Single-Stage Amplifiers

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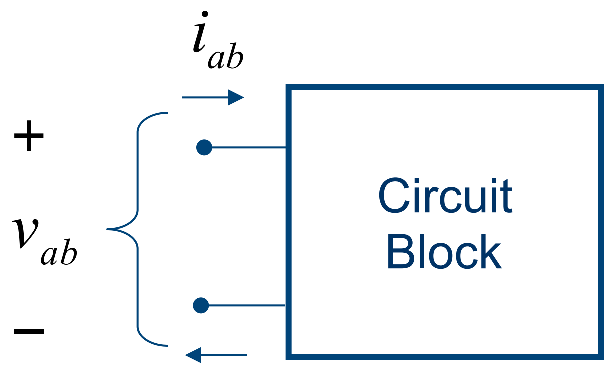
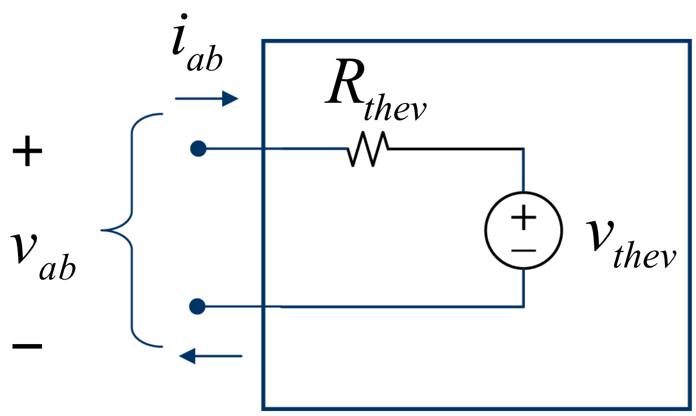
Announcements

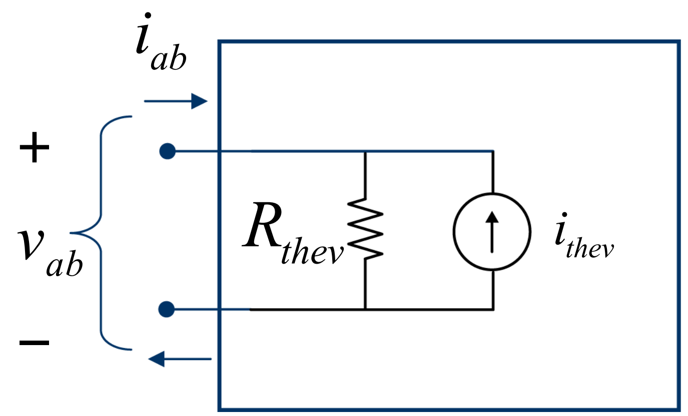
- HW8 due on Friday

One-Port Models (EECS 16A)

- A terminal pair across which a voltage and associated current are defined







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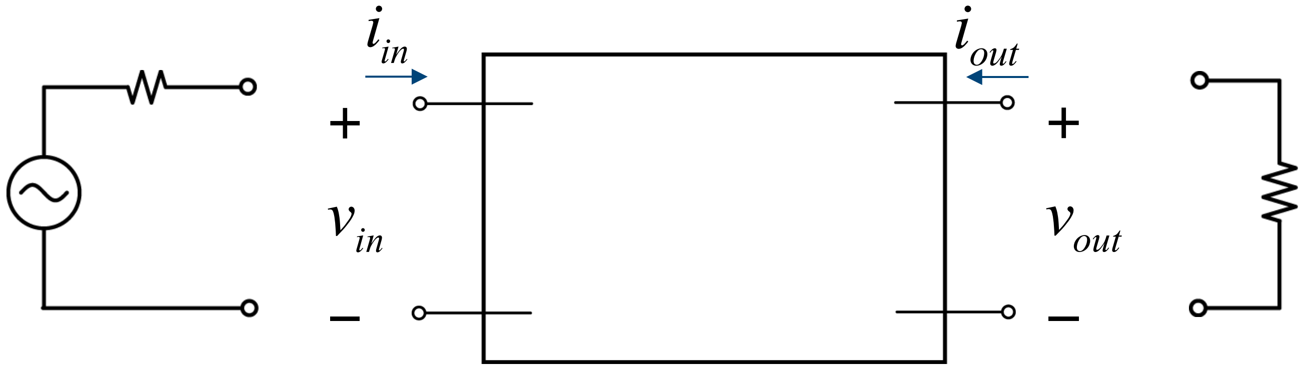
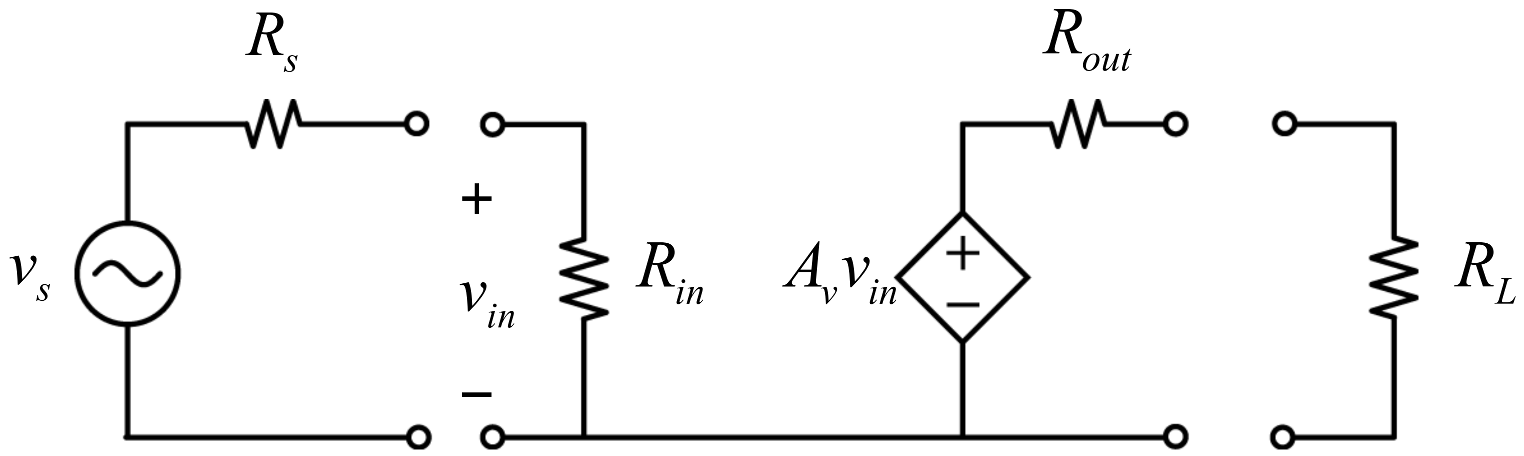
Small-Signal Two-Port Models

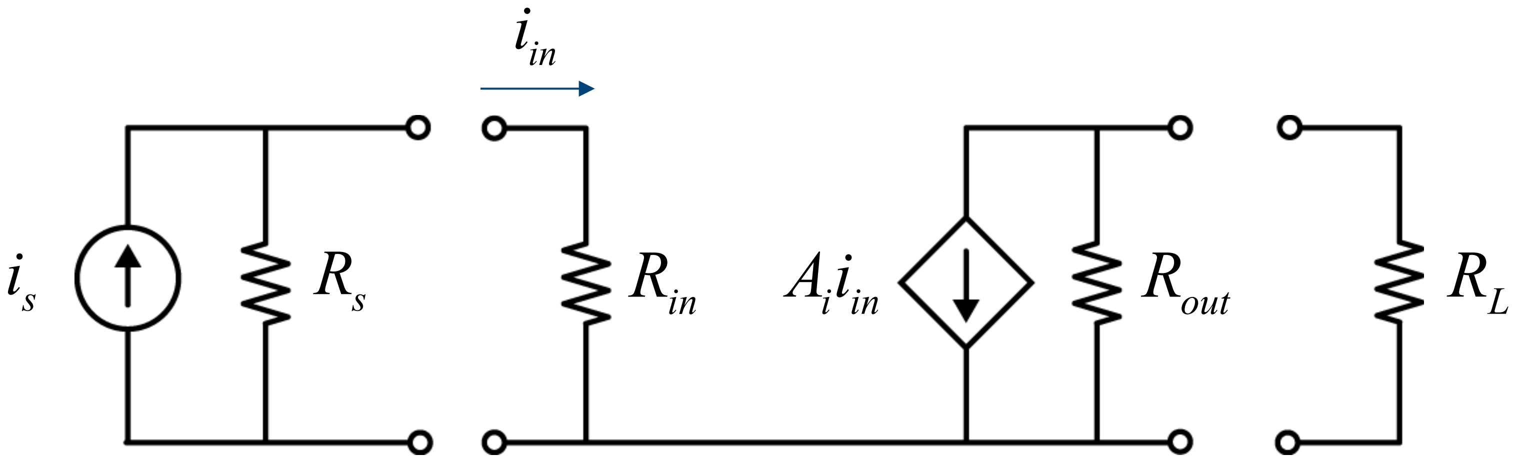


- We assume that input port is linear and that the amplifier is *unilateral*:
  - Output depends on input but input is independent of output.
- Output port : depends linearly on the current and voltage at the input and output ports
- Unilateral assumption is good as long as "overlap" capacitance is small (MOS)

Two-Port Small-Signal Amplifiers

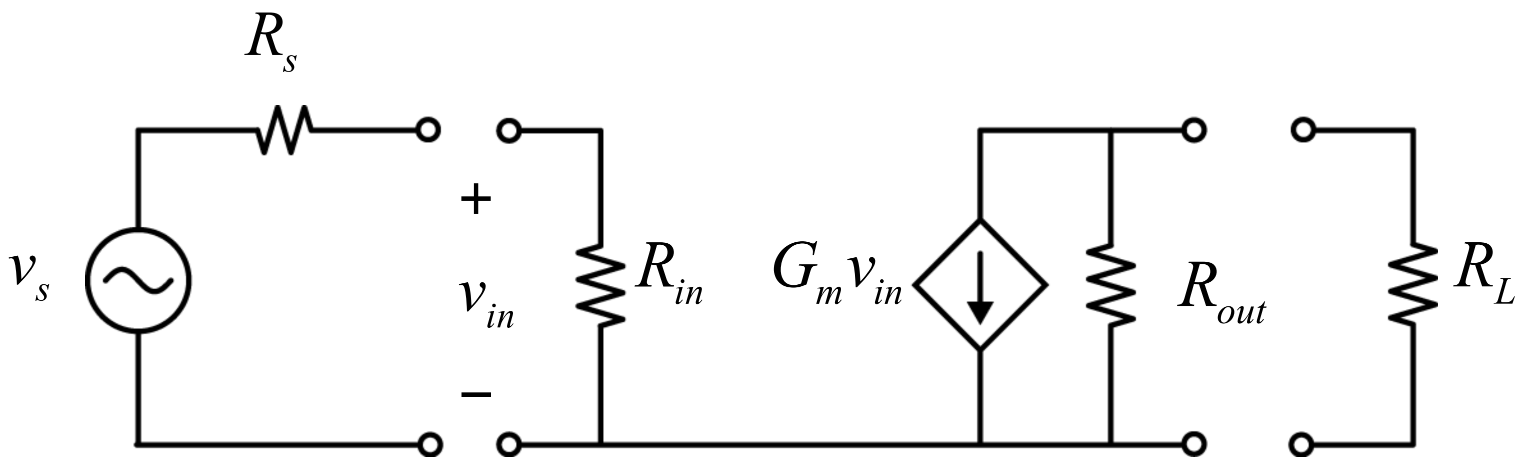


Voltage Amplifier

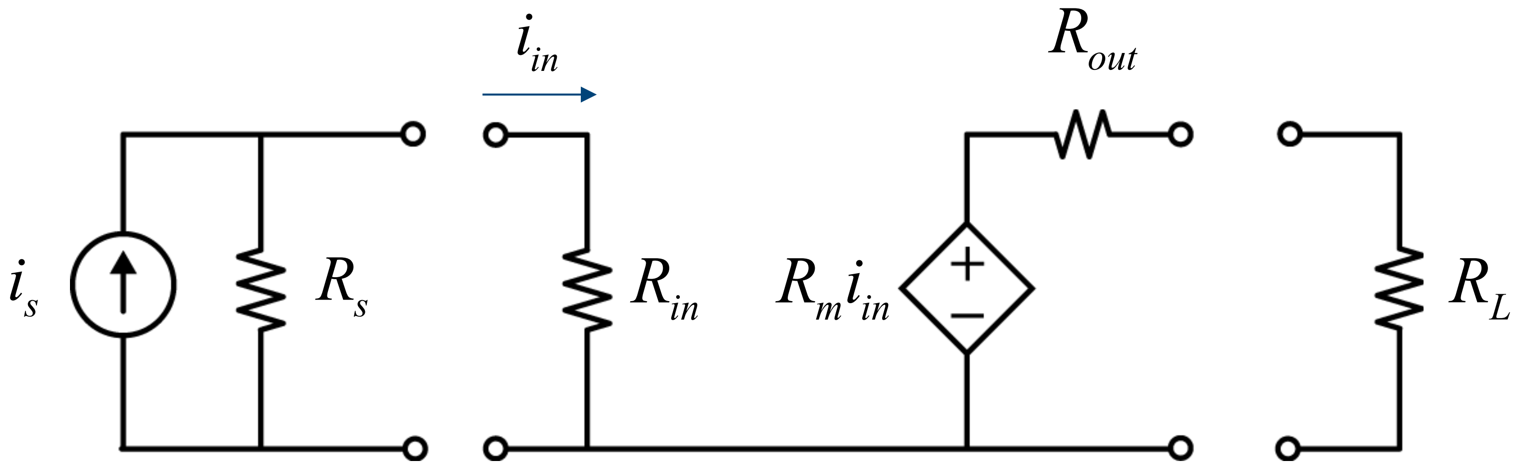


Current Amplifier

Two-Port Small-Signal Amplifiers



Transconductance Amplifier



Transresistance Amplifier

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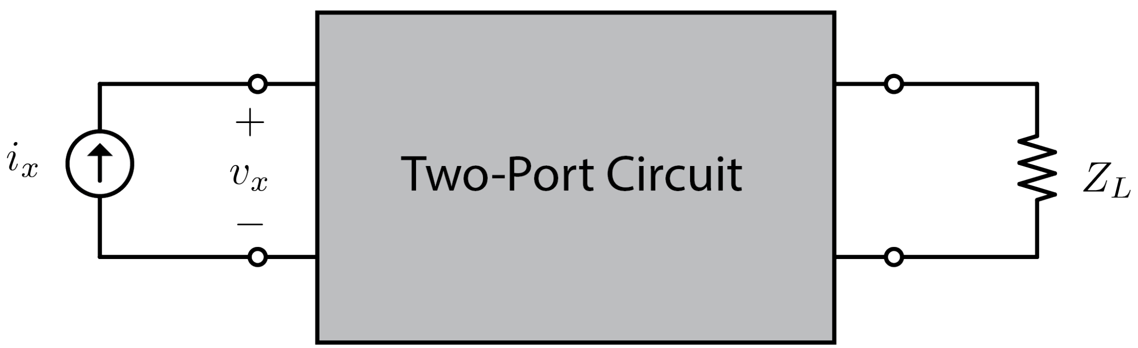
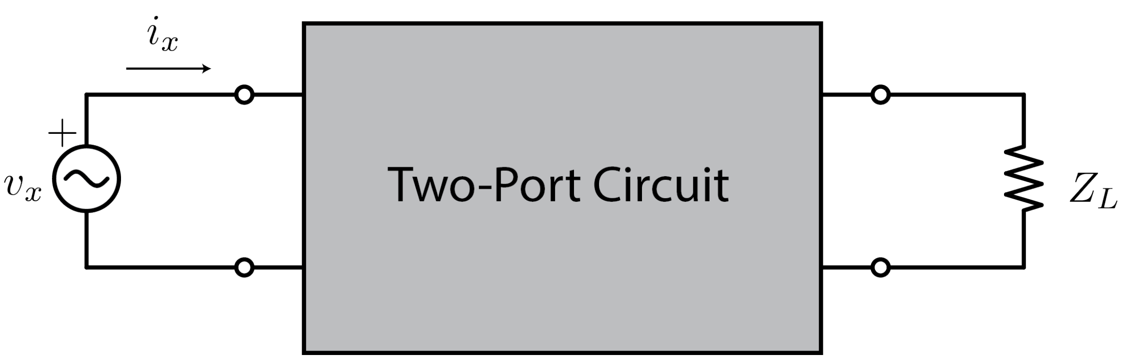
Input Impedance Z_{in}

Looks like a Thevenin resistance measurement, but note that the output port has the load resistance attached



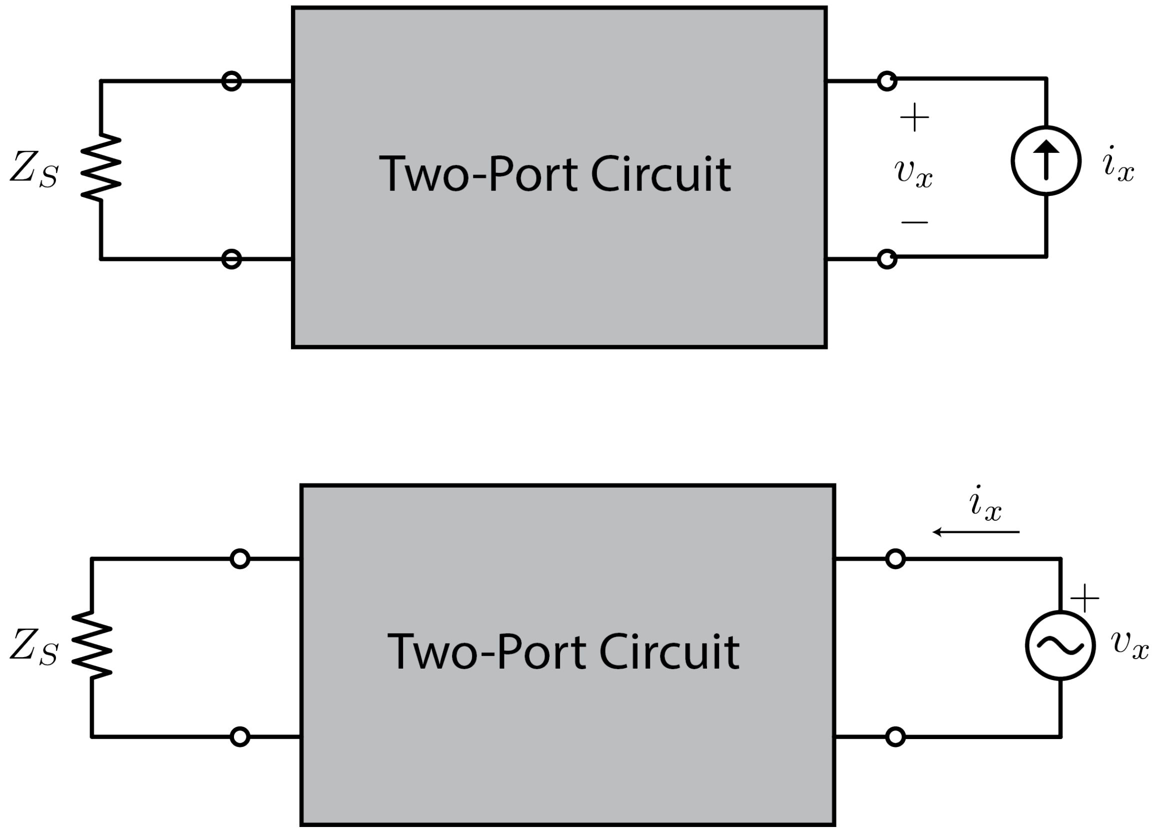
$$Z_{in} = \left.\frac{v_x}{i_x}\right|_{Z_S removed,\; Z_L attached}$$



Output Impedance Z_{out}

Looks like a Thevenin resistance measurement, but note that the *input* port has the *source* resistance attached

$$Z_{out} = \left.\frac{v_x}{i_x}\right|_{\substack{Z_L removed, \\ Z_S attached}}$$



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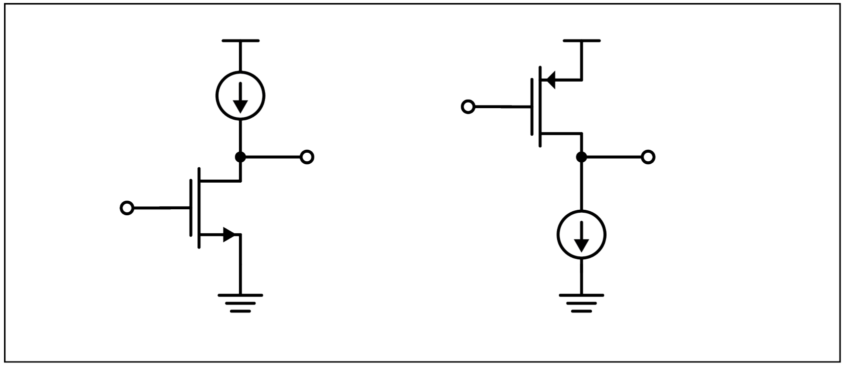
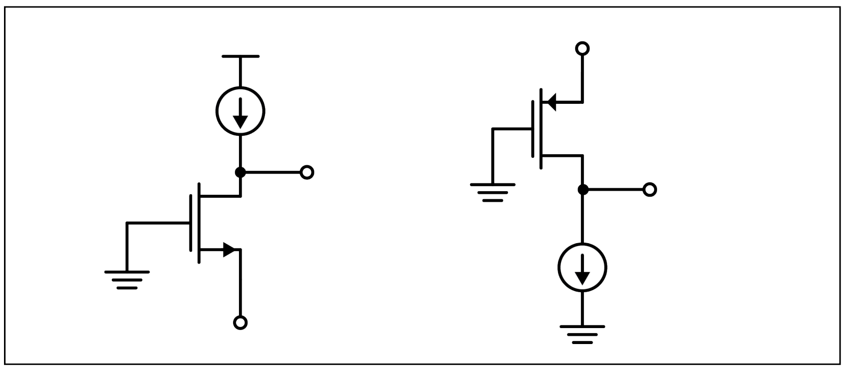
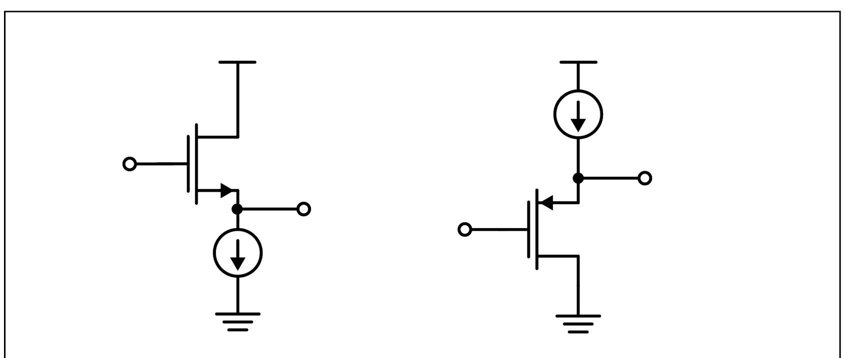
Single-Stage Amplifier Types



Common Source (CS)



Common Gate (CG)

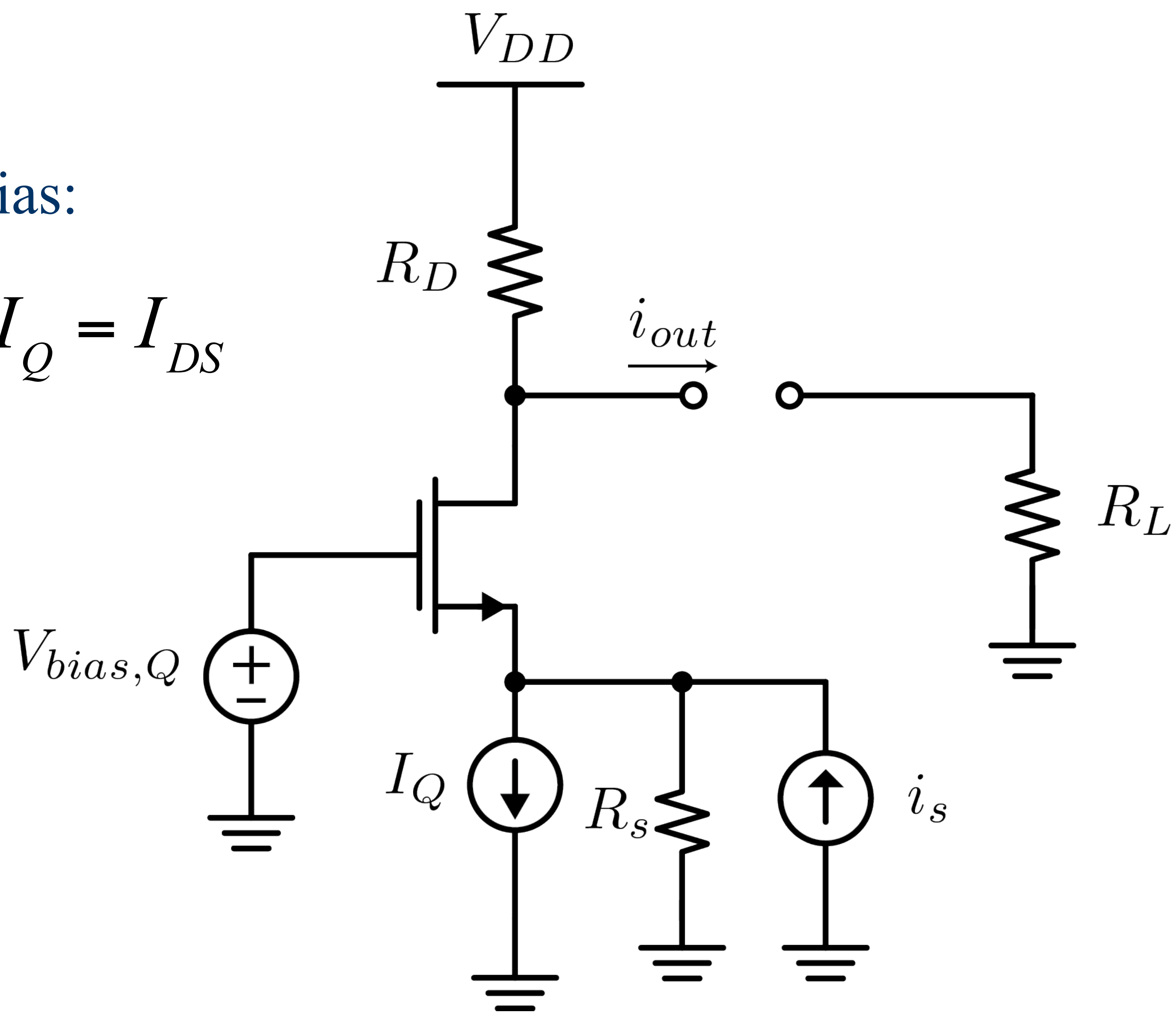


Common Drain (CD)

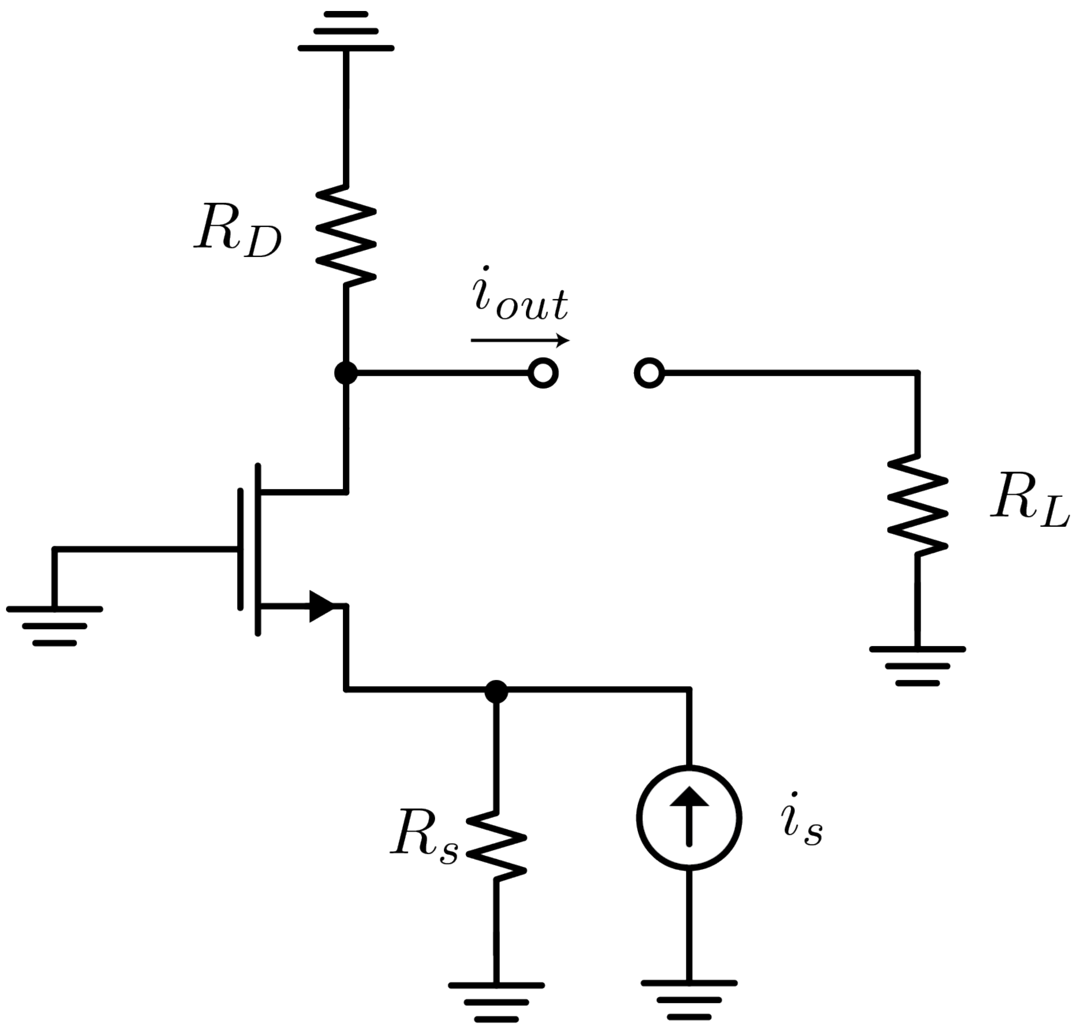
Common Gate (CG) Amplifier

DC bias:

$$I_{SUP} = I_Q = I_{DS}$$



Common Gate AC Model



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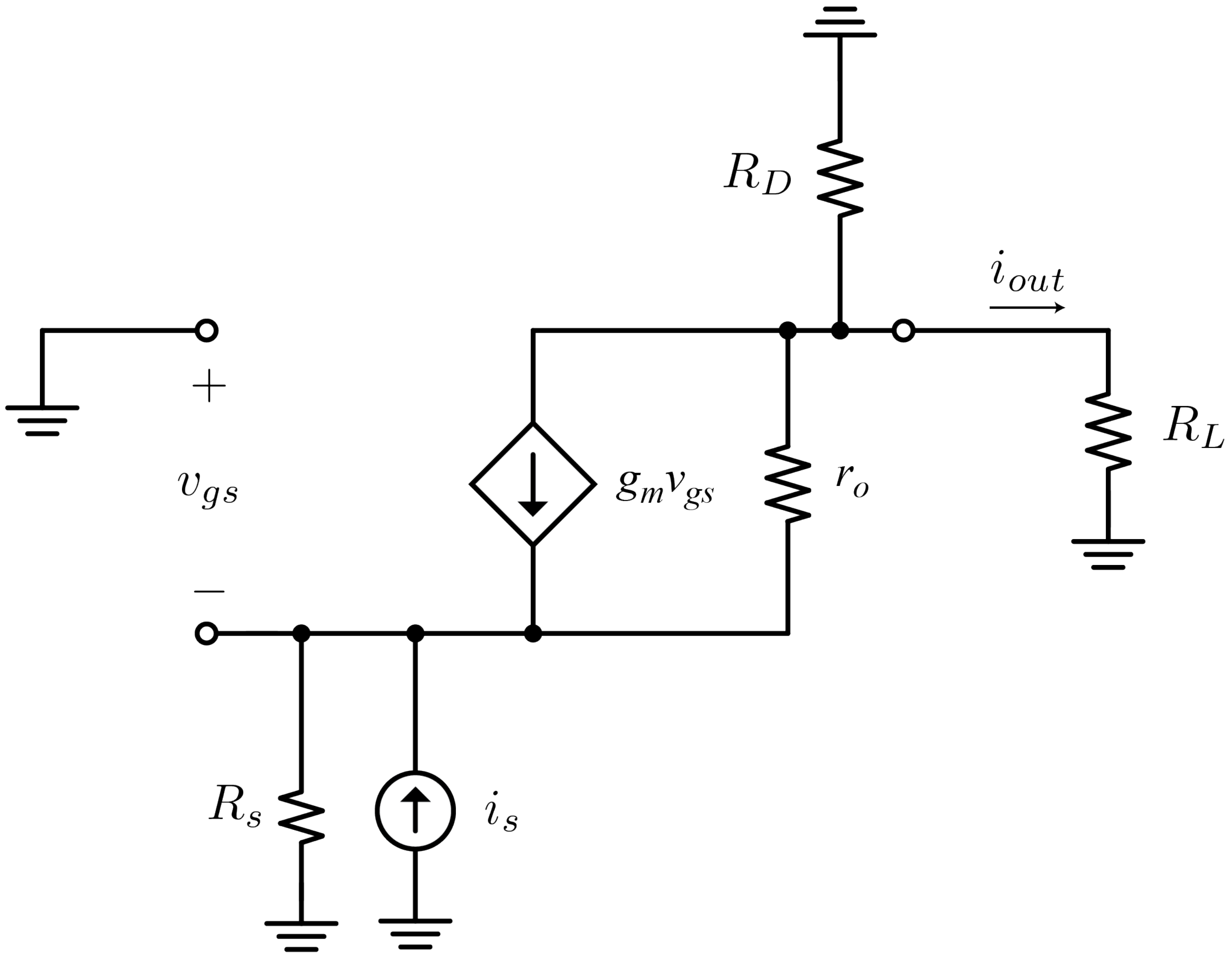
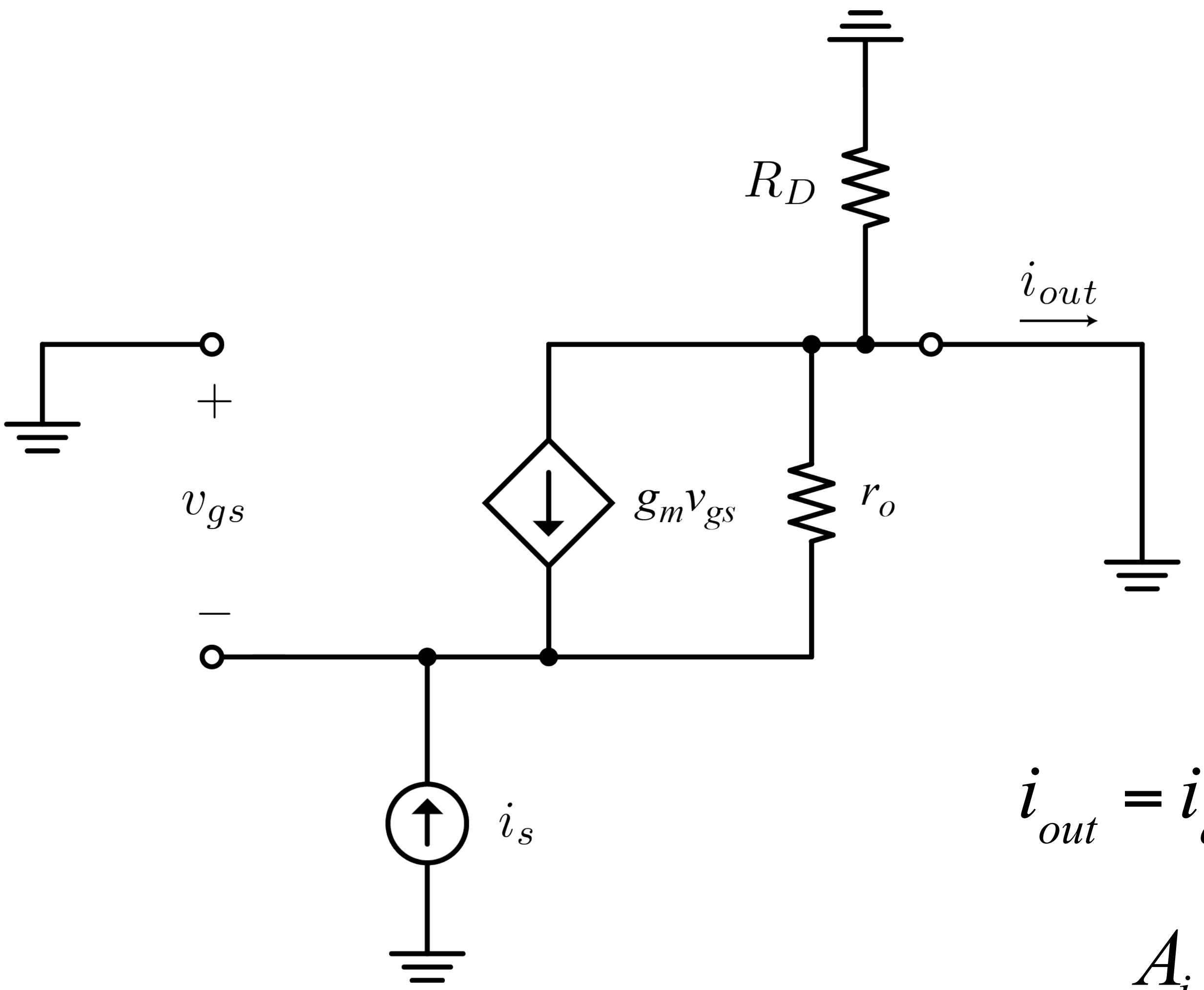
Common Gate Small Signal



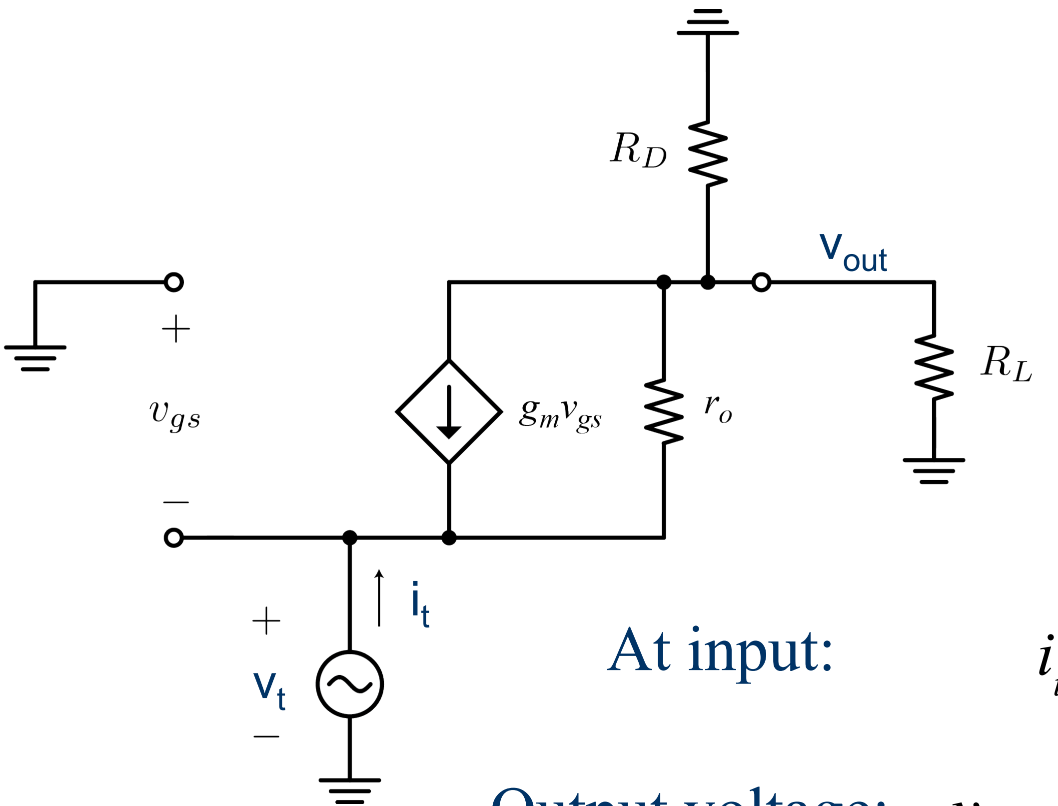
CG as a Current Amplifier: Find A_i



$$i_{out} = i_d = -i_s$$

$$A_i = -1$$

CG Input Resistance



At input: $$i_t = -g_m v_{gs} + \left(\frac{v_t - v_{out}}{r_o}\right)$$

Output voltage: $$v_{out} = -i_d (R_D \| R_L) = i_t (R_D \| R_L)$$

$$i_t = g_m v_t + \left(\frac{v_t - (R_D \| R_L) i_t}{r_o}\right)$$

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Approximations…

- We have this messy result

$$\frac{1}{R_{in}} = \frac{i_t}{v_t} = \frac{g_m + \dfrac{1}{r_o}}{1 + \dfrac{R_D \| R_L}{r_o}}$$

- But we don't need that much precision. Let's start approximating:

$$g_m >> \frac{1}{r_o} \qquad R_D \| R_L \approx R_L \qquad \frac{R_L}{r_o} \approx 0$$

$$R_{in} = \frac{1}{g_m}$$

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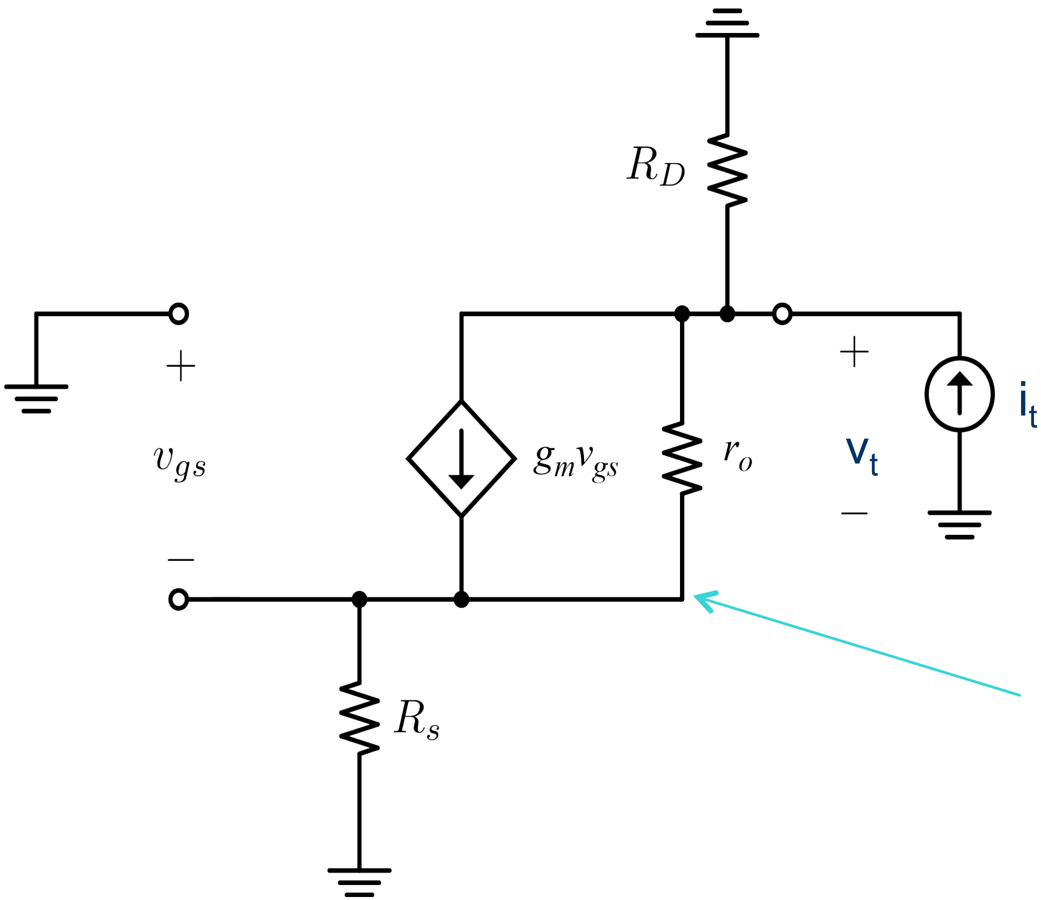
CG Output Resistance



$$\frac{v_s}{R_S} - g_m v_{gs} + \frac{v_s - v_t}{r_o} = 0$$

$$v_s \left(\frac{1}{R_S} + g_m + \frac{1}{r_o} \right) = \frac{v_t}{r_o}$$

CG Output Resistance

Substituting $v_s = i_t R_S$

$$i_t R_S \left(\frac{1}{R_S} + g_m + \frac{1}{r_o} \right) = \frac{v_t}{r_o}$$

The output resistance is $(v_t / i_t) \| R_D$

$$R_{out} = R_D \| \left(R_S \left(\frac{r_o}{R_S} + g_m r_o + 1 \right) \right)$$

$$R_{out} = R_D \| \left(r_o + g_m r_o R_S + R_S \right)$$

Approximating the CG R_{out}

The exact result is complicated, so let's try to make it simpler:

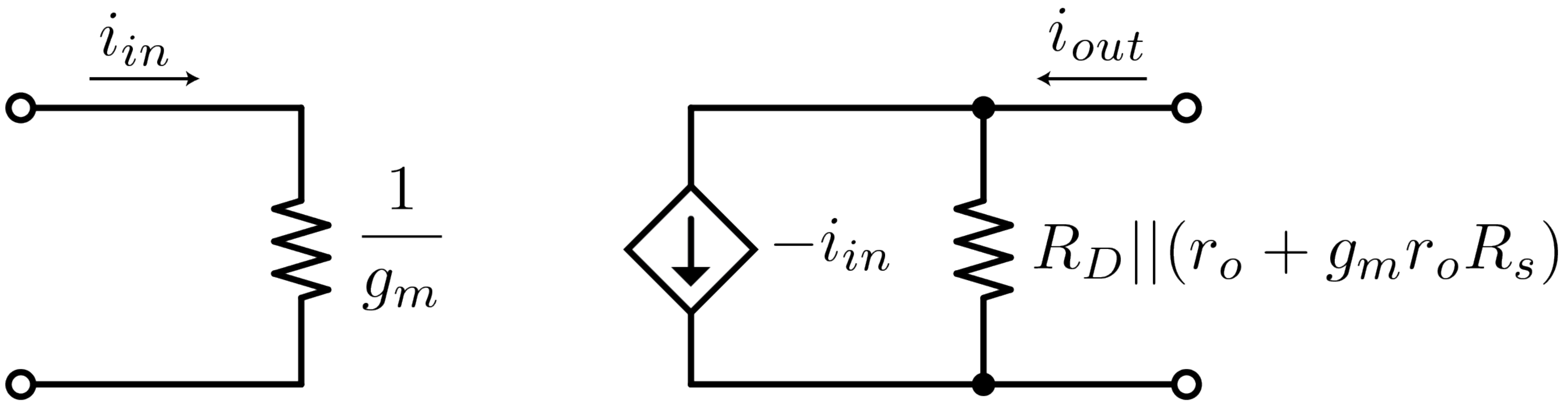
$$g_m \approx 500\mu S \qquad r_o \approx 200k\Omega$$

$$R_{out} \cong R_D \,||\, [r_o + g_m r_o R_S + R_S]$$

Assuming the source resistance is less than r_o,

$$R_{out} \approx R_D \,||\, [r_o + g_m r_o R_S] = R_D \,||\, [r_o(1 + g_m R_S)]$$

CG Two-Port Model



Function: a current buffer

- Low Input Impedance
- High Output Impedance

Common Gate as a "V Amplifier"

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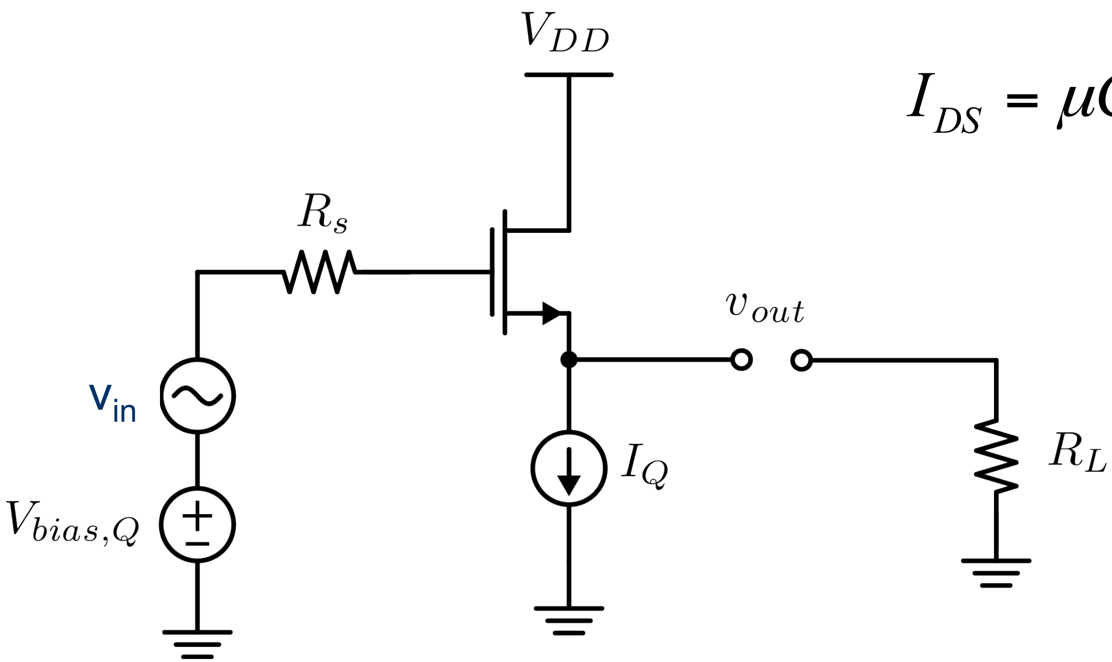
Common-Drain Amplifier

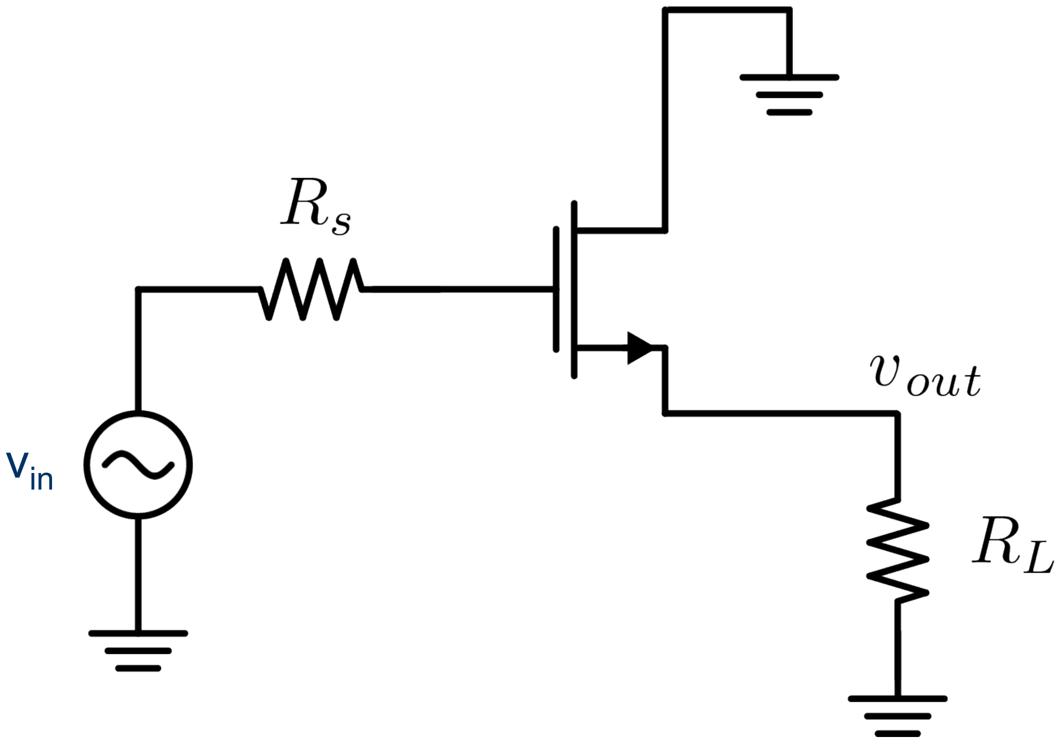


$$I_{DS} = \mu C_{ox} \frac{W}{L} \frac{1}{2} (V_{GS} - V_T)^2$$

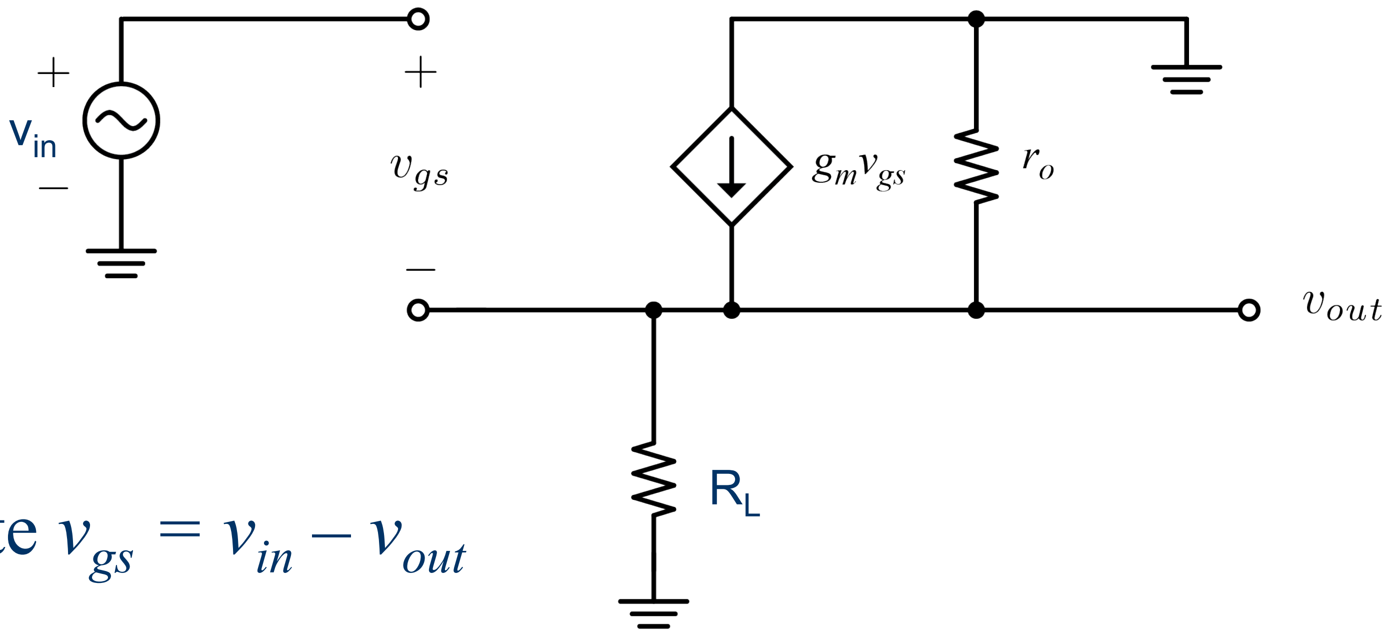
$$V_{GS} = V_T + \sqrt{\frac{2 I_{DS}}{\mu C_{ox} \frac{W}{L}}}$$

Weak I_{DS} dependence

Common Drain AC Schematic



CD Voltage Gain



Note $v_{gs} = v_{in} - v_{out}$

$$\frac{v_{out}}{R_L \parallel r_o} = g_m v_{gs}$$

$$\frac{v_{out}}{R_L \parallel r_o} = g_m \left(v_{in} - v_{out} \right)$$

CD Voltage Gain (Cont.)

KCL at source node: $$\frac{v_{out}}{R_L \parallel r_o} = g_m\left(v_{in} - v_{out}\right)$$

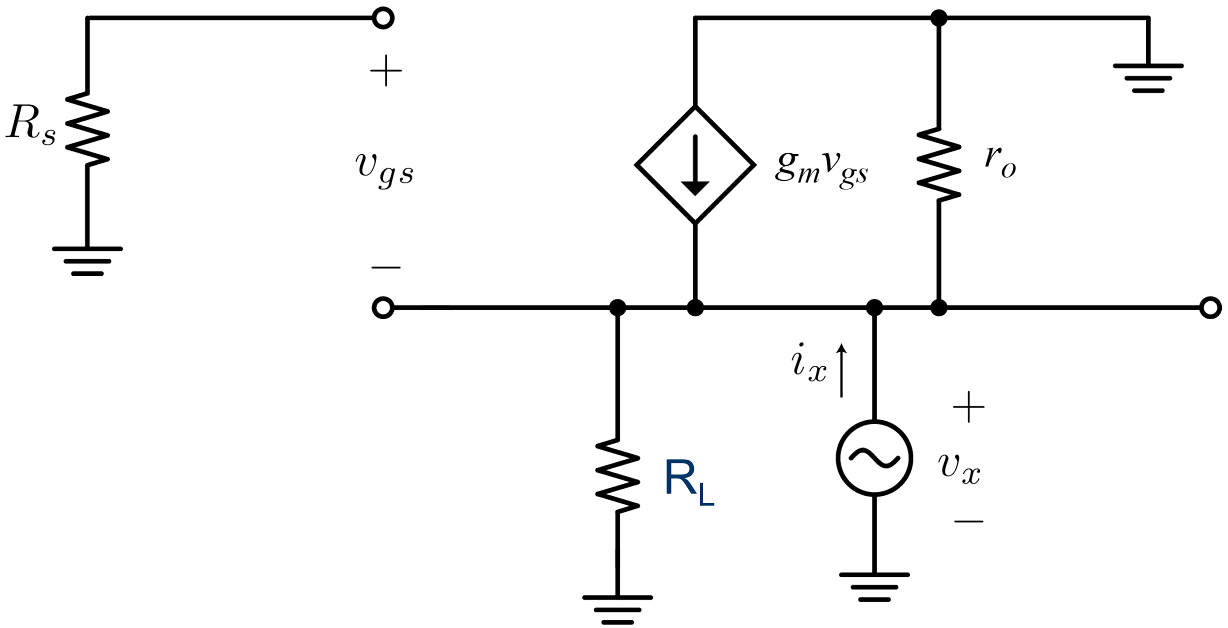
$$\left(\frac{1}{R_L \parallel r_o} + g_m\right)v_{out} = g_m v_{in}$$

Voltage gain:

$$\frac{v_{out}}{v_{in}} = \frac{g_m}{\dfrac{1}{R_L \parallel r_o} + g_m}$$

$$\frac{v_{out}}{v_{in}} \approx \frac{g_m}{1/R_L + g_m} \approx 1$$

CD Output Resistance

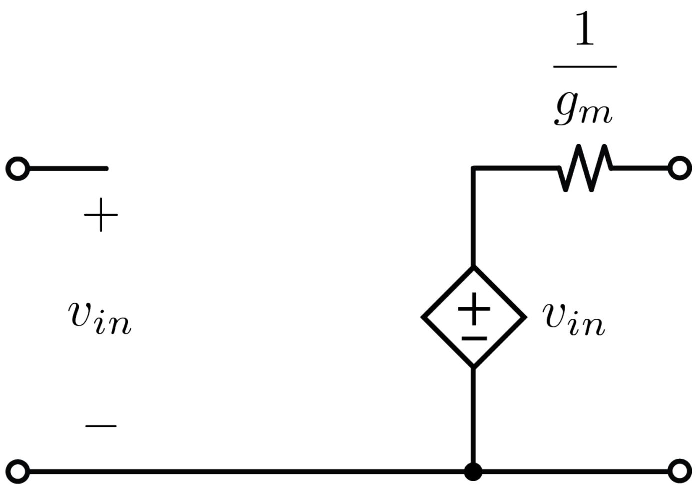


Sum currents at output (source) node:

$$i_x = g_m v_x \qquad R_{out} = r_o \,||\, R_L \,||\, \frac{v_x}{i_x} \qquad R_{out} \approx \frac{1}{g_m}$$

CD Output Resistance (Cont.)

$r_o \| R_L$ is much larger than the inverses of the transconductances → ignore



Function: a voltage buffer

- High Input Impedance
- Low Output Impedance

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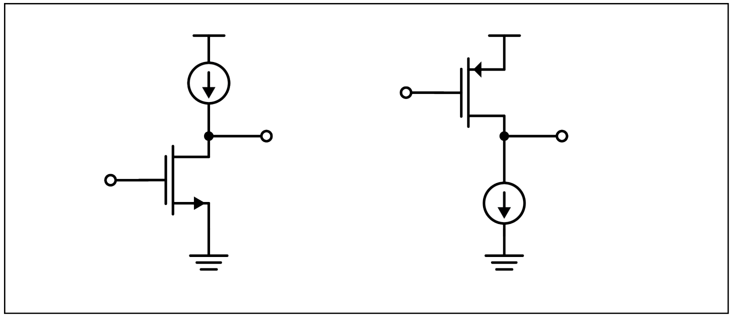
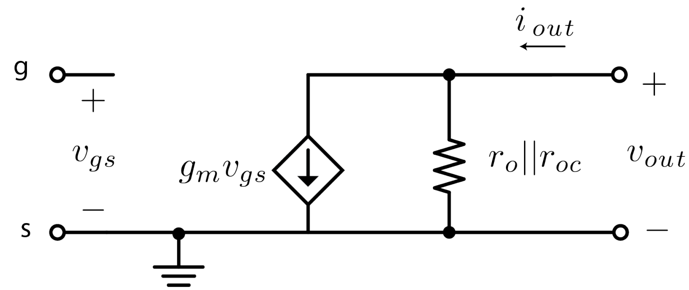
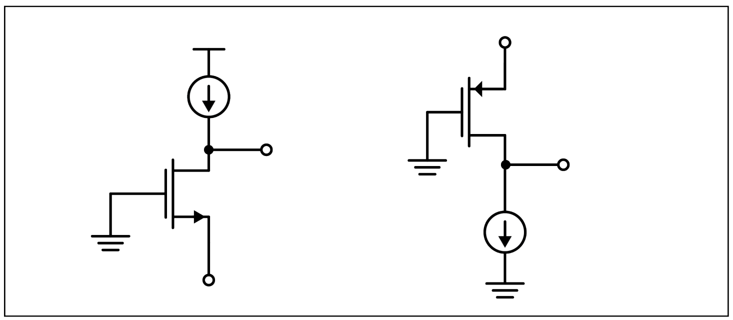
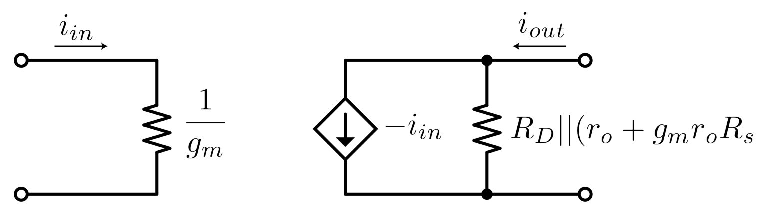
Transistor Amplifiers → Gm/V/I



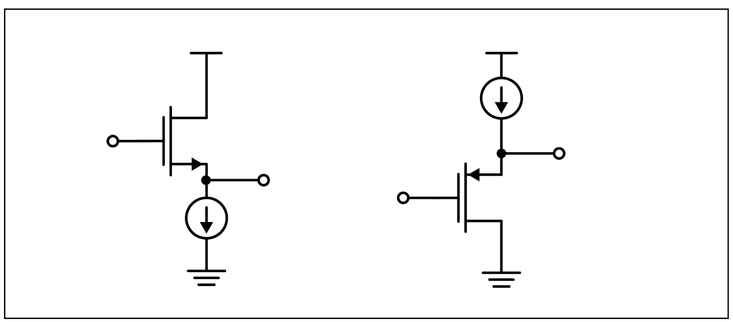


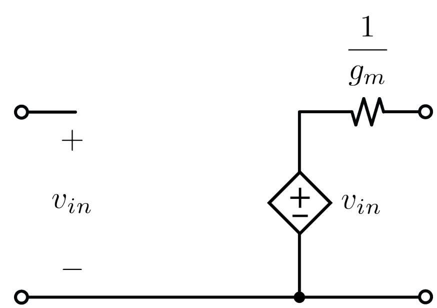
Gm Amplifier
Common Source





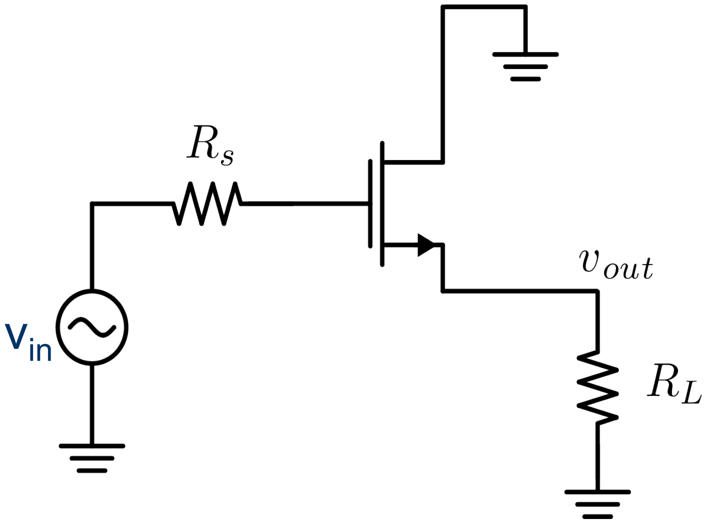
I-Buffer
Common Gate

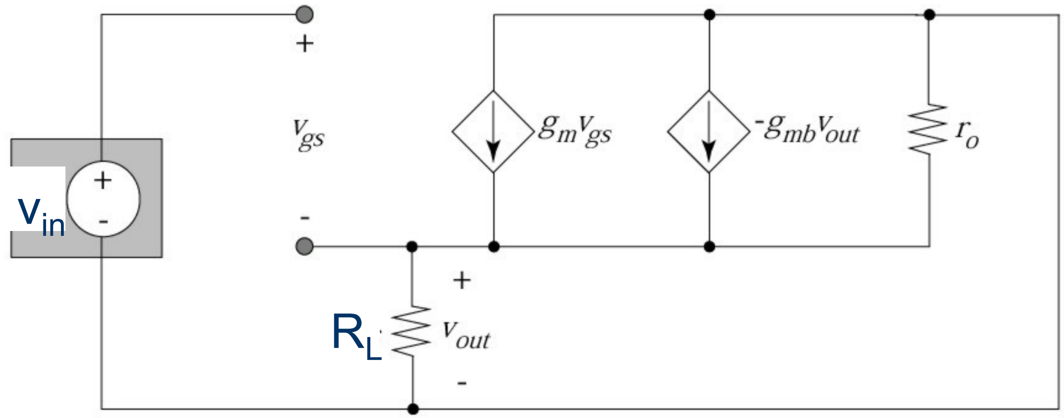




V-Buffer
Source Follower

Body Effect





If the backgate is tied to ground you cannot ignore the body effect. How does this effect the gain?

$$\frac{v_{out}}{R_L \| r_o} = g_m v_{gs} - g_{mb} v_{out}$$

$$\frac{v_{out}}{v_{in}} = ?$$