \dots \omega_{pj} \quad \forall j > 1$
 $\gg \dots z_k \quad \forall k$



$$\angle A(s) = \sum \angle z_{i|j\omega} - \sum \angle p_{i|j\omega}$$

$$\frac{\text{POLFS}}{1 + S\omega_{p1}} \approx \frac{1}{1 + S\omega_{p1} + S\omega_{p2} + S\omega_{p3} + \dots}$$

$$= \frac{1}{1 + S \left(\frac{1}{\omega_{p1}} + \frac{1}{\omega_{p2}} + \dots \right)} \approx \frac{1}{\omega_{\text{eff},1}}$$

Zeros

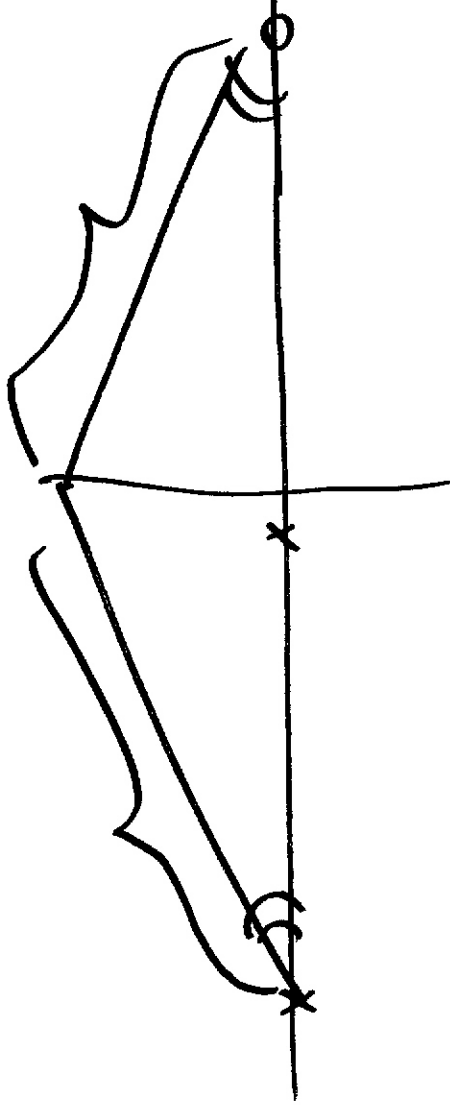
$$(1 + S/\omega_{z1}) (1 + S/\omega_{z2}) \dots (1 + S/\omega_{zm}) =$$

$$= 1 + S \left(\frac{1}{\omega_{z1}} + \frac{1}{\omega_{z2}} + \dots \right) = 1 + S \sum_{k=1}^m \frac{1}{\omega_{zk}}$$

$$= 1 + S = \frac{1}{1 - S} \approx \frac{1}{1 - S \left(\frac{1}{\omega_{z1}} + \dots \right)} \approx \omega_{\text{eff},2}$$

$$A(s) \approx \frac{1}{(1 + s/\omega_{p1}) (1 + s/\omega_{eff1}) (1 - s/\omega_{eff2})}$$

$$\approx \frac{1}{(1 + s/\omega_{p1}) (1 + s (\frac{1}{\omega_{eff1}} - \frac{1}{\omega_{eff2}}))}$$



$\omega \gg \omega_{p1}$ FREQ HIGHER THAN DOMINANT POLE

$$A(s) = \frac{A_0}{\left(\frac{s}{\omega_{p1}}\right) (1 + s/\omega_{cy})} = \frac{A_0 \omega_{p1}}{s(1 + s/\omega_{cy})}$$

$$= \frac{\omega_{cy}}{s(1 + s/\omega_{cy})}$$

$$|T(s)| = |\beta A(s)| = \left| \frac{\beta \omega_{cy}}{s(1 + s/\omega_{cy})} \right|_{s=j\omega_t} = 1$$

$$\frac{\beta \omega_{cy}}{\omega_t \sqrt{1 + \left(\frac{\omega_t}{\omega_{cy}}\right)^2}} = 1$$

$$\boxed{\beta \omega_{cy} = \omega_t \sqrt{1 + \left(\frac{\omega_t}{\omega_{cy}}\right)^2}}$$

check $\omega t \gg \omega t$

$$\beta \omega t = \omega t \quad \checkmark$$

$$\angle T(\omega t) = -90^\circ - \tan^{-1} \left(\frac{\omega t}{\omega t} \right) \quad \text{Ⓢ}$$

$$PM = \angle T = (-180^\circ) = 90^\circ - \tan^{-1} \frac{\omega t}{\omega t}$$

$$\tan^{-1} \frac{\omega t}{\omega t} = \text{PM } 90^\circ - \text{PM}$$

$$\frac{\omega t}{\omega t} = \tan^{-1} (90^\circ - \text{PM})$$

$$\omega t = \omega t \tan^{-1} (90^\circ - \text{PM})$$

$$PM = 45^\circ \Rightarrow \tan 45 = 1$$

$$\boxed{w_t = w_{ey}}$$

POLE/ZERO DOUBLET

$$\frac{z^x}{p^x} = 1 + \epsilon \quad \epsilon \ll 1$$

$$H(s) = \frac{(1 + s/z_x)}{(1 + s/p_x)(1 + s/p_1)}$$

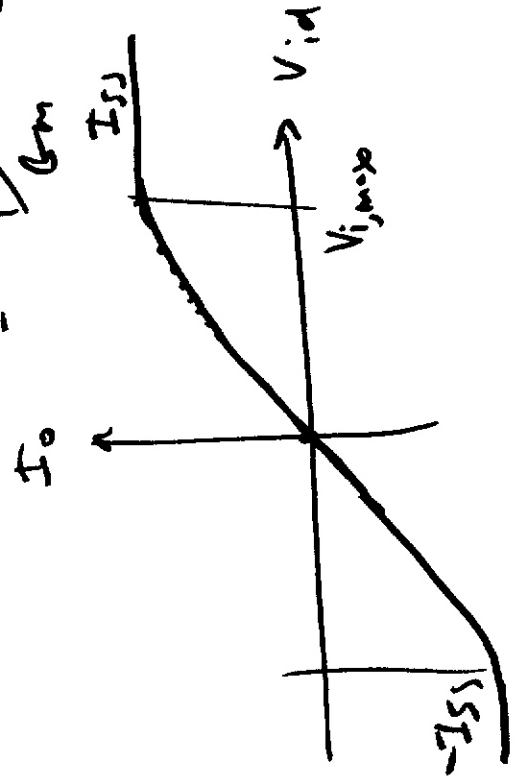
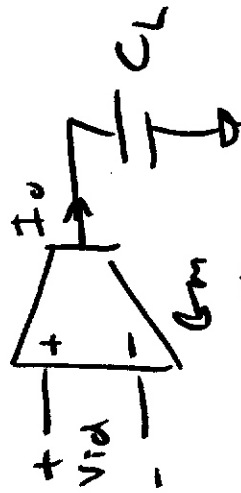
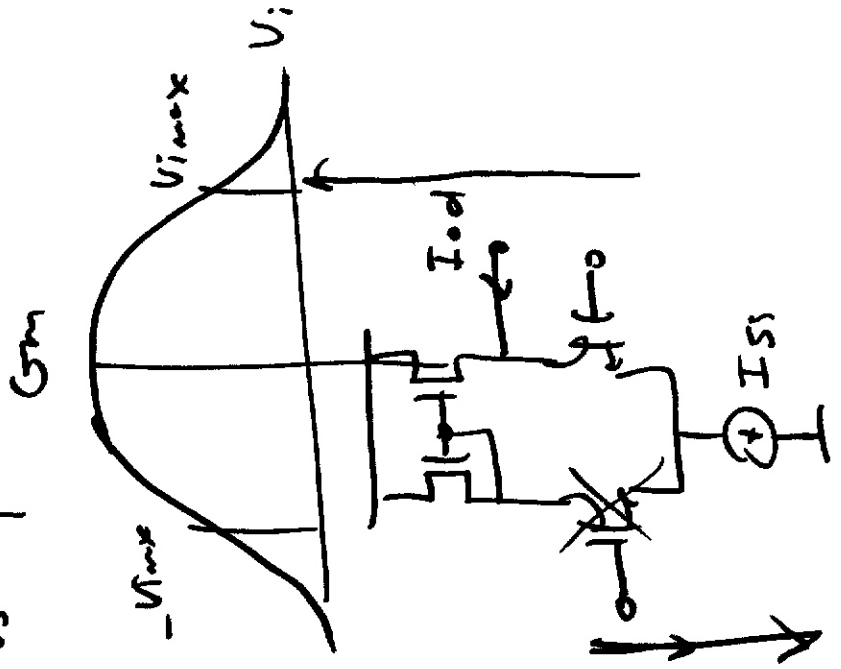
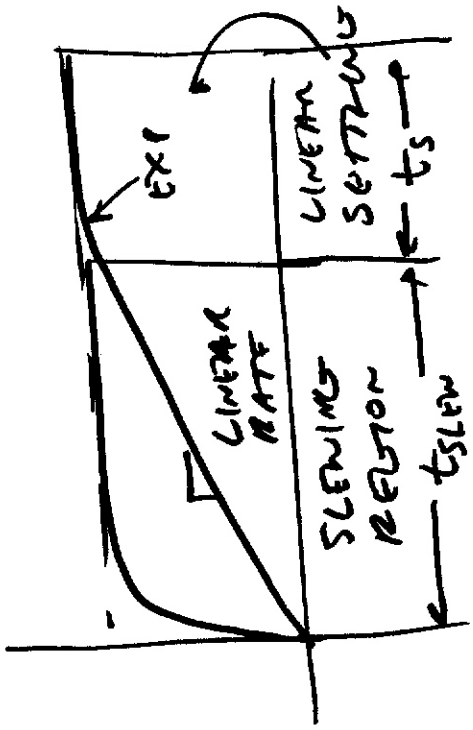
$$\mathcal{L}^{-1} \left\{ \frac{1}{s} H(s) \right\} = \frac{A}{s} + \frac{B}{1 + s/p_x} + \frac{C}{1 + s/p_1}$$

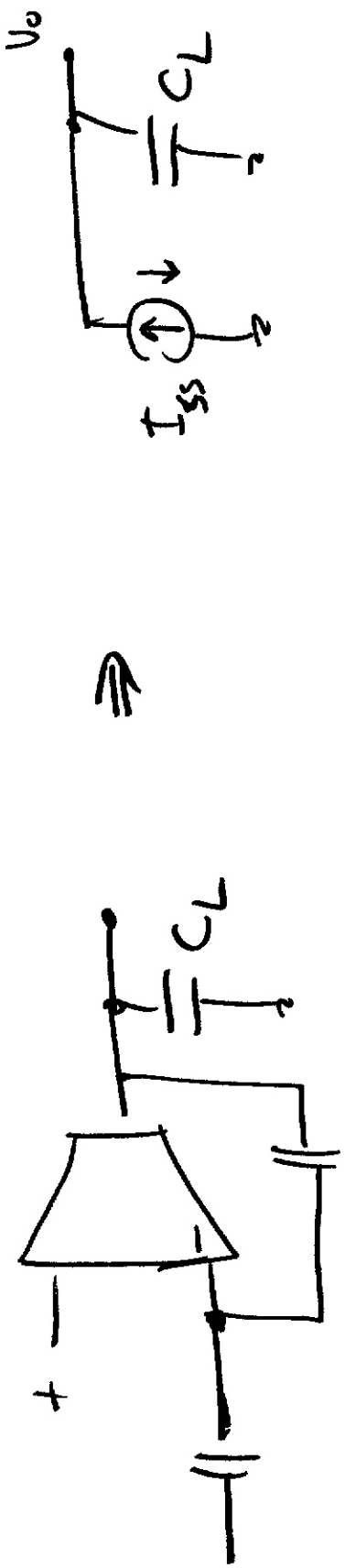
$$A = 1 \quad B = -\frac{p_1}{p_x} \quad C = 1 - \frac{p_1}{z_x} \epsilon$$

$$y(t) = u(t) \left(- \underbrace{e^{-t/p_1}}_{\text{DOMINANT POLE}} - \underbrace{\left(\frac{p_1}{p_x} \right) \epsilon}_{\text{ERROR TERM}} e^{-t/p_x} \right)$$

SETTLING TIME OF ERROR TERM

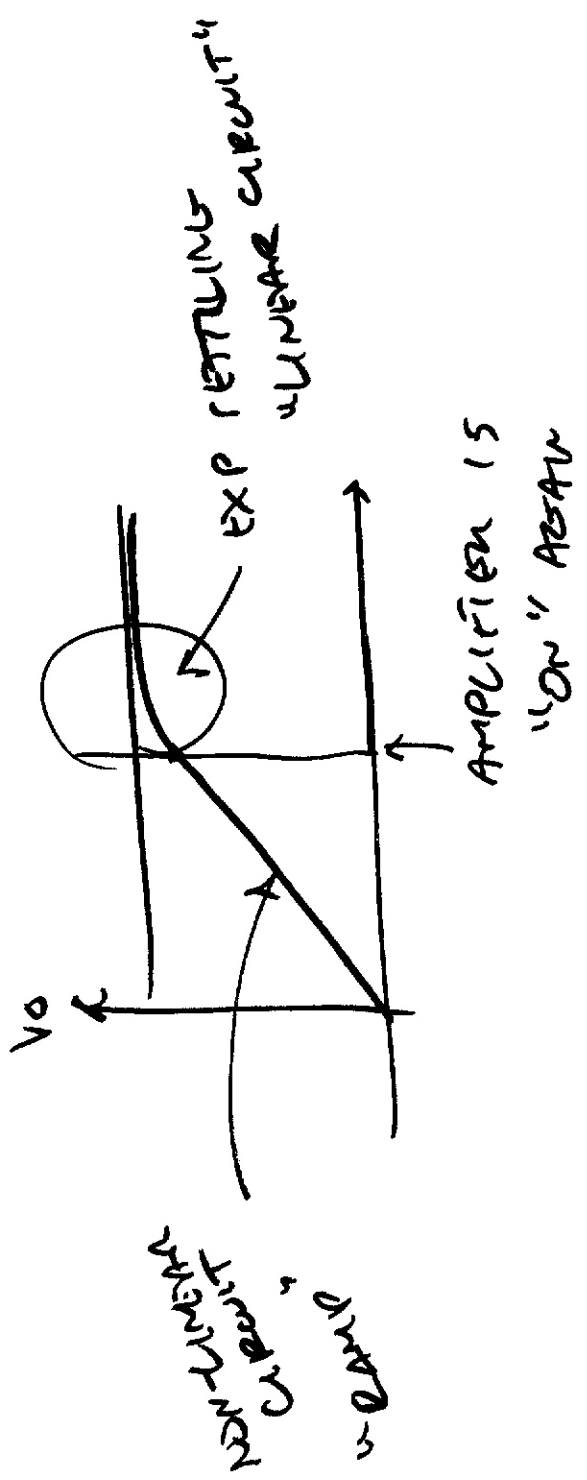
SLEWING

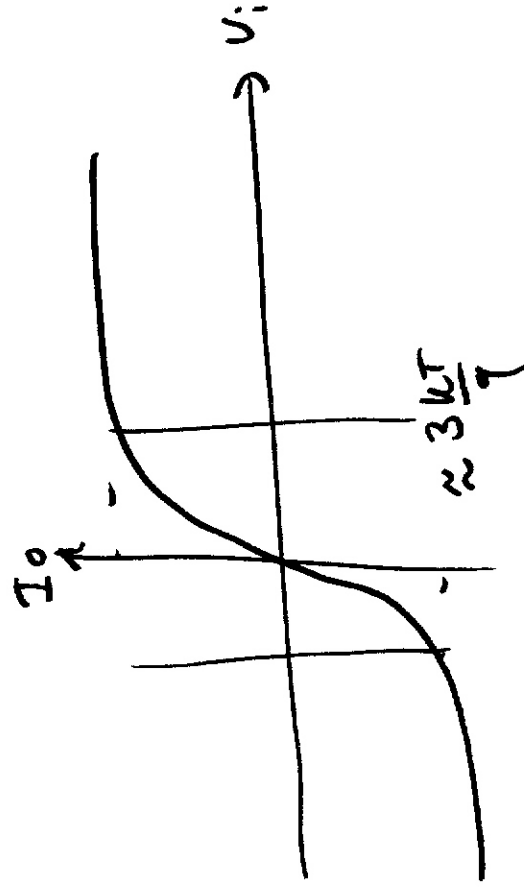
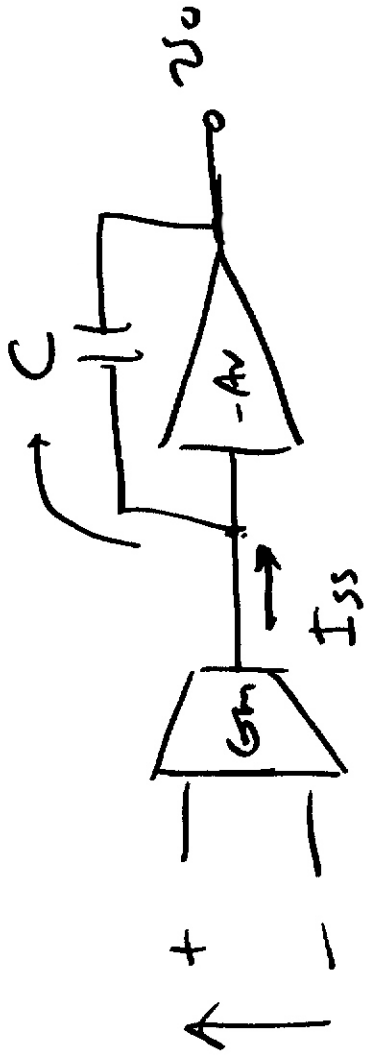




$$\frac{dV_o}{dt} = \frac{I_{SS}}{C_L}$$

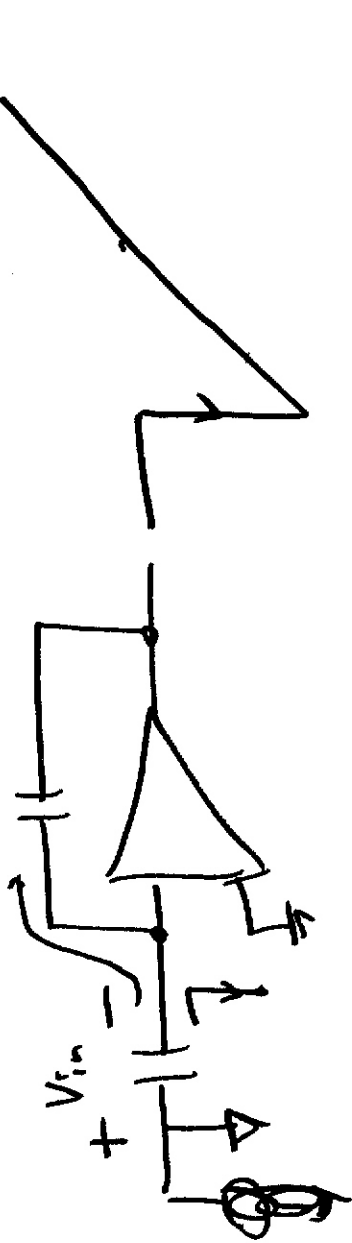
$$C_L \frac{dV_o}{dt} = I_{SS}$$





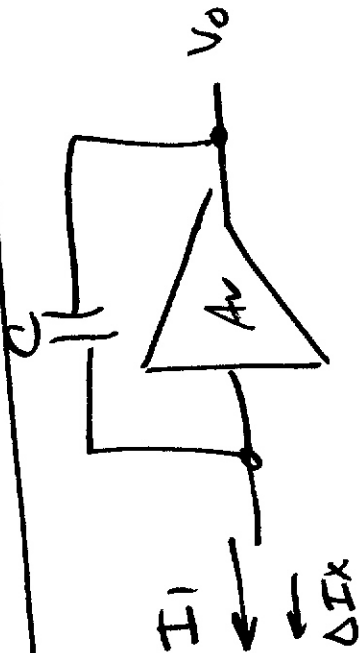
$$I_{D, \text{noise}} \approx \sqrt{2} I_{D, \text{load}} = \sqrt{2} I_{D, \text{load}}^{\#}$$

↑
SOURCE CURRENT



STEP INPUT (S) RENZ!

G&M



$$\frac{dV_o}{dt} = \frac{I_1}{C}$$

$$V_o(t) = \frac{I_1}{C} t$$

$$g_m \triangleq \frac{\Delta I_x}{\Delta V_x}$$

$$\frac{\Delta V_o}{\Delta I_x} = \frac{1}{sC}$$

SECOND
STAGE

↳ ACTING
LIKE INTEGRATOR

$$\frac{\Delta V_o}{\Delta I_A} = \frac{1}{j\omega C}$$

$$\frac{\Delta V_o}{\Delta V_i} = \frac{g_m}{j\omega C}$$

$$\frac{g_m}{\omega C} = |$$

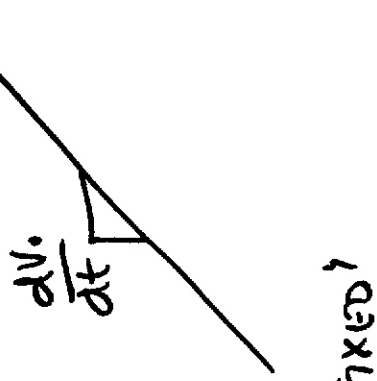
45° PM

$$|K| = 1$$

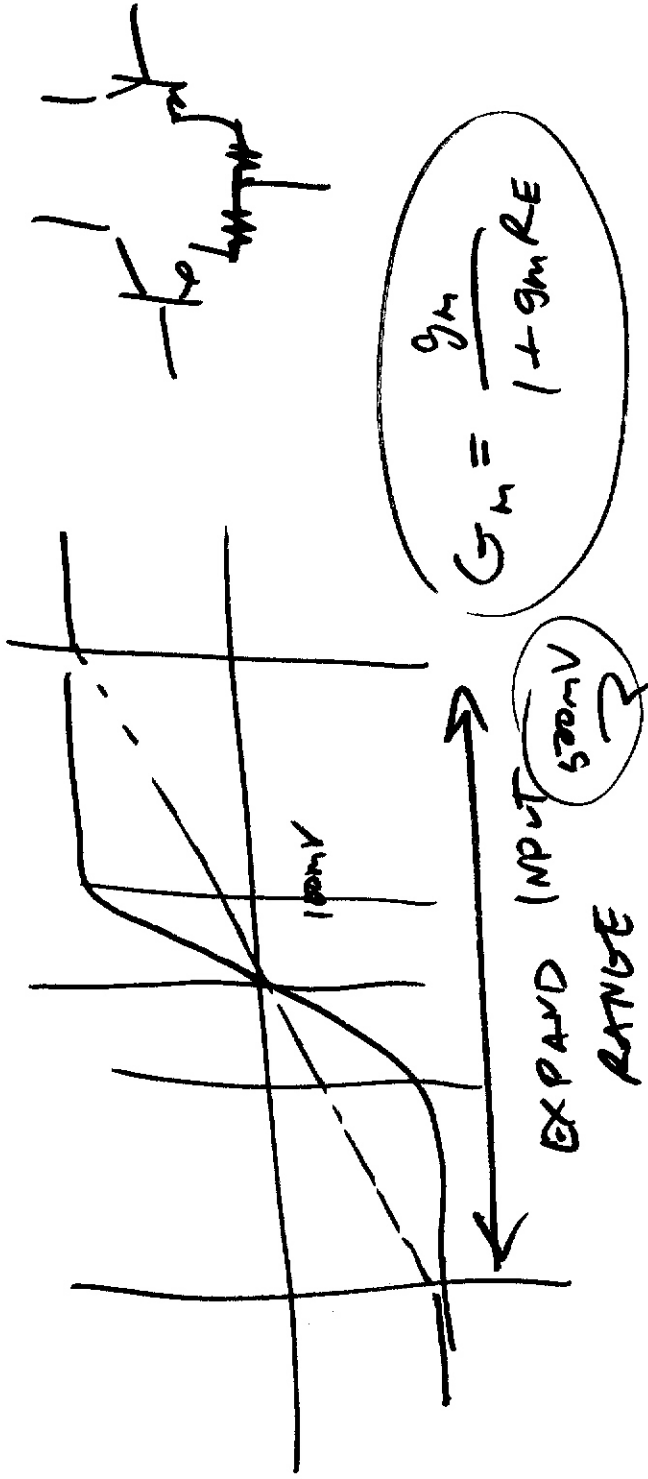
$$\omega_2 = K \omega_u$$

$$\omega_2 = \frac{\omega_u}{g_m}$$

$$\frac{1}{C} = \frac{\omega_u}{g_m}$$



iii $\frac{I}{g_m}$ ANSWER

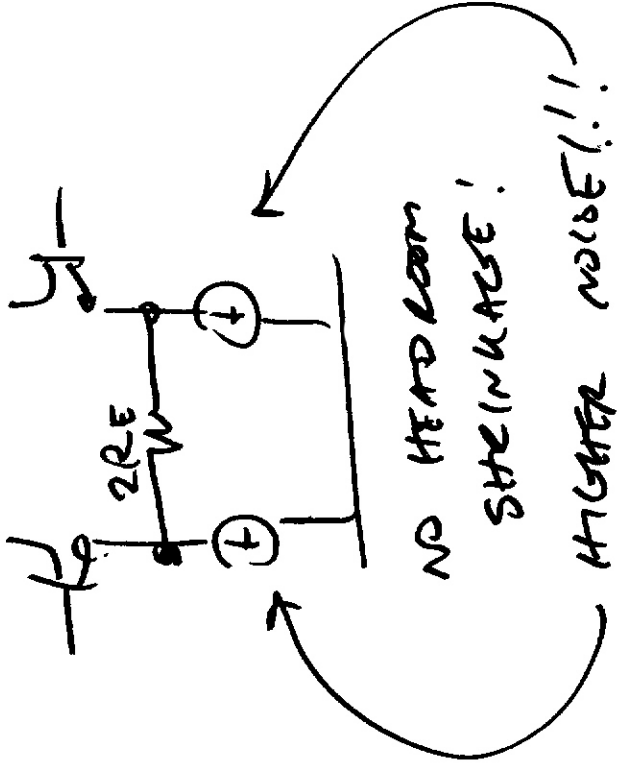
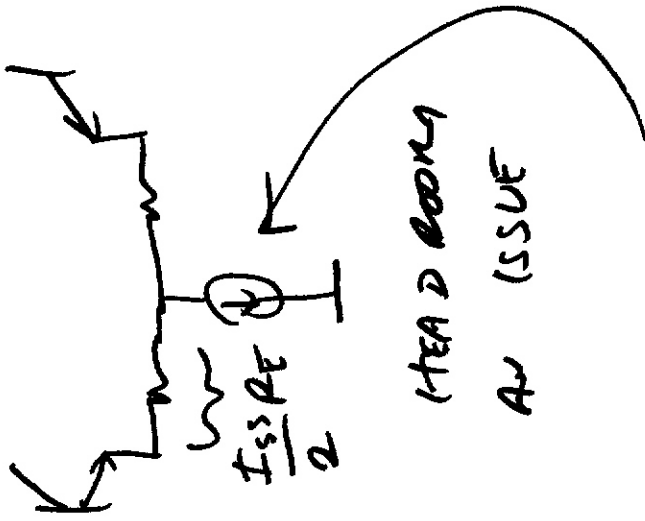


$-k_e \frac{1}{1 + g_m R_E}$

$$SR_{no,FB} = \frac{I_{SS}}{G_M} \omega_2 = 2 \frac{kT}{q} \omega_2 \quad K$$

$$SR_{RE} = \frac{I_{SS}}{G_M} \omega_2 = 2 \frac{kT}{q} \omega_2 (1 + g_m R_E)$$

INCREASE SR
BY COOL GAIN!



CORRELATED
NOISE \Rightarrow ZERO
FOR DIFF O/P

$$SR = \frac{I_{SS}}{gM} \omega_2 = \frac{2 I_1}{\sqrt{2 \mu C \times (\frac{w}{L})} I_1} \omega_2$$

$$= \frac{2 \omega_2}{\sqrt{2 \mu C \times (\frac{w}{L})}} \sqrt{I_1}$$

↑
DECREASE (w/L)

g_m DROPS → MUST PROP CL ...

AMP DESIGN : SPEED, RESOLUTION

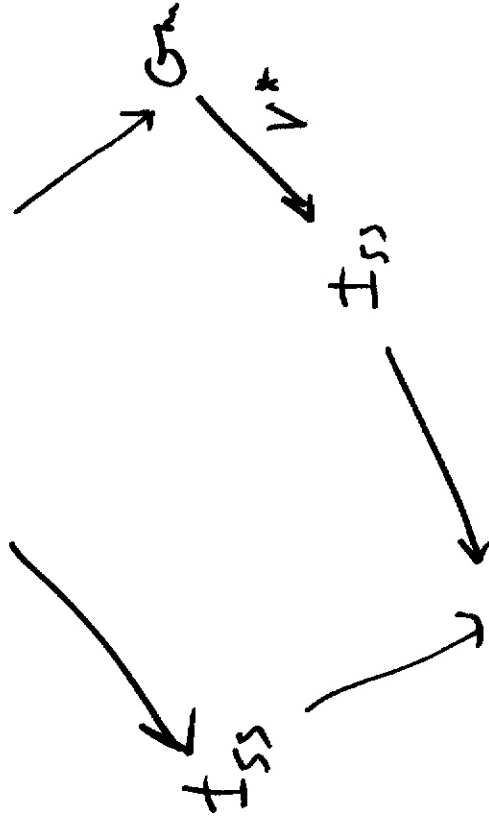
t_s, ϵ

$$\epsilon' = \frac{1}{2} \epsilon$$

(1) STATIC SETTLING $\Rightarrow A_{VO}$

(2) DYNAMIC SETTLING

$$t_s = t_{s,lin} + t_{s,slew}$$



TAKE MARGEN!