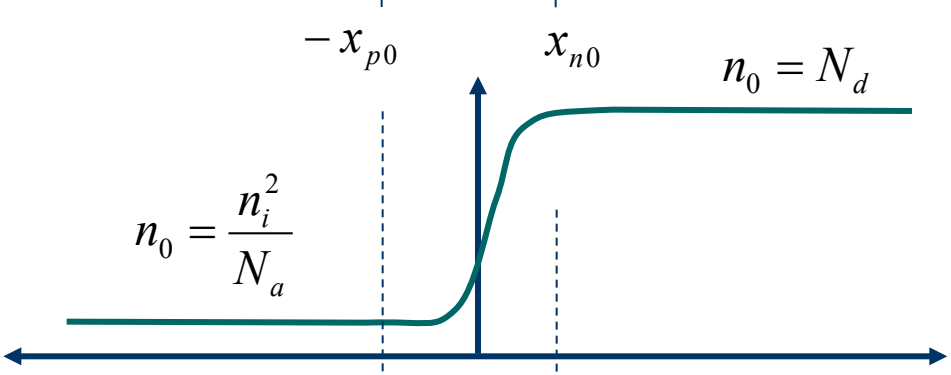
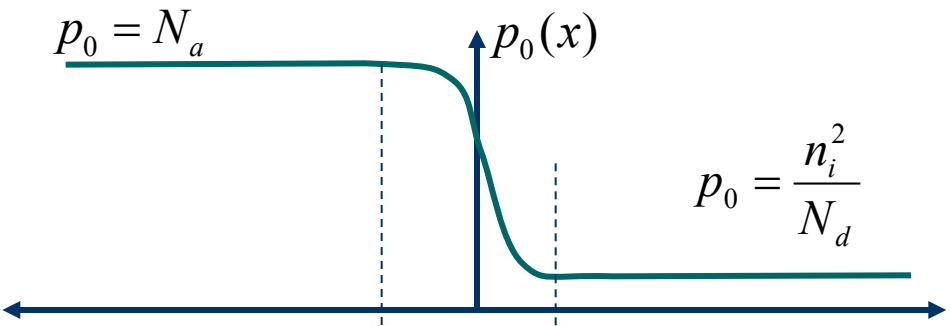
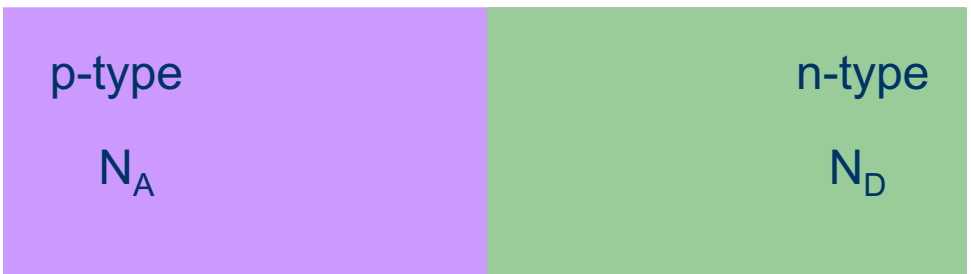


Module 2.3: PN Junctions

Prof. Ali M. Niknejad
Prof. Rikky Muller



What is a pn-junction?



Transition Region

AKA: diode

Module 2.3 Outline

- Part 1: Carrier concentration variation and potential
 - Show that any time there's a variation in carrier concentration, then at thermal equilibrium there must be a variation in potential
- Part 2: Apply this to a pn-junction at thermal equilibrium
 - Extend result to a reverse biased junction
- Part 3: Look at a forward biased pn-junction

Carrier Concentration and Potential

- In thermal equilibrium, there are no external fields and we thus expect the electron and hole current densities to be zero:

$$J_n = 0 = qn_o\mu_n E_0 + qD_n \frac{dn_o}{dx}$$

$$\frac{dn_o}{dx} = -\left(\frac{\mu_n}{D_n}\right)n_o E_0 = \left(\frac{q}{kT}\right)n_o \frac{d\phi_0}{dx}$$

$$d\phi_0 = \left(\frac{kT}{q}\right)\frac{dn_o}{n_o} = V_{th} \frac{dn_o}{n_o}$$

Carrier Concentration and Potential (2)

- We have an equation relating the potential to the carrier concentration

$$d\phi_0 = \left(\frac{kT}{q} \right) \frac{dn_o}{n_0} = V_{th} \frac{dn_0}{n_0}$$

- If we integrate the above equation we have

$$\phi_0(x) - \phi_0(x_0) = V_{th} \ln \frac{n_0(x)}{n_0(x_0)}$$

- We define the potential reference to be intrinsic Si:

$$\phi_0(x_0) = 0 \quad n_0(x_0) = n_i$$

Carrier Concentration Versus Potential

- The carrier concentration is thus a function of potential

$$n_0(x) = n_i e^{\phi_0(x)/V_{th}}$$

- Check that for zero potential, we have intrinsic carrier concentration (reference).
- If we do a similar calculation for holes, we arrive at a similar equation

$$p_0(x) = n_i e^{-\phi_0(x)/V_{th}}$$

- Note that the law of mass action is upheld

$$n_0(x)p_0(x) = n_i^2 e^{-\phi_0(x)/V_{th}} e^{\phi_0(x)/V_{th}} = n_i^2$$

The Doping Changes Potential

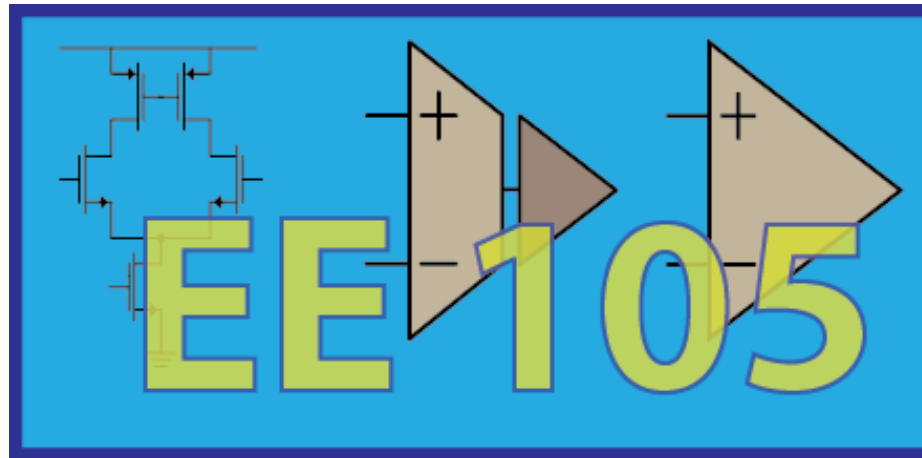
- Due to the log nature of the potential, the potential changes linearly for exponential increase in doping:

$$\phi_0(x) = V_{th} \ln \frac{n_0(x)}{n_i(x_0)} = 26\text{mV} \ln \frac{n_0(x)}{n_i(x_0)} \approx 26\text{mV} \ln 10 \log \frac{n_0(x)}{10^{10}}$$

$$\phi_0(x) \approx 60\text{mV} \log \frac{n_0(x)}{10^{10}}$$

$$\phi_0(x) \approx -60\text{mV} \log \frac{p_0(x)}{10^{10}}$$

- Quick calculation aid: For a p-type concentration of 10^{16} cm^{-3} , the potential is -360 mV
- N-type materials have a positive potential with respect to intrinsic Si



Reversed Biased PN Junctions

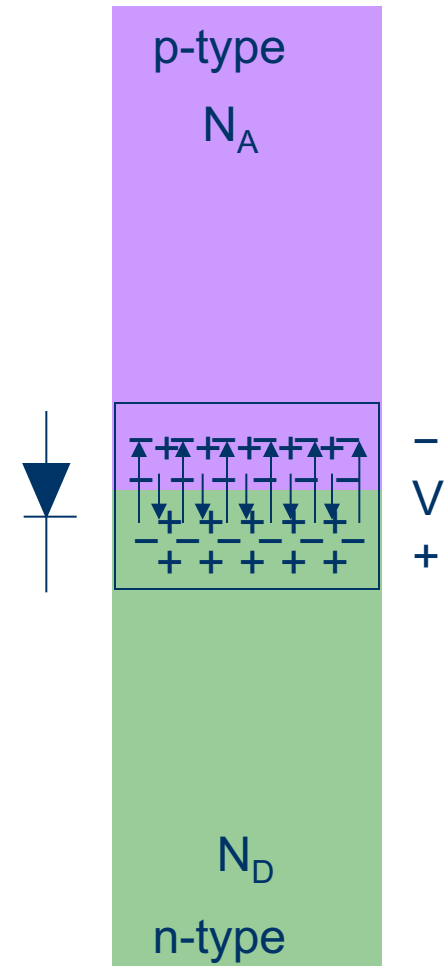
Prof. Ali M. Niknejad

Prof. Rikky Muller



PN Junctions: Overview

- The most important device is a junction between a p-type region and an n-type region
- When the junction is first formed, due to the concentration gradient, mobile charges transfer near junction
- Electrons leave n-type region and holes leave p-type region
- These mobile carriers become minority carriers in new region (can't penetrate far due to recombination)
- Due to charge transfer, a voltage difference occurs between regions
- This creates a field at the junction that causes drift currents to oppose the diffusion current
- In thermal equilibrium, drift current and diffusion must balance



PN Junction Currents

- Consider the PN junction in thermal equilibrium
- Again, the currents have to be zero, so we have

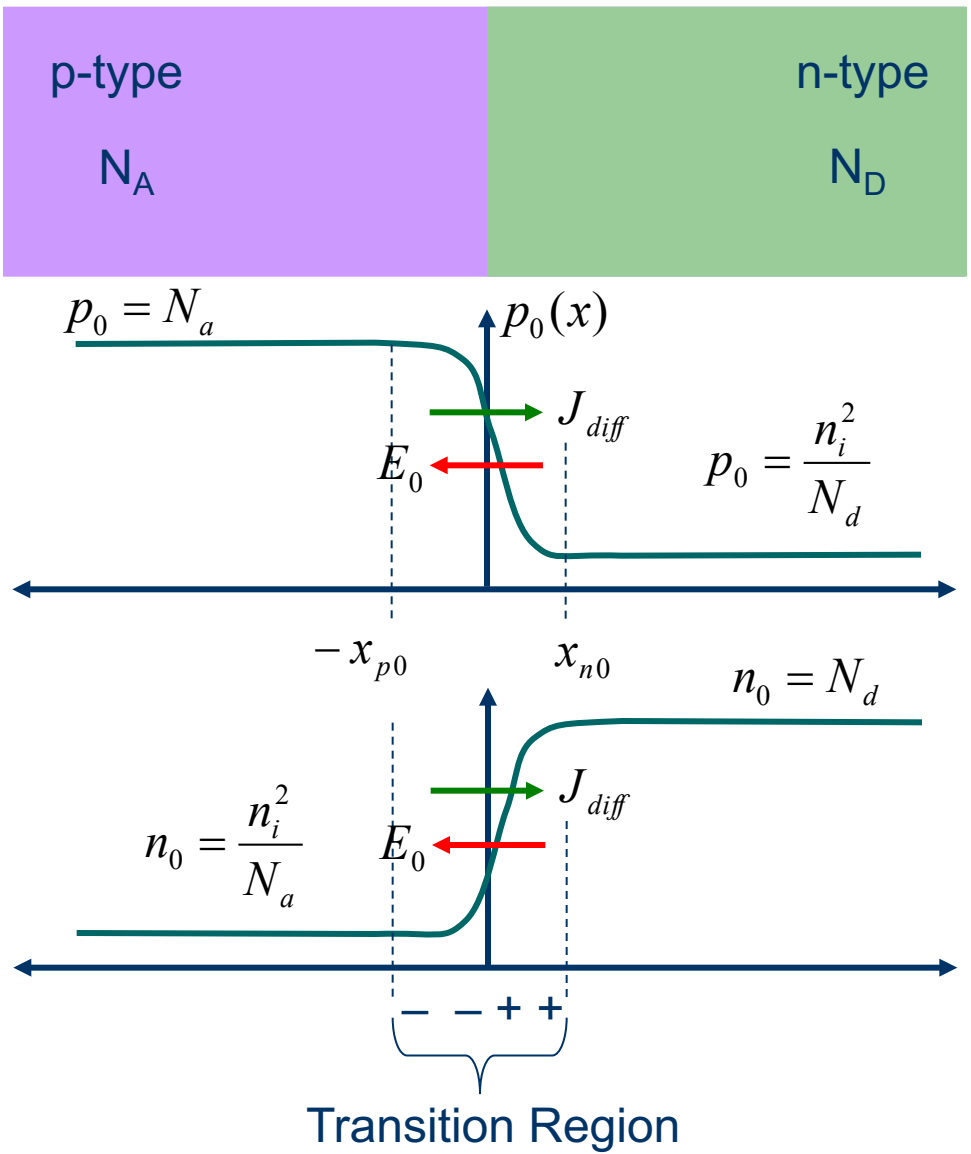
$$J_n = 0 = qn_0\mu_n E_0 + qD_n \frac{dn_o}{dx}$$

$$qn_0\mu_n E_0 = -qD_n \frac{dn_o}{dx}$$

$$E_0 = \frac{-D_n \frac{dn_o}{dx}}{n_0\mu_n} = -\frac{kT}{q} \frac{1}{n_0} \frac{dn_o}{dx}$$

$$E_0 = \frac{D_p \frac{dp_o}{dx}}{n_0\mu_p} = -\frac{kT}{q} \frac{1}{p_0} \frac{dp_o}{dx}$$

PN Junction Fields



Total Charge in Transition Region

- To solve for the electric fields, we need to write down the charge density in the transition region:

$$\rho_0(x) = q(p_0 - n_0 + N_d - N_a)$$

- In the p-side of the junction, there are very few electrons and only acceptors:

$$\rho_0(x) \approx q(p_0 - N_a) \quad -x_{p0} < x < 0$$

- Since the hole concentration is decreasing on the p-side, the net charge is negative:

$$N_a > p_0 \quad \rho_0(x) < 0$$

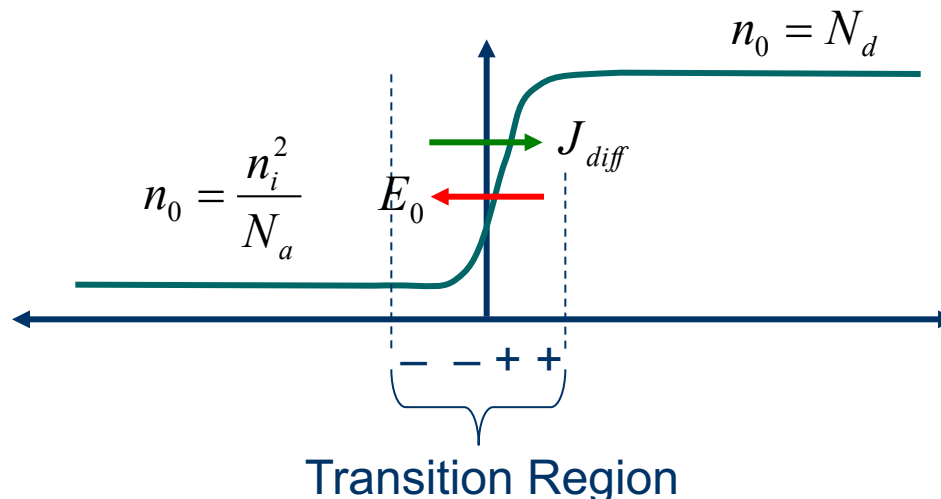
Charge on N-Side

- Analogous to the p-side, the charge on the n-side is given by:

$$\rho_0(x) \approx q(-n_0 + N_d) \quad 0 < x < x_{n0}$$

- The net charge here is positive since:

$$N_d > n_0 \quad \rho_0(x) > 0$$



“Exact” Solution for Fields

- Given the above approximations, we now have an expression for the charge density

$$\rho_0(x) \cong \begin{cases} q(n_i e^{-\phi_0(x)/V_{th}} - N_a) & -x_{po} < x < 0 \\ q(N_d - n_i e^{\phi_0(x)/V_{th}}) & 0 < x < x_{n0} \end{cases}$$

- We also have the following result from electrostatics

$$\frac{dE_0}{dx} = -\frac{d^2\phi}{dx^2} = \frac{\rho_0(x)}{\epsilon_s}$$

- Notice that the potential appears on both sides of the equation... difficult problem to solve
- A much simpler way to solve the problem...

Depletion Approximation

- Let's assume that the transition region is completely depleted of free carriers (only immobile dopants exist)
- Then the charge density is given by

$$\rho_0(x) \cong \begin{cases} -qN_a & -x_{p0} < x < 0 \\ +qN_d & 0 < x < x_{n0} \end{cases}$$

- The solution for electric field is now easy

$$\frac{dE_0}{dx} = \frac{\rho_0(x)}{\epsilon_s}$$

$$E_0(x) = \int_{-x_{p0}}^x \frac{\rho_0(x')}{\epsilon_s} dx' + E_0(-x_{p0})$$

Field zero outside transition region

Depletion Approximation (2)

- Since charge density is a constant

$$E_0(x) = \int_{-x_{p0}}^x \frac{\rho_0(x')}{\epsilon_s} dx' = -\frac{qN_a}{\epsilon_s} (x + x_{p0})$$

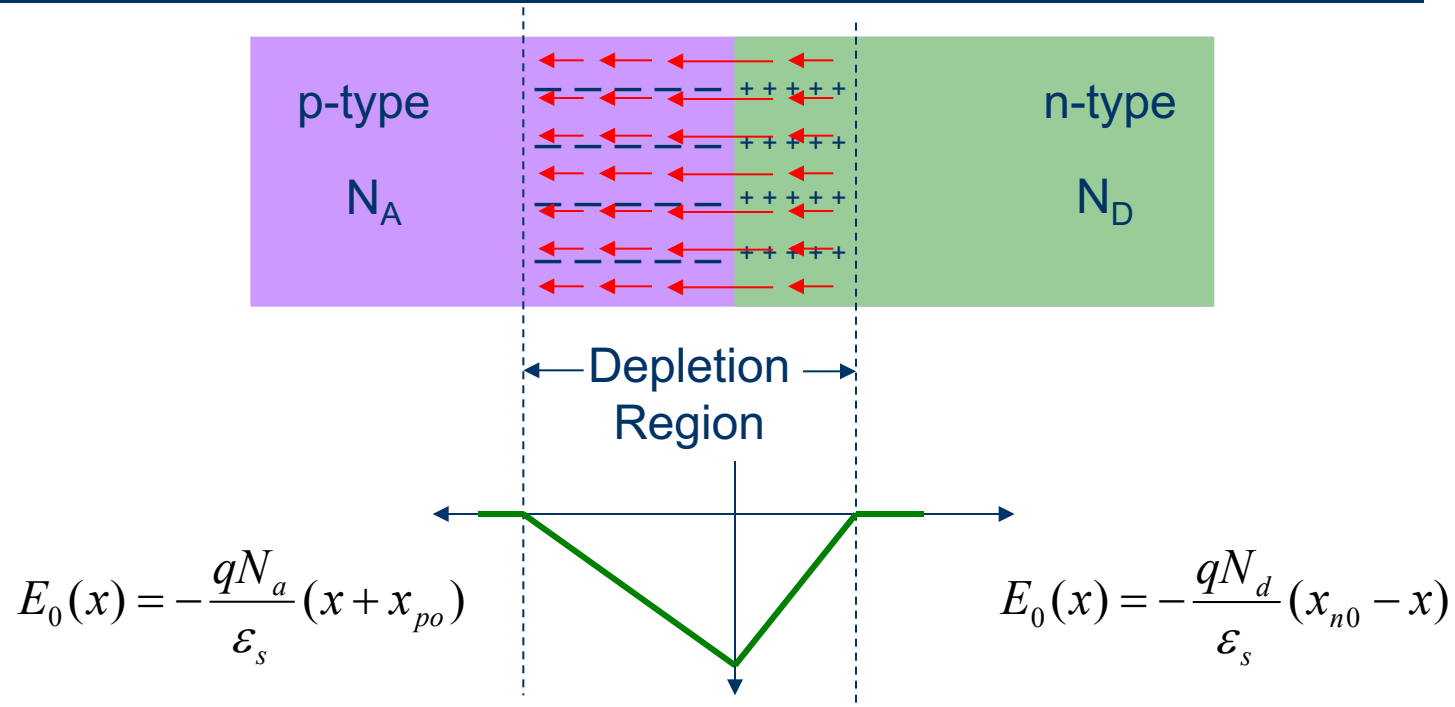
- If we start from the n-side we get the following result

$$E_0(x_{n0}) = \int_x^{x_{n0}} \frac{\rho_0(x')}{\epsilon_s} dx' + E_0(x) = \frac{qN_d}{\epsilon_s} (x_{n0} - x) + E_0(x)$$

Field zero outside
transition region

$$E_0(x) = -\frac{qN_d}{\epsilon_s} (x_{n0} - x)$$

Plot of Fields In Depletion Region



- E-Field zero outside of depletion region
- Note the asymmetrical depletion widths
- Which region has higher doping?
- Slope of E-Field larger in n-region. Why?
- Peak E-Field at junction. Why continuous?

Continuity of E-Field Across Junction

- Recall that E-Field diverges on charge. For a sheet charge at the interface, the E-field could be discontinuous
- In our case, the depletion region is only populated by a background density of fixed charges so the E-Field is continuous
- What does this imply?

$$E_0^n(x=0) = -\frac{qN_a}{\epsilon_s} x_{po} = -\frac{qN_d}{\epsilon_s} x_{no} = E_0^p(x=0)$$

$$qN_a x_{po} = qN_d x_{no}$$

- Total fixed charge in n-region equals fixed charge in p-region! Somewhat obvious result.

Potential Across Junction

- From our earlier calculation we know that the potential in the n-region is higher than p-region
- The potential has to smoothly transition from high to low in crossing the junction
- Physically, the potential difference is due to the charge transfer that occurs due to the concentration gradient
- Let's integrate the field to get the potential:

$$\phi(x) = \phi(-x_{p0}) + \int_{-x_{p0}}^x \frac{qN_a}{\epsilon_s} (x' + x_{p0}) dx'$$

$$\phi(x) = \phi_p + \frac{qN_a}{\epsilon_s} \left(\frac{x'^2}{2} + x'x_{p0} \right) \Big|_{-x_{p0}}^x$$

Potential Across Junction

- We arrive at potential on p-side (parabolic)

$$\phi_o^p(x) = \phi_p + \frac{qN_a}{2\epsilon_s} (x + x_{p0})^2$$

- Do integral on n-side

$$\phi_n(x) = \phi_n - \frac{qN_d}{2\epsilon_s} (x - x_{n0})^2$$

- Potential *must* be continuous at interface (field finite at interface)

$$\phi_n(0) = \phi_n - \frac{qN_d}{2\epsilon_s} x_{n0}^2 = \phi_p + \frac{qN_a}{2\epsilon_s} x_{p0}^2 = \phi_p(0)$$

Solve for Depletion Lengths

- We have two equations and two unknowns. We are finally in a position to solve for the depletion depths

$$\phi_n - \frac{qN_d}{2\epsilon_s} x_{n0}^2 = \phi_p + \frac{qN_a}{2\epsilon_s} x_{p0}^2 \quad (1)$$

$$qN_a x_{p0} = qN_d x_{n0} \quad (2)$$

$$x_{n0} = \sqrt{\frac{2\epsilon_s \phi_{bi}}{qN_d} \left(\frac{N_a}{N_a + N_d} \right)} \quad x_{p0} = \sqrt{\frac{2\epsilon_s \phi_{bi}}{qN_a} \left(\frac{N_d}{N_d + N_a} \right)}$$

$$\phi_{bi} \equiv \phi_n - \phi_p > 0$$

Sanity Check

- Does the above equation make sense?
- Let's say we dope one side very highly. Then physically we expect the depletion region width for the heavily doped side to approach zero:

$$x_{n0} = \lim_{N_d \rightarrow \infty} \sqrt{\frac{2\varepsilon_s \phi_{bi}}{qN_d} \frac{N_d}{N_d + N_a}} = 0 \quad \checkmark$$

$$x_{p0} = \lim_{N_d \rightarrow \infty} \sqrt{\frac{2\varepsilon_s \phi_{bi}}{qN_a} \left(\frac{N_d}{N_d + N_a} \right)} = \sqrt{\frac{2\varepsilon_s \phi_{bi}}{qN_a}}$$

- Entire depletion width dropped across p-region

Total Depletion Width

- The sum of the depletion widths is the “space charge region”

$$X_{d0} = x_{p0} + x_{n0} = \sqrt{\frac{2\epsilon_s \phi_{bi}}{q} \left(\frac{1}{N_a} + \frac{1}{N_d} \right)}$$

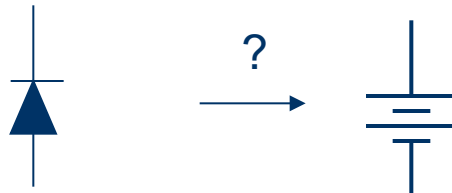
- This region is essentially depleted of all mobile charge
- Due to high electric field, carriers move across region at velocity saturated speed

$$X_{d0} = \sqrt{\frac{2\epsilon_s \phi_{bi}}{q} \left(\frac{1}{10^{15}} \right)} \approx 1\mu \qquad E_{pn} \approx \frac{1\text{V}}{1\mu} = 10^4 \frac{\text{V}}{\text{cm}}$$

Have we invented a battery?

- Can we harness the PN junction and turn it into a battery?

$$\phi_{bi} \equiv \phi_n - \phi_p = V_{th} \left(\ln \frac{N_D}{n_i} + \ln \frac{N_A}{n_i} \right) = V_{th} \ln \frac{N_D N_A}{n_i^2}$$

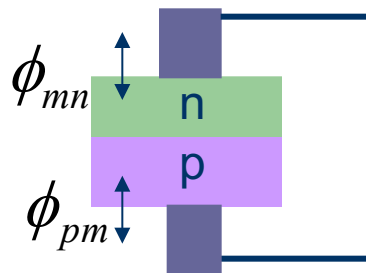
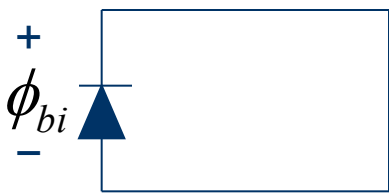


- Numerical example:

$$\phi_{bi} = 26\text{mV} \ln \frac{N_D N_A}{n_i^2} = 60\text{mV} \times \log \frac{10^{15} 10^{15}}{10^{20}} = 600\text{mV}$$

Contact Potential

- The contact between a PN junction creates a potential difference
- Likewise, the contact between two dissimilar metals creates a potential difference (proportional to the difference between the work functions)
- When a metal semiconductor junction is formed, a contact potential forms as well
- If we short a PN junction, the sum of the voltages around the loop must be zero:



$$0 = \phi_{bi} + \phi_{pm} + \phi_{mn}$$

$$\phi_{bi} = -(\phi_{pm} + \phi_{mn})$$

PN Junction Capacitor

- Under thermal equilibrium, the PN junction does not draw any (much) current
- But notice that a PN junction stores charge in the space charge region (transition region)
- Since the device is storing charge, it's acting like a capacitor
- Positive charge is stored in the n-region, and negative charge is in the p-region:

$$qN_a x_{po} = qN_d x_{no}$$

Reverse Biased PN Junction

- What happens if we “reverse-bias” the PN junction?



- Since no current is flowing, the entire reverse biased potential is dropped across the transition region
- To accommodate the extra potential, the charge in these regions must increase
- If no current is flowing, the only way for the charge to increase is to grow (shrink) the depletion regions

Voltage Dependence of Depletion Width

- Can redo the math but in the end we realize that the equations are the same except we replace the built-in potential with the effective reverse bias:

$$x_n(V_D) = \sqrt{\frac{2\epsilon_s(\phi_{bi} - V_D)}{qN_d} \left(\frac{N_a}{N_a + N_d} \right)} = x_{n0} \sqrt{1 - \frac{V_D}{\phi_{bi}}}$$

$$x_p(V_D) = \sqrt{\frac{2\epsilon_s(\phi_{bi} - V_D)}{qN_a} \left(\frac{N_d}{N_a + N_d} \right)} = x_{p0} \sqrt{1 - \frac{V_D}{\phi_{bi}}}$$

$$X_d(V_D) = x_p(V_D) + x_n(V_D) = \sqrt{\frac{2\epsilon_s(\phi_{bi} - V_D)}{q} \left(\frac{1}{N_a} + \frac{1}{N_d} \right)}$$

$$X_d(V_D) = X_{d0} \sqrt{1 - \frac{V_D}{\phi_{bi}}}$$

Charge Versus Bias

- As we increase the reverse bias, the depletion region grows to accommodate more charge

$$Q_J(V_D) = -qN_a x_p(V_D) = -qN_a \sqrt{1 - \frac{V_D}{\phi_{bi}}}$$

- Charge is *not* a linear function of voltage
- This is a non-linear capacitor
- We can define a small signal capacitance for small signals by breaking up the charge into two terms

$$Q_J(V_D + v_D) = Q_J(V_D) + q(v_D)$$

Derivation of Small Signal Capacitance

- Do a Taylor Series expansion:

$$Q_J(V_D + v_D) = Q_J(V_D) + \left. \frac{dQ_D}{dV} \right|_{V_D} v_D + \dots$$

$$C_j = C_j(V_D) = \left. \frac{dQ_j}{dV} \right|_{V=V_D} = \left. \frac{d}{dV} \left(-qN_a x_{p0} \sqrt{1 - \frac{V}{\phi_{bi}}} \right) \right|_{V=V_D}$$

$$C_j = \frac{qN_a x_{p0}}{2\phi_{bi} \sqrt{1 - \frac{V_D}{\phi_{bi}}}} = \frac{C_{j0}}{\sqrt{1 - \frac{V_D}{\phi_{bi}}}}$$

- Notice that

$$C_{j0} = \frac{qN_a x_{p0}}{2\phi_{bi}} = \frac{qN_a}{2\phi_{bi}} \sqrt{\left(\frac{2\varepsilon_s \phi_{bi}}{qN_a} \right) \left(\frac{N_d}{N_a + N_d} \right)} = \sqrt{\frac{q\varepsilon_s}{2\phi_{bi}} \frac{N_a N_d}{N_a + N_d}}$$

Physical Interpretation of Depletion Cap

$$C_{j0} = \sqrt{\frac{q\epsilon_s}{2\phi_{bi}} \frac{N_a N_d}{N_a + N_d}}$$

- Notice that the expression on the right-hand-side is just the depletion width in thermal equilibrium

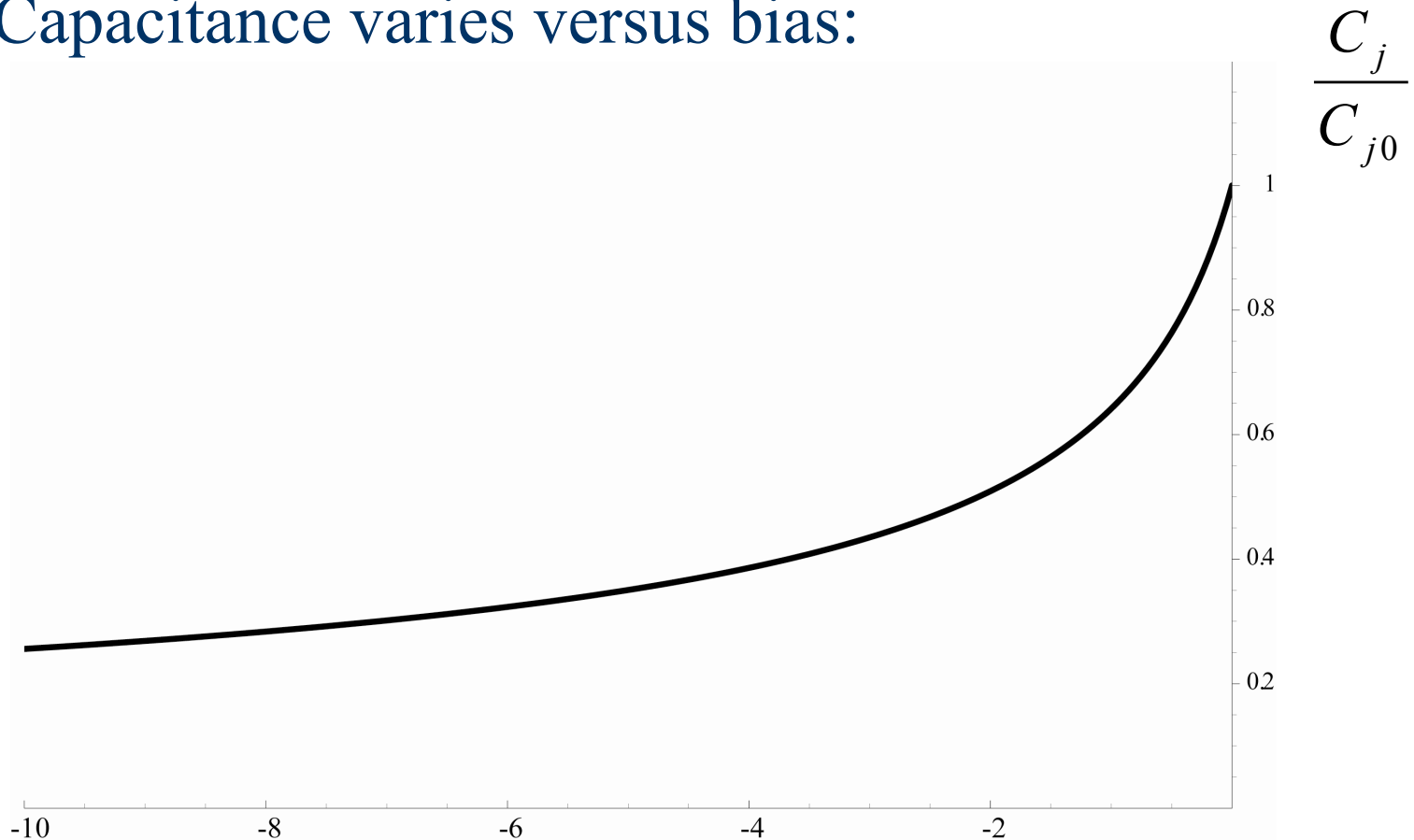
$$C_{j0} = \epsilon_s \sqrt{\frac{q}{2\epsilon_s \phi_{bi}} \left(\frac{1}{N_a} + \frac{1}{N_d} \right)^{-1}} = \frac{\epsilon_s}{X_{d0}}$$

- This looks like a parallel plate capacitor!

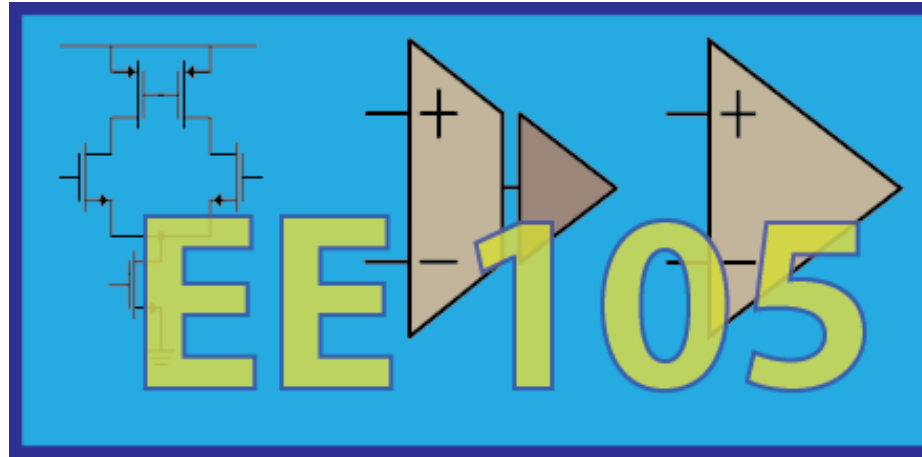
$$C_j(V_D) = \frac{\epsilon_s}{X_d(V_D)}$$

A Variable Capacitor (Varactor)

- Capacitance varies versus bias:



- Application: Radio Tuner

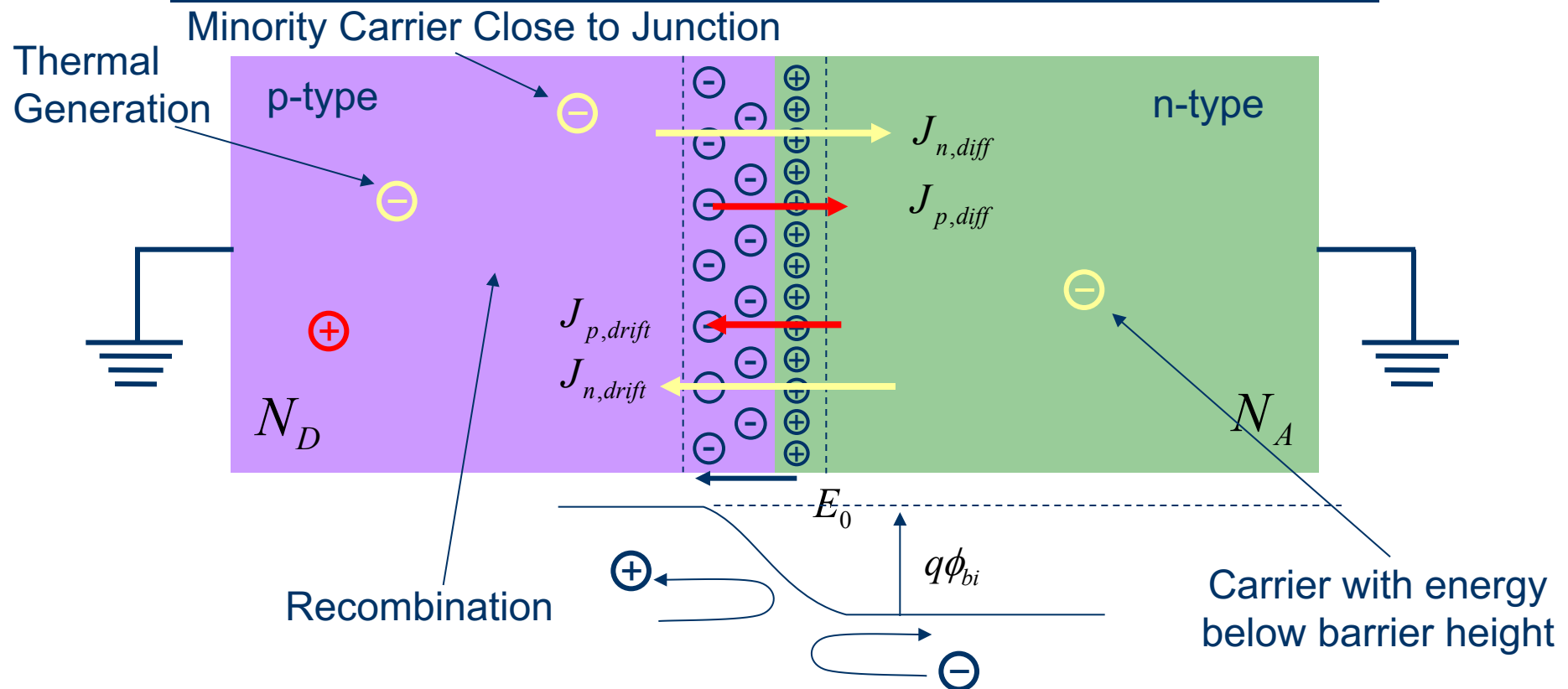


Currents in PN Junctions

Prof. Ali M. Niknejad
Prof. Rikky Muller



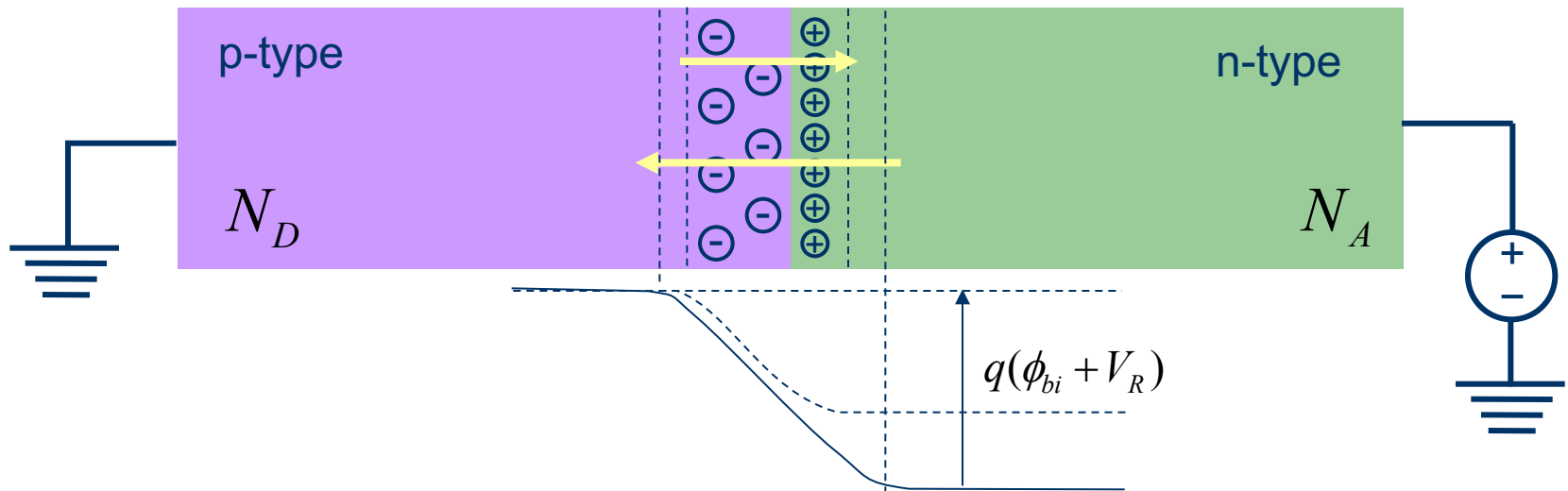
Diode under Thermal Equilibrium



- Diffusion small since few carriers have enough energy to penetrate barrier
- Drift current is small since minority carriers are few and far between: Only minority carriers generated within a diffusion length can contribute current
- **Important Point: Minority drift current independent of barrier!**
- **Diffusion current strong (exponential) function of barrier**

Reverse Bias

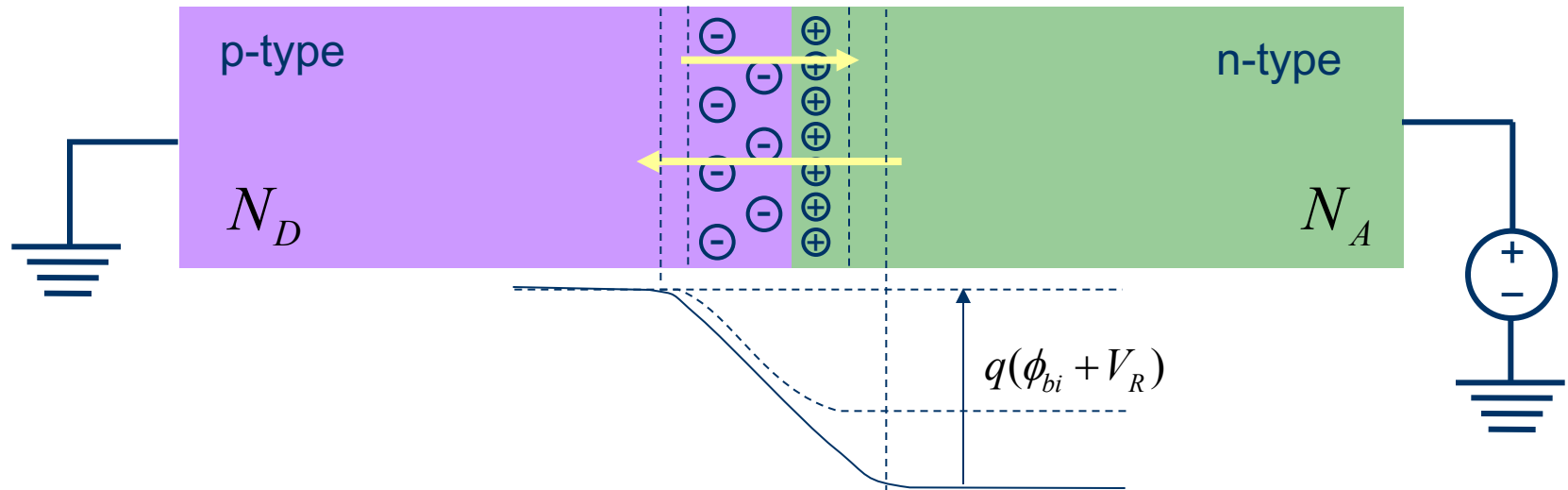
- Reverse Bias causes an increases barrier to diffusion
- Diffusion current is reduced exponentially



- Drift current does not change
- Net result: Small reverse current

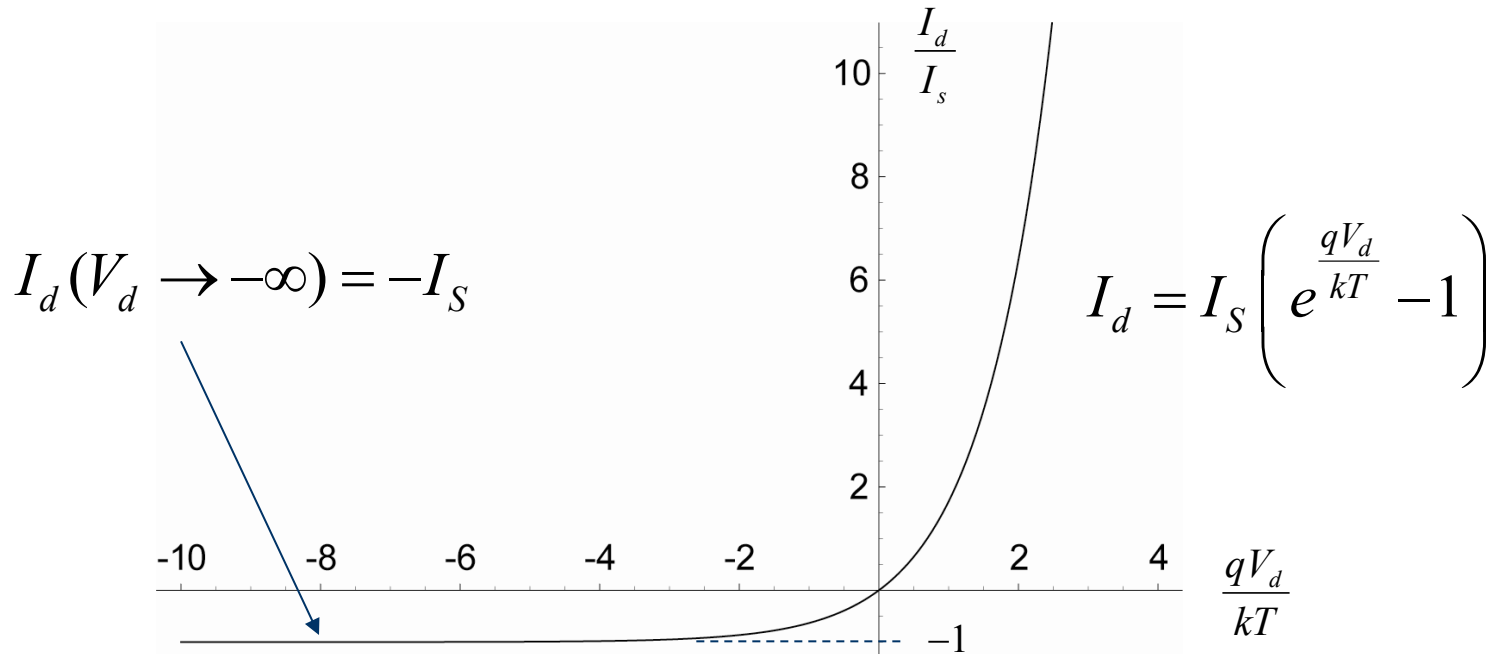
Forward Bias

- Forward bias causes an exponential increase in the number of carriers with sufficient energy to penetrate barrier
- Diffusion current **increases** exponentially



- Drift current does not change
- Net result: Large forward current

Diode I-V Curve



- Diode IV relation is an exponential function
- This exponential is due to the Boltzmann distribution of carriers versus energy
- For reverse bias the current saturations to the drift current due to minority carriers

Minority Carriers at Junction Edges

Minority carrier concentration at boundaries of depletion region increase as barrier lowers ...
the function is

$$\frac{p_n(x = x_n)}{p_p(x = -x_p)} = \frac{\text{(minority) hole conc. on n-side of barrier}}{\text{(majority) hole conc. on p-side of barrier}}$$

$$= e^{-(\text{Barrier Energy}) / kT}$$

$$\frac{p_n(x = x_n)}{N_A} = e^{-q(\phi_B - V_D) / kT}$$

(Boltzmann's Law)

“Law of the Junction”

Minority carrier concentrations at the edges of the depletion region are given by:

$$p_n(x = x_n) = N_A e^{-q(\phi_B - V_D)/kT}$$

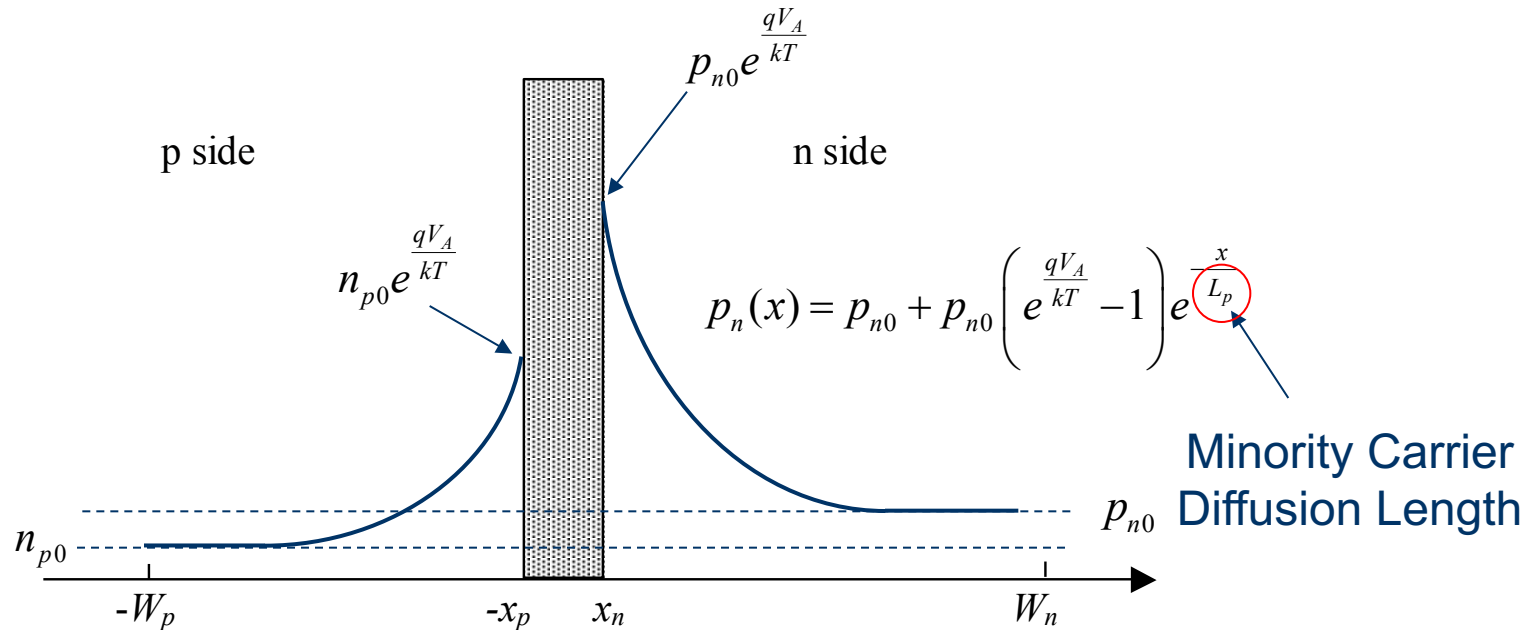
$$n_p(x = -x_p) = N_D e^{-q(\phi_B - V_D)/kT}$$

Note 1: N_A and N_D are the majority carrier concentrations on the *other* side of the junction

Note 2: we can reduce these equations further by substituting $V_D = 0$ V (thermal equilibrium)

Note 3: assumption that $p_n \ll N_D$ and $n_p \ll N_A$

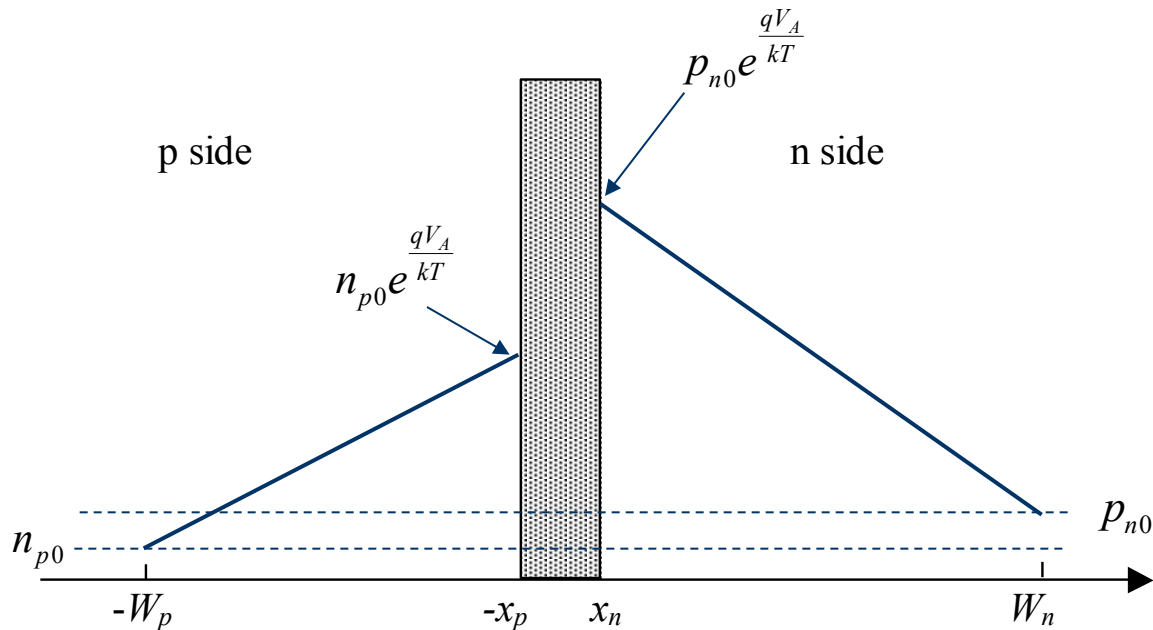
Minority Carrier Concentration



The minority carrier concentration in the bulk region for forward bias is a decaying exponential due to recombination

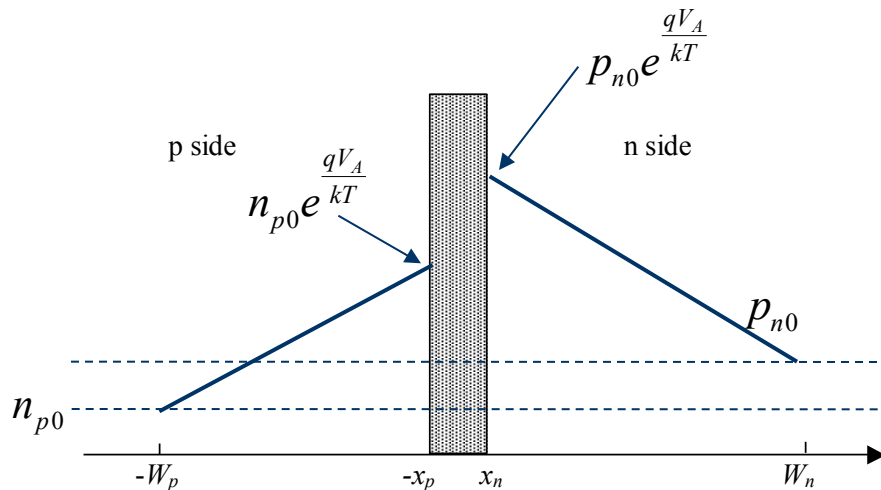
Steady-State Concentrations

Assume that none of the diffusing holes and electrons recombine \rightarrow get straight lines ...



This also happens if the minority carrier diffusion lengths are much larger than $W_{n,p}$ $L_{n,p} \gg W_{n,p}$

Diode Current Densities



$$\frac{dn_p}{dx}(x) \approx \frac{n_{p0} e^{\frac{qV_A}{kT}} - n_{p0}}{-x_p - (-W_p)}$$

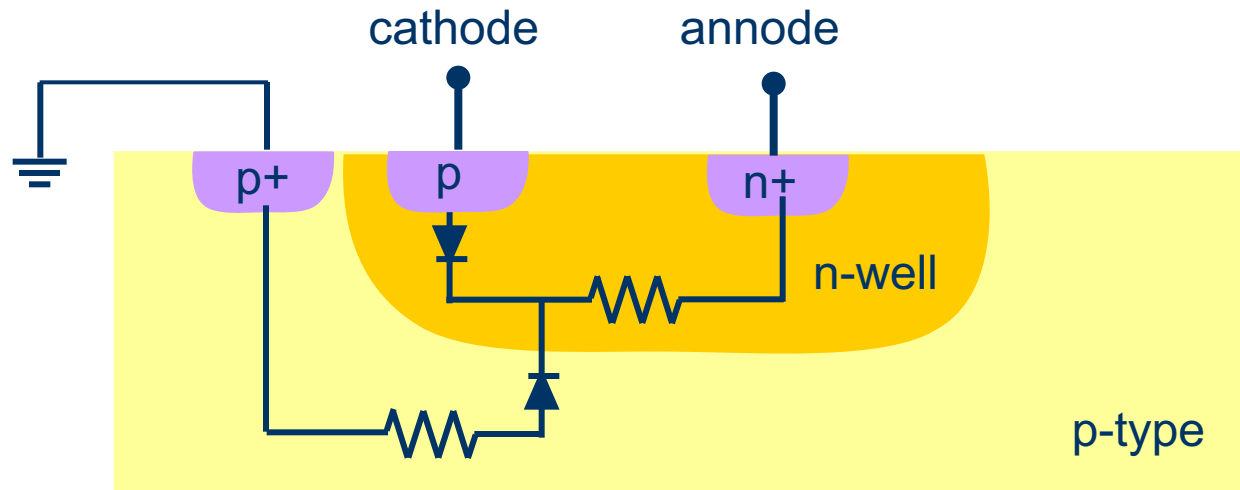
$$n_{p0} = \frac{n_i^2}{N_a}$$

$$J_n^{diff} = qD_n \left. \frac{dn_p}{dx} \right|_{x=-x_p} \approx q \frac{D_n}{W_p} n_{p0} \left(e^{\frac{qV_A}{kT}} - 1 \right)$$

$$J_p^{diff} = -qD_p \left. \frac{dp_n}{dx} \right|_{x=x_n} \approx -q \frac{D_p}{W_n} p_{n0} \left(1 - e^{\frac{qV_A}{kT}} \right)$$

$$J^{diff} = qn_i^2 \left(\frac{D_p}{N_d W_n} + \frac{D_n}{N_a W_p} \right) \left(e^{\frac{qV_A}{kT}} - 1 \right)$$

Fabrication of IC Diodes



- Start with p-type substrate
- Create n-well to house diode
- p and n+ diffusion regions are the cathode and anode
- N-well must be reverse biased from substrate
- Parasitic resistance due to well resistance

Diode Small Signal Model

- The I-V relation of a diode can be linearized

$$I_D + i_D = I_S \left(e^{\frac{q(V_d + v_d)}{kT}} - 1 \right) \approx I_S e^{\frac{qV_d}{kT}} e^{\frac{qv_d}{kT}}$$

$$e^x = 1 + x + \frac{x^2}{2!} + \frac{x^3}{3!} + \dots$$

$$I_D + i_D \approx I_D \left(1 + \frac{q(V_d + v_d)}{kT} + \dots \right)$$

$$i_D \approx \frac{qv_d}{kT} = g_d v_d$$

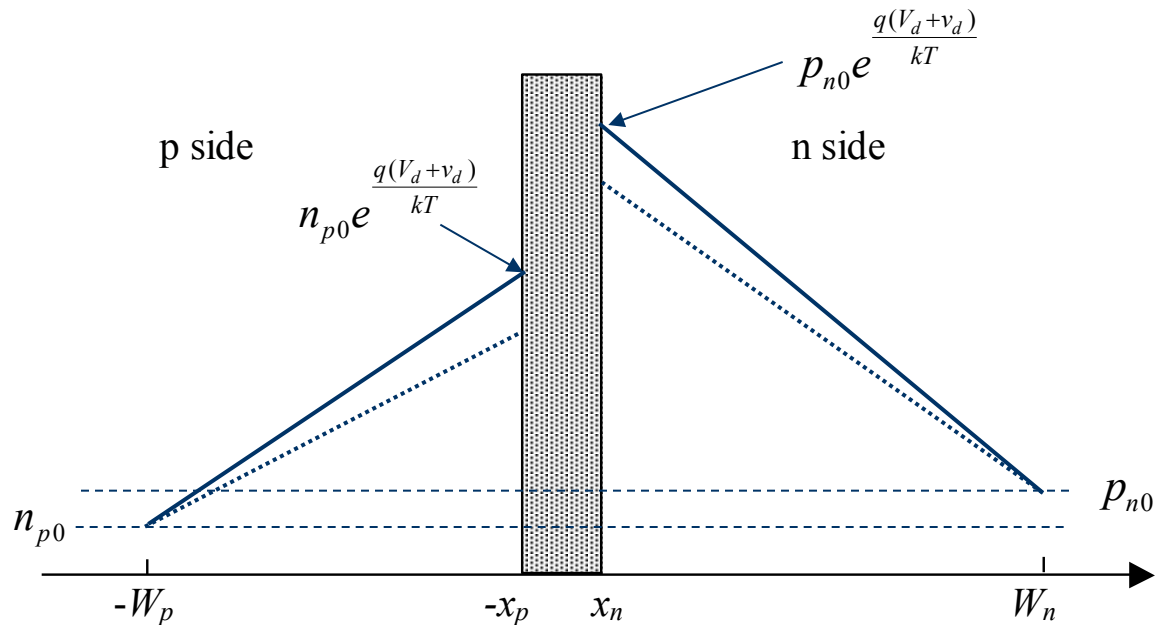
Diode Capacitance

- We have already seen that a reverse biased diode acts like a capacitor since the depletion region grows and shrinks in response to the applied field. The capacitance in forward bias is given by

$$C_j = A \frac{\epsilon_s}{X_{dep}} \approx 1.4C_{j0}$$

- But another charge storage mechanism comes into play in forward bias
- Minority carriers injected into p and n regions “stay” in each region for a while
- On average additional charge is stored in diode

Charge Storage



- Increasing forward bias increases minority charge density
- By charge neutrality, the source voltage must supply equal and opposite charge

- A detailed analysis yields:
$$C_d = \frac{1}{2} \frac{qI_d}{kT} \tau$$

Time to cross junction
(or minority carrier lifetime)

Diode Circuits

- Rectifier (AC to DC conversion)
- Average value circuit
- Peak detector (AM demodulator)
- DC restorer
- Voltage doubler / quadrupler / ...