

Integrated Circuits for Communication



**Berkeley**

## The Smith Chart

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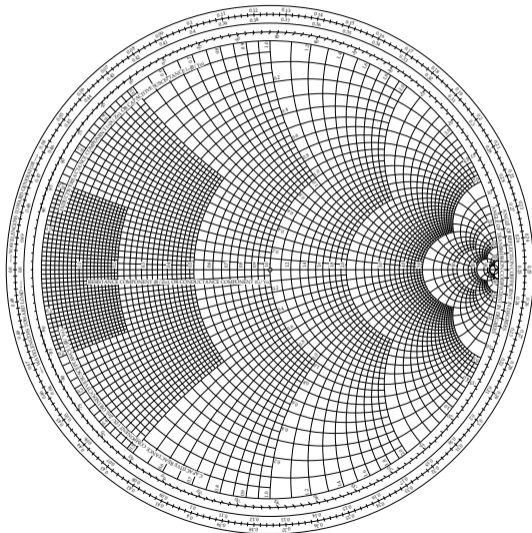
February 11, 2025

# The Smith Chart

- The Smith Chart is simply a graphical calculator for computing impedance as a function of reflection coefficient  $z = f(\rho)$
- More importantly, many problems can be easily visualized with the Smith Chart
- This visualization leads to a insight about the behavior of transmission lines
- All the knowledge is coherently and compactly represented by the Smith Chart
- Why else study the Smith Chart? It's beautiful!
- Aside: There are deep mathematical connections in the Smith Chart. It's the tip of the iceberg! Study complex analysis to learn more.

# An Impedance Smith Chart

- Without further ado, here it is!



# Generalized Reflection Coefficient

- We have found that in sinusoidal steady-state, the voltage on the line is a T-line

$$v(z) = v^+(z) + v^-(z) = V^+(e^{-\gamma z} + \rho_L e^{\gamma z})$$

- Recall that we can define the reflection coefficient anywhere by taking the ratio of the reflected wave to the forward wave

$$\rho(z) = \frac{v^-(z)}{v^+(z)} = \frac{\rho_L e^{\gamma z}}{e^{-\gamma z}} = \rho_L e^{2\gamma z}$$

- Therefore the impedance on the line ...

$$Z(z) = \frac{v^+ e^{-\gamma z} (1 + \rho_L e^{2\gamma z})}{\frac{v^+}{Z_0} e^{-\gamma z} (1 - \rho_L e^{2\gamma z})}$$

# Normalized Impedance

- ...can be expressed in terms of  $\rho(z)$

$$Z(z) = Z_0 \frac{1 + \rho(z)}{1 - \rho(z)}$$

- It is extremely fruitful to work with normalized impedance values  $z = Z/Z_0$

$$z(z) = \frac{Z(z)}{Z_0} = \frac{1 + \rho(z)}{1 - \rho(z)}$$

- Let the normalized impedance be written as  $z = r + jx$  (note small case)
- The reflection coefficient is “normalized” by default since for passive loads  $|\rho| \leq 1$ . Let  $\rho = u + jv$

# Dissection of the Transformation

- Now simply equate the real ( $\Re$ ) and imaginary ( $\Im$ ) components in the above equation

$$r + jx = \frac{(1 + u) + jv}{(1 - u) - jv} = \frac{(1 + u + jv)(1 - u + jv)}{(1 - u)^2 + v^2}$$

- To obtain the relationship between the  $(r, x)$  plane and the  $(u, v)$  plane

$$r = \frac{1 - u^2 - v^2}{(1 - u)^2 + v^2}$$

$$x = \frac{v(1 - u) + v(1 + u)}{(1 - u)^2 + v^2}$$

- The above equations can be simplified and put into a nice form

## Completing Your Squares...

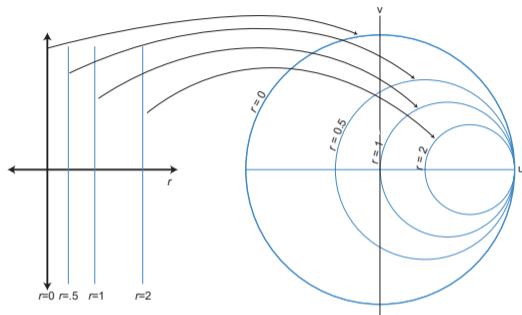
- If you remember your high school algebra, you can derive the following equivalent equations

$$\left(u - \frac{r}{1+r}\right)^2 + v^2 = \frac{1}{(1+r)^2}$$

$$(u-1)^2 + \left(v - \frac{1}{x}\right)^2 = \frac{1}{x^2}$$

- These are circles in the  $(u, v)$  plane! Circles are good!
- We see that vertical and horizontal lines in the  $(r, x)$  plane (complex impedance plane) are transformed to circles in the  $(u, v)$  plane (complex reflection coefficient)

# Resistance Transformations

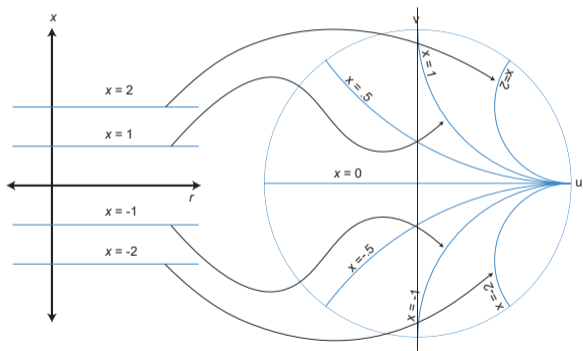


- $r = 0$  maps to  $u^2 + v^2 = 1$  (unit circle)
- $r = 1$  maps to  $(u - 1/2)^2 + v^2 = (1/2)^2$  (matched real part)
- $r = .5$  maps to  $(u - 1/3)^2 + v^2 = (2/3)^2$  (load  $R$  less than  $Z_0$ )
- $r = 2$  maps to  $(u - 2/3)^2 + v^2 = (1/3)^2$  (load  $R$  greater than  $Z_0$ )

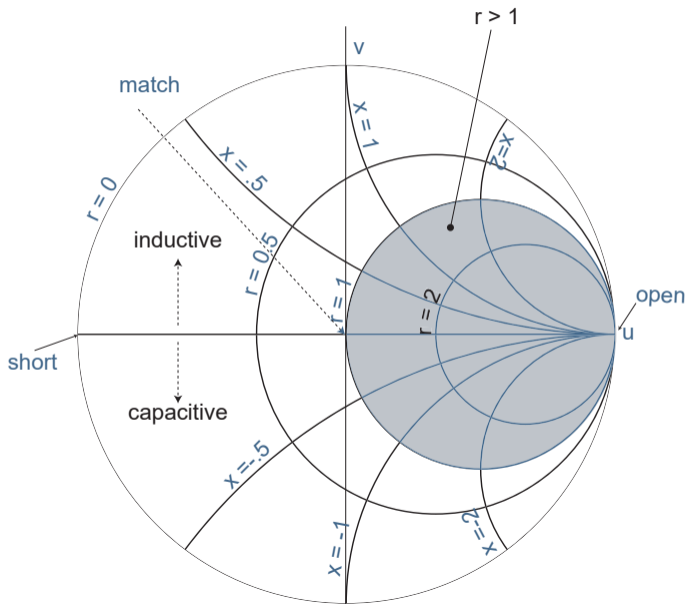


# Reactance Transformations

- $x = \pm 1$  maps to  $(u - 1)^2 + (v \mp 1)^2 = 1$
- $x = \pm 2$  maps to  $(u - 1)^2 + (v \mp 1/2)^2 = (1/2)^2$
- $x = \pm 1/2$  maps to  $(u - 1)^2 + (v \mp 2)^2 = 2^2$
- Inductive reactance maps to upper half of unit circle
- Capacitive reactance maps to lower half of unit circle

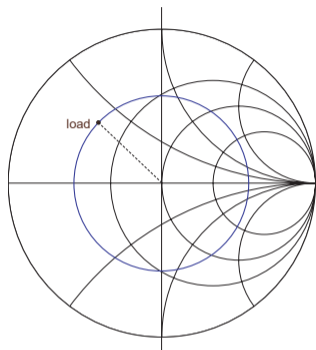


# Complete Smith Chart



## Reading the Smith Chart

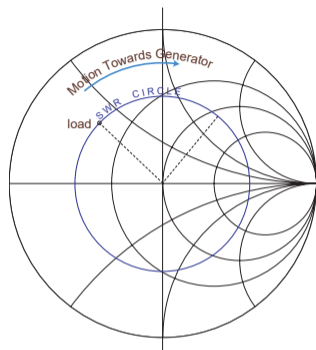
# Reading the Smith Chart



- First map  $z_L$  on the Smith Chart as  $\rho_L$
- To read off the impedance on the T-line at any point on a lossless line, simply move on a circle of constant radius since

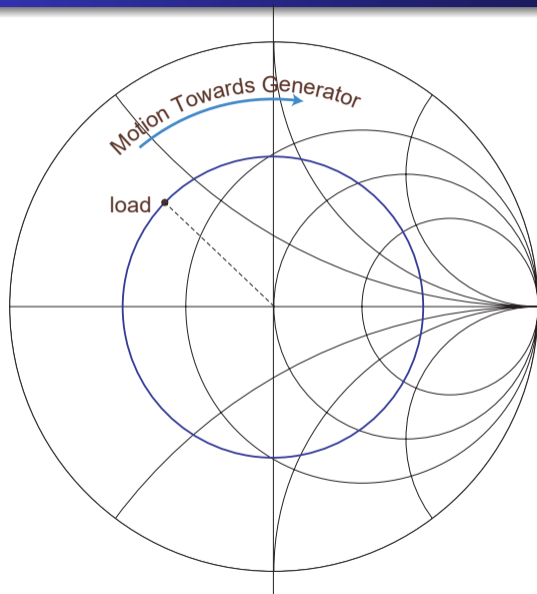
$$\rho(z) = \rho_L e^{2j\beta z}$$

# Motion Towards Generator



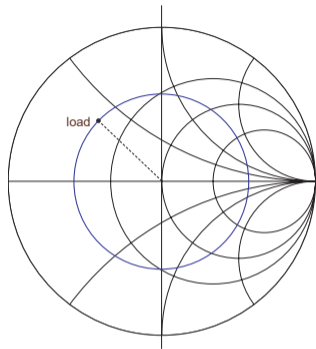
- Moving towards generator means  $\rho(-\ell) = \rho_L e^{-2j\beta\ell}$ , or clockwise motion
- We're back to where we started when  $2\beta\ell = 2\pi$ , or  $\ell = \lambda/2$
- Thus the impedance is periodic (as we know)
- Aside: For a lossy line, this corresponds to a spiral motion and so the Smith Chart is more useful for low-loss lines

# SWR Circle



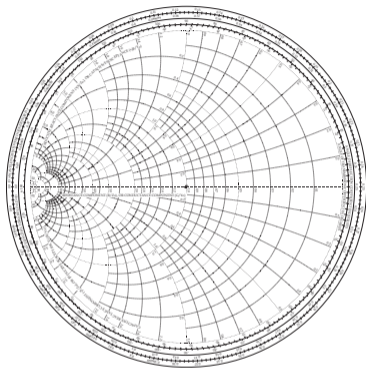
- Since SWR is a function of  $|\rho|$ , a circle at origin in  $(u, v)$  plane is called an SWR circle
- Recall the voltage max occurs when the reflected wave is in phase with the forward wave, so  $\rho(z_{min}) = |\rho_L|$
- This corresponds to the intersection of the SWR circle with the positive real axis (read off SWR by just reading the value of  $r$ )
- Likewise, the intersection with the negative real axis is the location of the voltage min

# Example of Smith Chart Visualization



- Prove that if  $Z_L$  has an inductance reactance, then the position of the first voltage maximum occurs before the voltage minimum as we move towards the generator
- Proof: On the Smith Chart start at any point in the upper half of the unit circle. Moving towards the generator corresponds to clockwise motion on a circle. Therefore we will always cross the positive real axis first and then the negative real axis.

# Admittance Chart



- Since  $y = 1/z = \frac{1-\rho}{1+\rho}$ , you can imagine that an Admittance Smith Chart looks very similar
- In fact everything is switched around a bit and you can construct a combined admittance/impedance Smith Chart. You can also use an impedance chart for admittance if you simply map  $x \rightarrow b$  and  $r \rightarrow g$
- Be careful ... the caps are now on the top of the chart and the inductors on the bottom
- The short and open likewise swap positions



# Admittance on Smith Chart

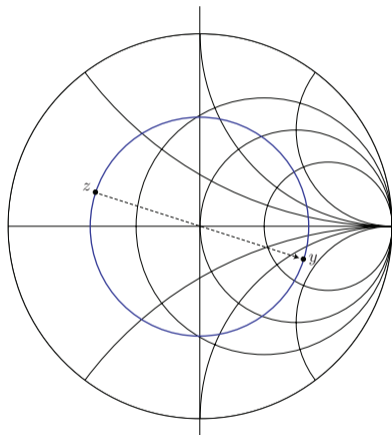
- Sometimes you may need to work with both impedances and admittances.
- This is not easy on the Smith Chart and requires proficient use of the impedance inversion property of a  $\lambda/4$  line (it actually can get pretty confusing)

$$Z' = \frac{Z_0^2}{Z}$$

- If we normalize  $Z'$  we get  $y$

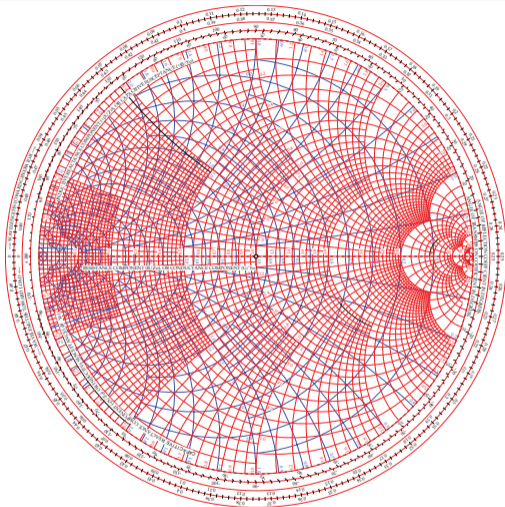
$$\frac{Z'}{Z_0} = \frac{Z_0}{Z} = \frac{1}{z} = y$$

# Admittance Conversion



- Thus if we simply rotate  $\pi$  degrees on the Smith Chart and read off the impedance, we're actually reading off the admittance!
- Rotating  $\pi$  degrees is easy. Simply draw a line through origin and  $z_L$  and read off the second point of intersection on the SWR circle

# Combined Chart

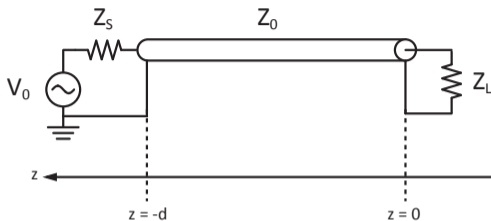


- On a combined chart, you can read off both  $y$  and  $z$ . You can also easily visualize and draw motions along constant  $r$ ,  $g$ ,  $x$ , and  $b$  circles all on the same chart.

## Example Calculation

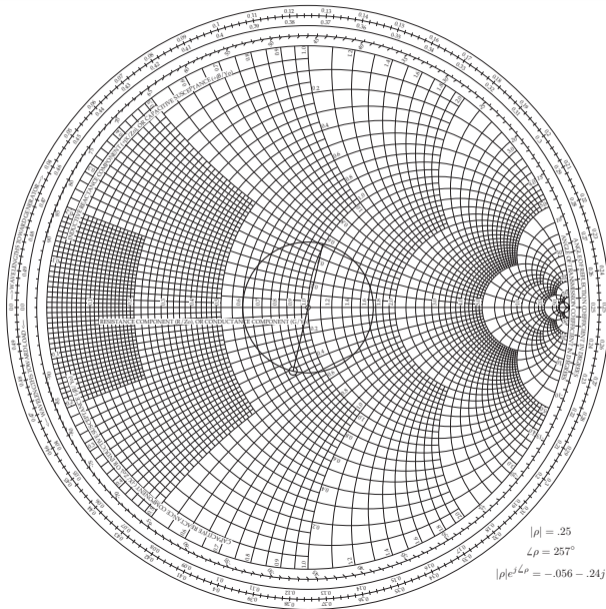
## Example Calculation

# Example Problem



- 1 Consider the transmission line circuit shown below. A voltage source generating 10V amplitude of sinewave at 10 GHz is driving a transmission line terminated with load  $Z_L = 80 - j40$  ohm. The transmission line has a characteristic impedance of  $Z_0 (= 100\Omega)$ , effective dielectric constant of 4, and length  $d = 22.5$  mm.
  - 1 Find the reflection coefficient at the load ( $z = 0$ ) and at the source ( $z = -d$ ). [ Note this is  $1.5\lambda$  ]
  - 2 Find the input impedance at the source ( $z = -d$ ) and at  $z = 18.75$  mm. [Note this is  $1.25\lambda$  ]
  - 3 Plot the magnitude of the voltage along the line. Find voltage maximum, voltage minimum, and standing wave ratio.

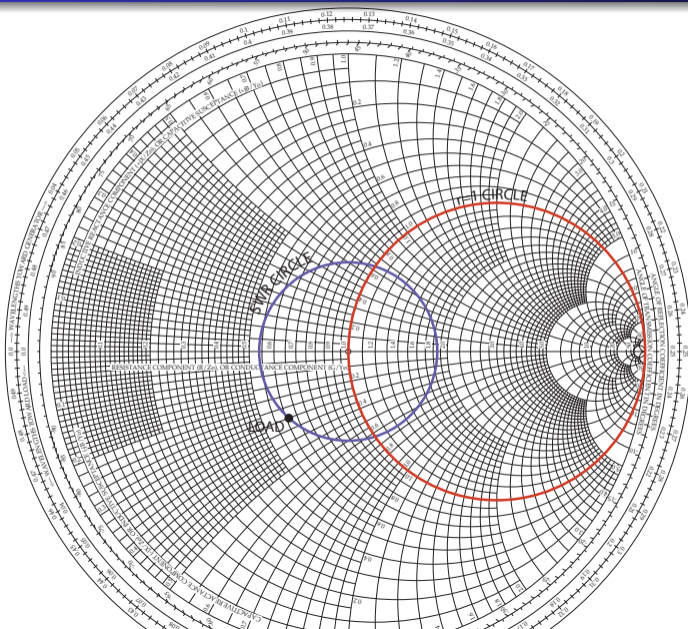
# Homework Problem with Aid from Mr. Smith



## Impedance Matching with Smith Chart

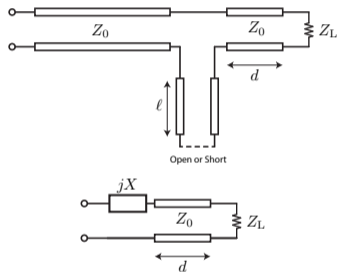
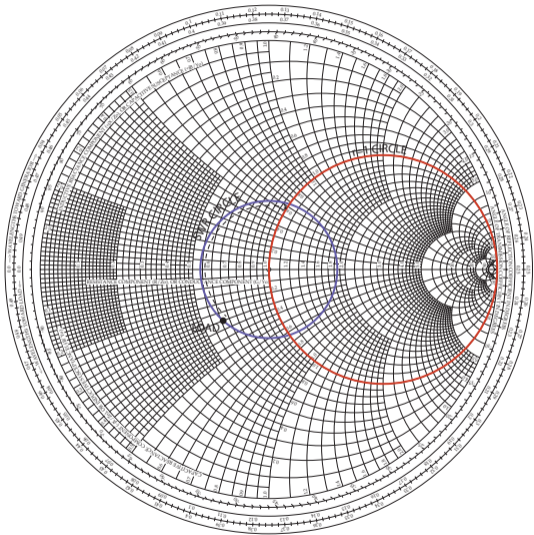


# Impedance Matching Example

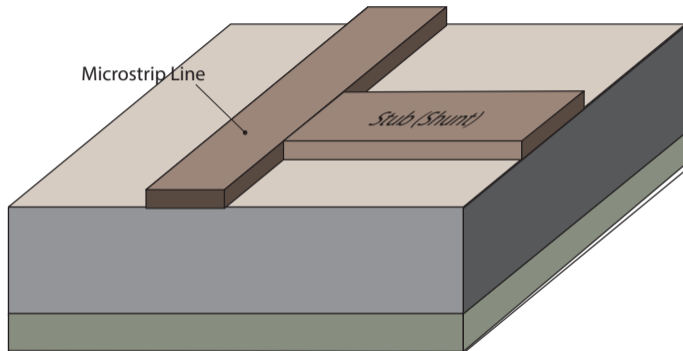


- Single stub impedance matching is easy to do with the Smith Chart
- Simply find the intersection of the SWR circle with the  $r = 1$  circle
- The match is at the center of the circle. Grab a reactance in series or shunt to move you there!

# Series Stub Match

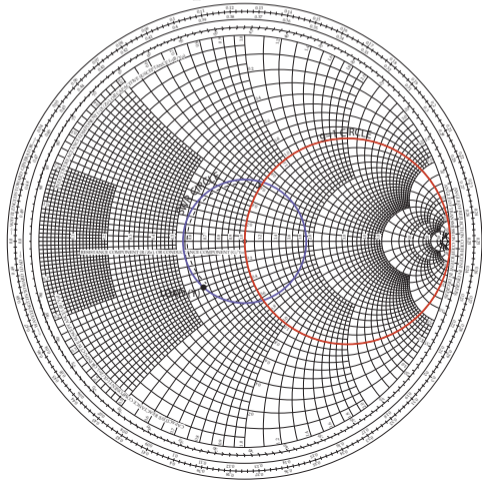
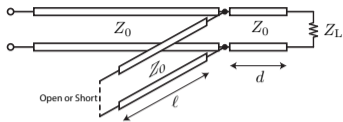


## Series Stub Using Microstrip ?



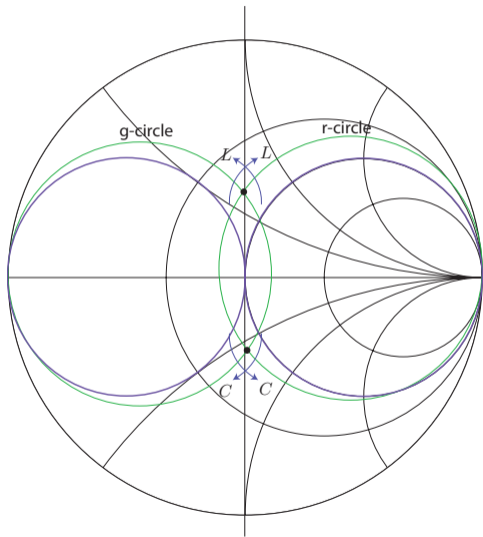
- Shunt stubs are easy but series stubs are not easy and require cuts in the ground plane.

# Shunt Stub Match



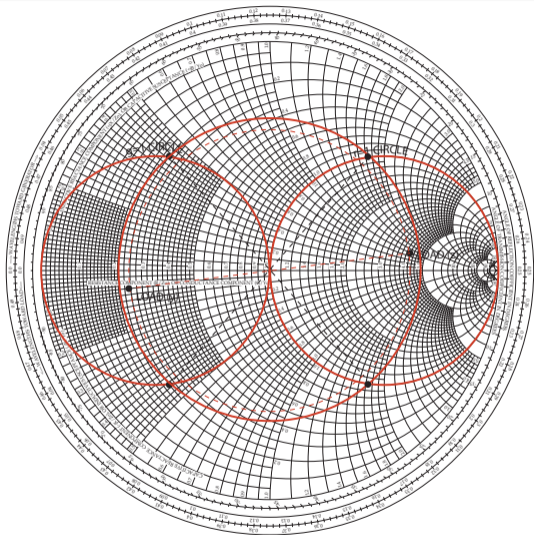
- Let's now solve the same matching problem with a shunt stub.
- To find the shunt stub value, simply convert the value of  $z = 1 + jx$  to  $y = 1 + jb$  and use the Smith chart as an Admittance chart.
- Find the distance to move on an SWR circle to reach the  $1 + jb$  circle (same as  $1 + jx$  circle since we're using it as Y-chart) and read off the distance in wavelengths. To find the shunt stub length, start at a short (open) and move until you reach the desired susceptance.

# Lumped Components On Smith Chart



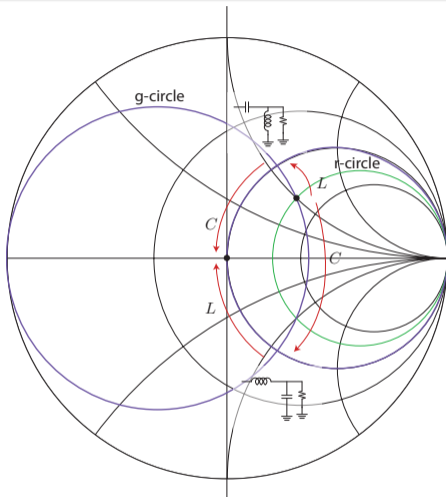
- Adding an inductor in series moves us on the constant  $r$  circle clock-wise (CW). Adding a capacitor in series moves counter clock-wise (CCW).
- On the Y-plane, to go CW, add a shunt C. To move CCW, add a shunt L.

# Matching with Lumped Components (Inside)



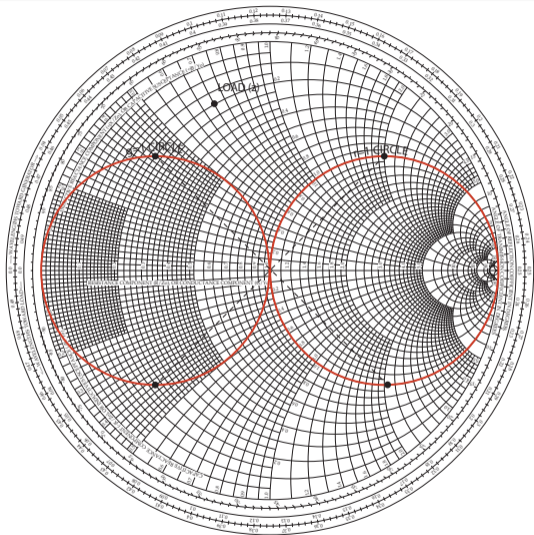
Suppose the load is inside the  $1 + jx$  circle.

# Escaping from "Insdie"



- Notice that there are two paths to get to the center. The difference is one is AC coupled versus DC coupled, so often the application will determine the choice.

# Matching with Lumped Components (Outside)



Suppose the load is outside the  $1 + jx$  circle.



- For designing matching networks, it's very convenient to know the required  $Q$  to achieve a match (related to bandwidth and loss). Let's find the contours of constant  $Q$  on the Smith Chart. Recall that  $z = r + jx$  can be related to the reflection coefficient  $\rho = u + jv$  by the following equations

$$r = \frac{1 - u^2 - v^2}{(1 - u)^2 + v^2}$$

$$x = \frac{v(1 - u) + v(1 + u)}{(1 - u)^2 + v^2}$$

So that the  $Q$  is given by:

$$Q = \frac{x}{r} = \frac{2v}{1 - u^2 - v^2}$$

- We can write this as

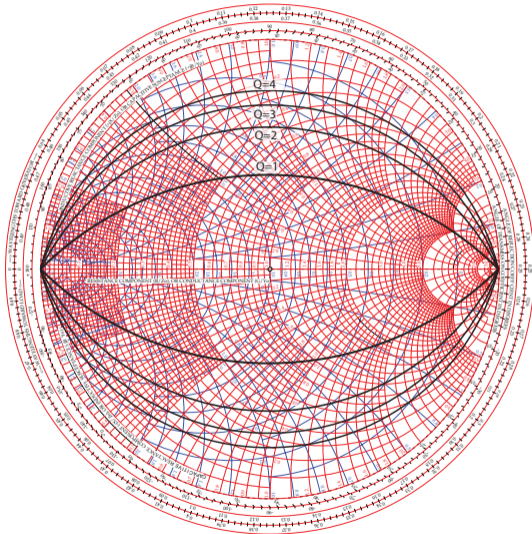
$$Q(1 - u^2 - v^2) = 2v$$

$$(1 - u^2) = v^2 + 2v/Q = v^2 + 2v/Q + 1/Q^2 - 1/Q^2$$

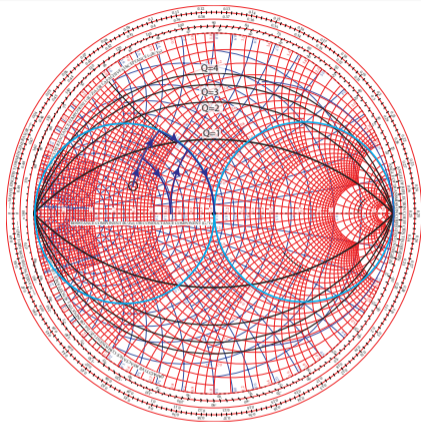
$$1 - 1/Q^2 = u^2 + (v + 1/Q)^2$$

- This is an equation for another circle, centered at  $(u, v) = (0, -1/Q)$  with a radius of  $R = \sqrt{1 + \frac{1}{Q^2}}$ .
- For a capacitive element, the same derivation holds except the circle is centered at  $(u, v) = (0, +1/Q)$

# Q Circles on Smith Chart

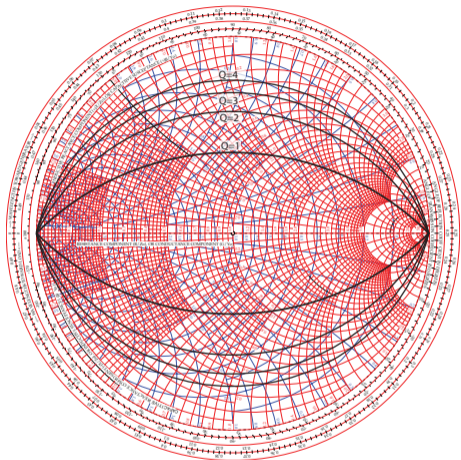


# Single Stage vs Two-Stage Matching Network



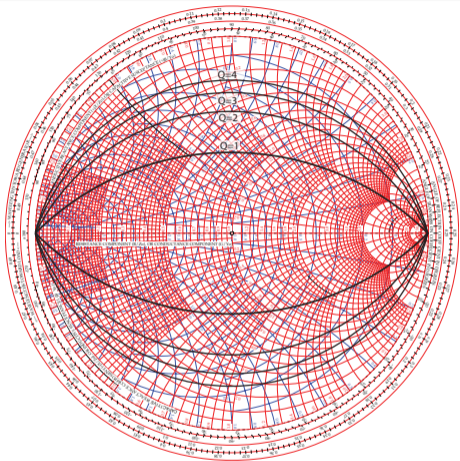
- Notice that with a one stage matching network, the  $Q$  is fixed (we already knew this but now we see it graphically).
- On the other hand, with a two-stage matching network we can actually take a different path and lower the  $Q$ .

# Multi-Stage Matching Network



- For broadband matching, “hug” the x-axis. At high frequency, we can also include transmission line leads into the network.

# Constant Q Matching Network



- Pick a desired  $Q$  (set by bandwidth), and then never allow the matching ratio to go above this value. The number of steps required will be set by the matching ratio.